



Produced by: KK297 Approved by:
Creation date: 31 August 2010

Revision: Sign:
Revision date:

Design Drawings

1.1 Mechanical and Hydraulic Drawings

Drawing Title	Drawing Number	Design
Shafting		
Shafting Arrangement	DMN200000864 rev E	
Main Assembly and Marking Drawing	DMN200001313 rev A	
Propeller Unit Drawing with Marking, Port	RRM200005971 rev B	
Propeller Unit Drawing with Marking, Starboard	RRM200005972 rev B	
Propeller Shaft Assembly	RRM200005966 rev B	
Twin tube	RRM200008623 rev A	
Stern Tube Assembly	RRM200006467 rev A	
Stern Tube Bearing Aft	RRM200006474 rev B	
Stern Tube Intermediate Bearing	RRM200006475 rev B	
Stern Tube Bearing forward	RRM200006476 rev B	
SKF Coupling Assembly	RRM200005975 rev A	
PDn Diagram	10S000239/42061-O	
Propeller Hub		
Hub Assembly Left	RRM200009345 rev A	
Blade Outline	10S000239/R185033-O	
Tightening and Locking of Screws		
Instruction for Tightening of Screws	586431 rev A	
Instruction for Locking of Screws	998174 rev A	
Plug for Lifting Hole Assembly	144 112 rev –	
Oil Distribution Box		
OD-box Assembly	214 000 rev A	
OD-box Dimension	154 903	
OD-box Connection to Gear	214740	
Feed Back Box Assembly (F0/FA)	RRM200000128 rev C	



Drawing Title	Drawing Number	Design
Hydraulic System		
Hydraulic System Assembly	RRM200007036 rev B	
Hydraulic Diagram	DMN200000689 rev D	
Gravity Tank Assembly	RRM200011521 rev A	
 Hydraulic Power Pack	RRM200007037 rev D	
Connection Diagram Power Pack	DMN200000981 rev B	
 Pump Motor Starter P1/P2	RRM200007038 rev B	
Pump Motor Starter P3	RRM200007039 rev B	
 Cable drawing	DMN200000983 rev B	
Cable Connection drawing	DMN200000984 rev B	
 Remote Supervision Hydraulic	DMN200000982 rev B	



Produced by: WKM Approved by: Ena
Creation date: 2010-04-15

Revision: A Sign:
Revision date:

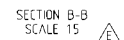
Design Drawings

Yard: Halifax Shipyard

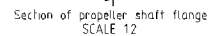
Yard number: 2603

Remote Control System

Drawing Title	Drawing Number	Revision
Main drawing	RRM200005995	A
Bom Report	RRM200005995	A
Cable drawing	DMN200001162	A
Cable connection drawing	DMN200001162	A
Load curve	-	-
Combinator diagram	-	-
Control panel Main bridge PORT	RRM200005922	A
Control panel Main bridge STBD	RRM200005925	A
Control panel Wing stations (PORT propeller)	RRM200005949	A
Control panel Wing stations (STBD propeller)	RRM200005950	A
Control panel ECR	RRM200005951	A
Load control panel	RRM200001864	A
Sep. RPM control panel	RRM200002414	A
Clutch Control panel Main bridge	RRM200005928	A
Clutch Control panel ECR	RRM200005952	A
RPM indicator	128 952	-
RPM indicator ECR	128 967	-
Impulse band	107 127	b
RPM transmitter for indication	510 800	c
RPM transmitter for control system	107 009	c
Central unit	129 066	b
Clutch Control unit	129 066	b

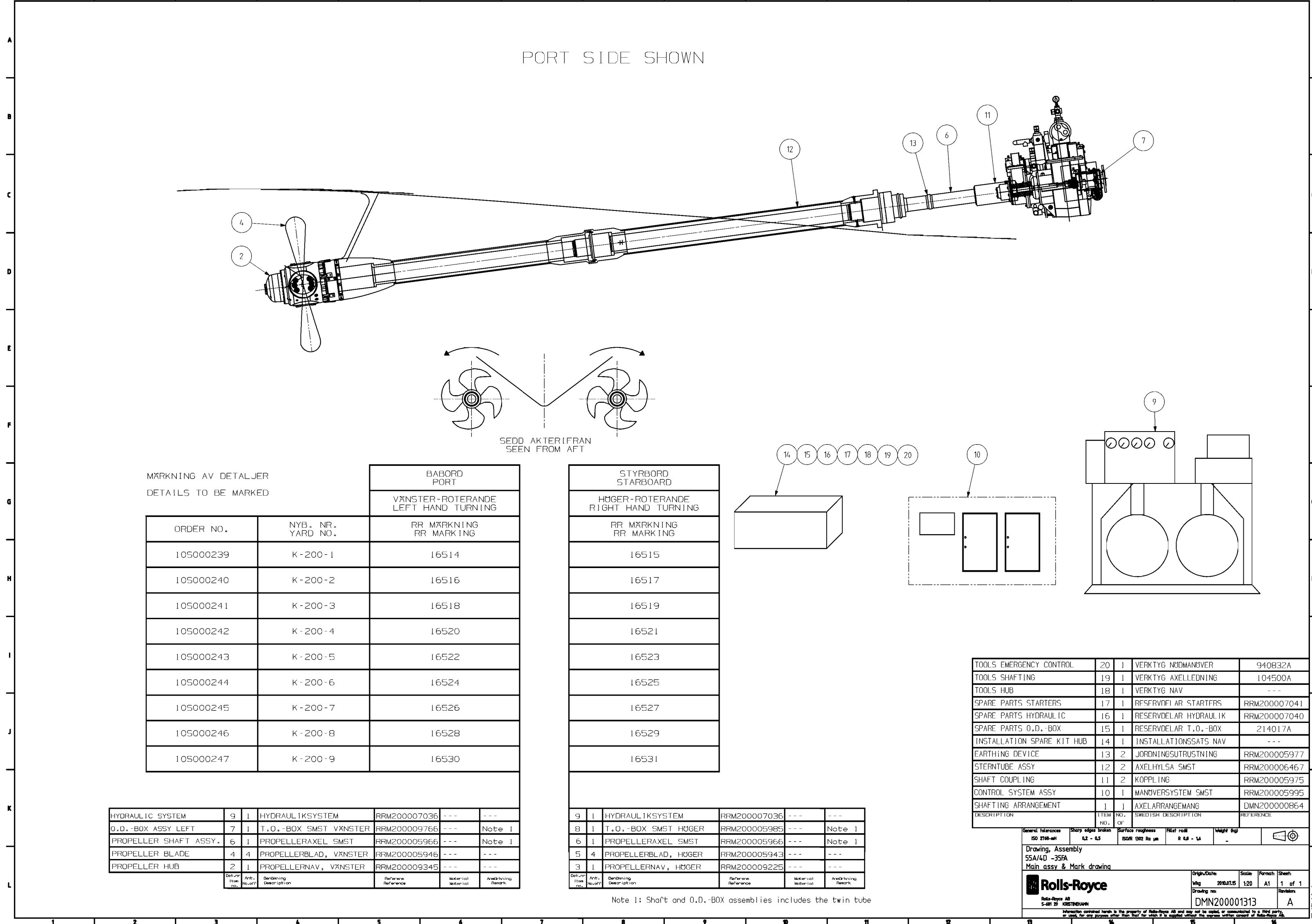
[illegible]

PROTECTION COVER IS OPTIONAL
MAY BE REMOVED AFTER INSTALLATION



 Rolls-Royce Rolls-Royce AB S-401 FF KISTINGSÄNN	Origin/Date		Scale	Format	Sheet
	JA 2003.02.22		1:20	A1	1 of 1
	Drawing no.		Revision		
	DMN200000864		E		

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PORT SIDE SHOWN

SEDD AKTERIFRAN
SEEN FROM AFT

MÄRKNING AV DETALJER
DETAILS TO BE MARKED

		BABORD PORT
		VÄNSTER-ROTERANDE LEFT HAND TURNING
ORDER NO.	NYB. NR. YARD NO.	RR MÄRKNING RR MARKING
10S000239	K-200-1	16514
10S000240	K-200-2	16516
10S000241	K-200-3	16518
10S000242	K-200-4	16520
10S000243	K-200-5	16522
10S000244	K-200-6	16524
10S000245	K-200-7	16526
10S000246	K-200-8	16528
10S000247	K-200-9	16530

HYDRAULIC SYSTEM	9	1	HYDRAULIKSYSTEM	RRM200007036	---	---
O.D.-BOX ASSY LEFT	7	1	T.O.-BOX SMST VÄNSTER	RRM200009766	---	Note 1
PROPELLER SHAFT ASSY.	6	1	PROPELLERAXEL SMST	RRM200005966	---	Note 1
PROPELLER BLADE	4	4	PROPELLERBLAD, VÄNSTER	RRM200005946	---	---
PROPELLER HUB	2	1	PROPELLERNAV, VÄNSTER	RRM200009345	---	---
	Defining Item no.	Ant. No./of	Denoting Description	Reference Reference	Material Material	Anmärkning Remark

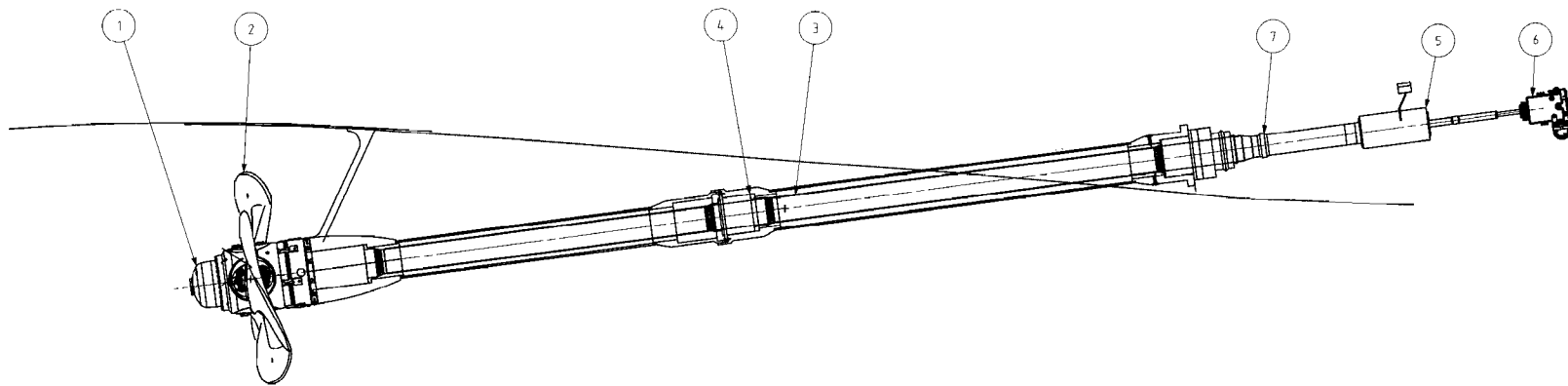
		STYRBORD STARBOARD
		HÖGER-ROTERANDE RIGHT HAND TURNING
		RR MÄRKNING RR MARKING
		16515
		16517
		16519
		16521
		16523
		16525
		16527
		16529
		16531



9	1	HYDRAULIKSYSTEM	RRM200007036	---	---
8	1	T.O.-BOX SMST HÖGER	RRM200005985	---	Note 1
6	1	PROPELLERAXEL SMST	RRM200005966	---	Note 1
5	4	PROPELLERBLAD, HÖGER	RRM200005943	---	---
3	1	PROPELLERNAV, HÖGER	RRM200009225	---	---
Defining Item no.	Ant. No./of	Denoting Description	Reference Reference	Material Material	Anmärkning Remark

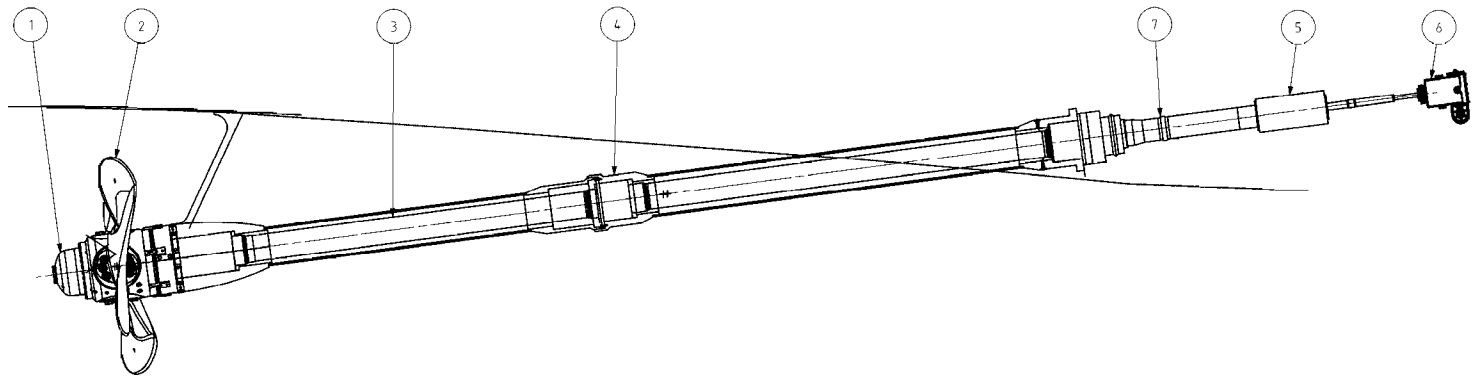
Note 1: Shaft and O.D.-BOX assemblies includes the twin tube

TOOLS EMERGENCY CONTROL	20	1	VERKTYG NÖDMÅNÖVER	940832A
TOOLS SHAFTING	19	1	VERKTYG AXELLEDNING	104500A
TOOLS HUB	18	1	VERKTYG NAV	---
SPARE PARTS STARTERS	17	1	RESERVDELAR STARTERS	RRM200007041
SPARE PARTS HYDRAULIC	16	1	RESERVDELAR HYDRAULIK	RRM200007040
SPARE PARTS O.D.-BOX	15	1	RESERVDELAR T.O.-BOX	214017A
INSTALLATION SPARE KIT HUB	14	1	INSTALLATIONSSATS NAV	---
EARTHING DEVICE	13	2	JÖRNINGSTRUSTNING	RRM200005977
STERN TUBE ASSY	12	2	AXELHYLSA SMST	RRM200006467
SHAFT COUPLING	11	2	KOPPLING	RRM200005975
CONTROL SYSTEM ASSY	10	1	MÅNÖVERSYSTEM SMST	RRM200005995
SHAFTING ARRANGEMENT	9	1	AXELARRANGEMANG	DMN200000864
DESCRIPTION	ITEM NO.	NO. OF	SWEDISH DESCRIPTION	REFERENCE

General tolerances ISO 2768-mS	Sharp edges broken 0.2 - 0.5	Surface roughness ISO 1302 Ra µm	Filet radii R 0.8 - 1.6	Weight (kg)	
Drawing, Assembly 55A/4D -35FA Main assy & Mark drawing					
Rolls-Royce S-601 29 KÖSTENHAMN			Original Date: Whg 2010.07.15 Drawing no: DMN200001313	Scale: 1:20 Format: A1 Sheet: 1 of 1 Revision: A	
Information contained herein is the property of Rolls-Royce AB and may not be copied, or communicated to a third party, or used for any purpose other than that for which it is supplied without the express written consent of Rolls-Royce AB.					

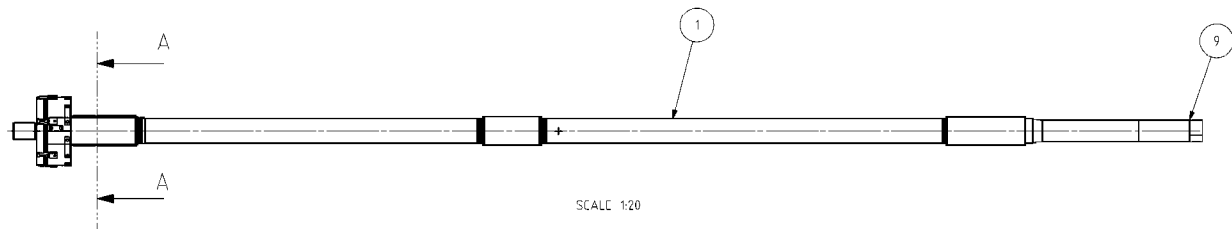


General tolerances ISO 2768-MS	Sharp edges broken 0.3 - 0.5	Surface roughness Ra 0.8 to 1.6	Fillet radii R 0.5 - 1.5	Weight (kg) 314.0	
Propeller Unit, CPP 55A/4-DBG Propellerenhet, Babord					
 Rolls-Royce Rolls-Royce AB S-401 37 10078014001			Original Date 2018.02.09	Scale 1:20	Format A1
Drawing no. RRM200005971			Sheet 1 of 1 Revisions B		
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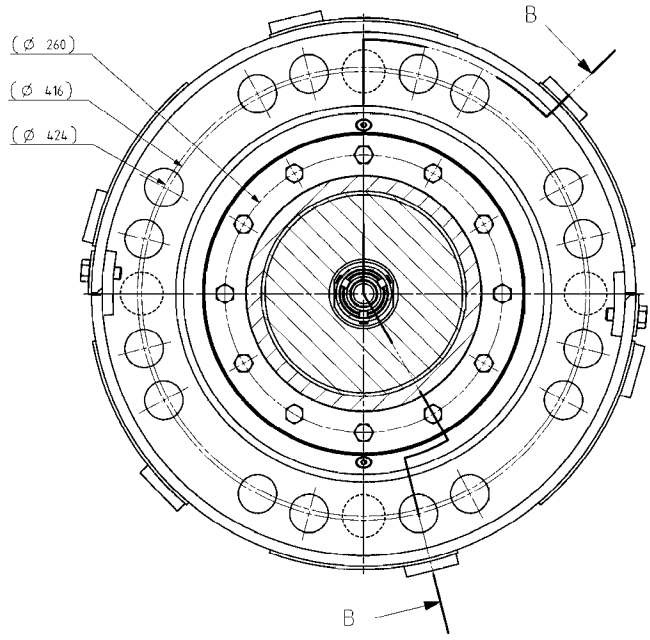
General tolerances ISO 2768-mS	Sharp edges broken 0.3 - 0.5	Surface roughness Ra 0.8 to 1.6	Fillet radii R 0.4 - 1.6	Weight (kg) 314.0	
Propeller Unit, CPP 55A/4-DBG Propellerenhet, styrbord					
Rolls-Royce Rolls-Royce AB S-401 27 100780244001		Originals 2018.02.09 Drawing no. RRM200005972		Scale 1:20 Format A1 Sheet 1 of 1 Revisions B	
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A
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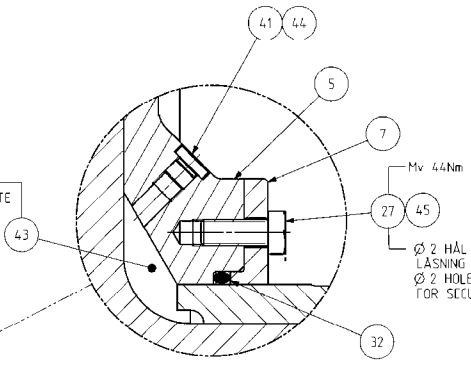
SCALE 1:20

YTORNA UNDER AXELFLÄNSSKYDDAD BELÄGGES
MED SKYDDSPÄSTA
THE SURFACES UNDER THE SHAFT FLANGE
COVER TO BE COATED WITH PROTECTION PASTE



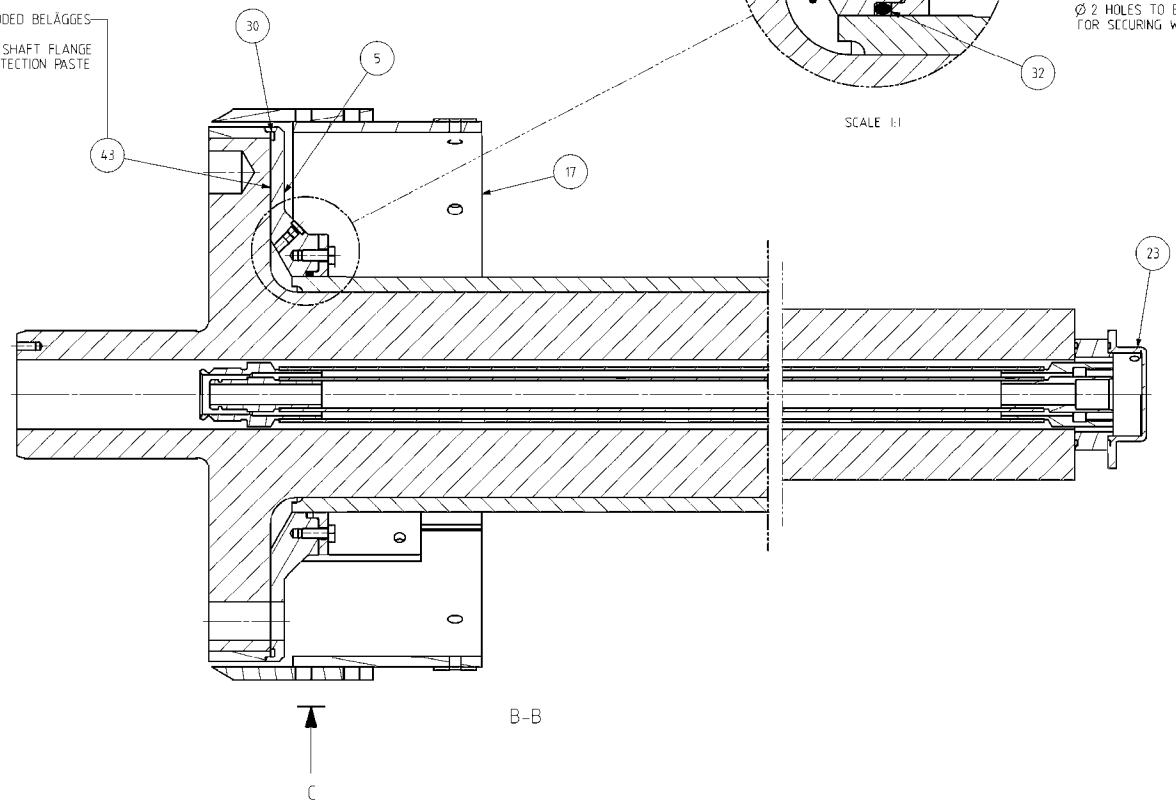
A-A
SKALA / SCALE 2:5

FYLLES MED SKYDDSPÄSTA
TO BE FILLED WITH PROTECTION PASTE



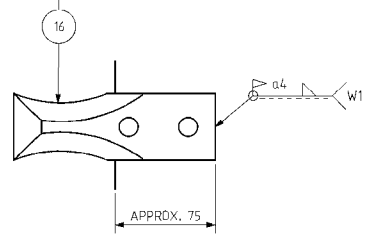
SCALE 1:1

Ø 2 HÅL BORRAS I BULTSKALLARNA FÖR
LÅSNING MED LÅSTRÅD
Ø 2 HOLES TO BE DRILLED IN BOLT HEADS
FOR SECURING WITH LOCKING WIRE



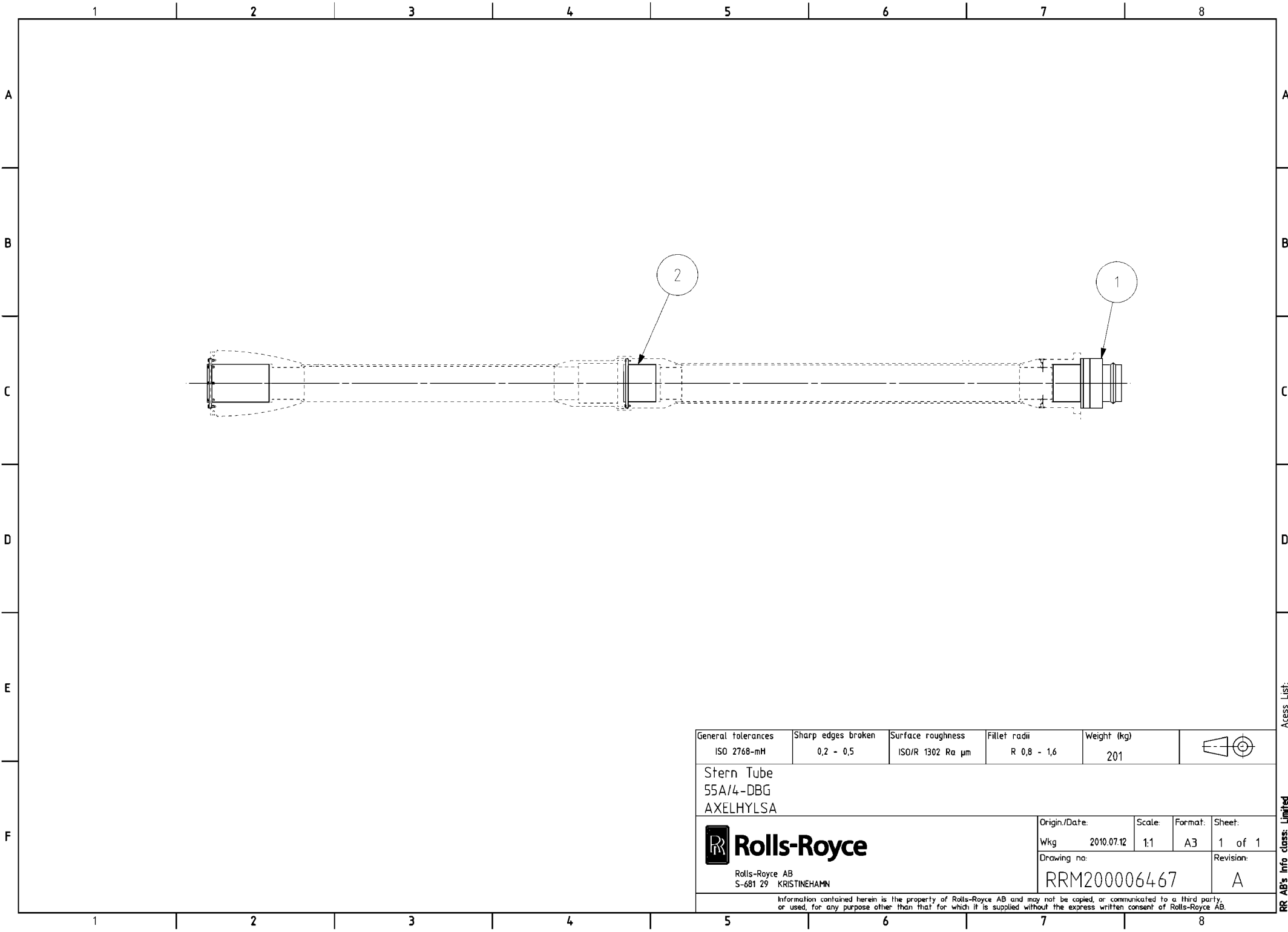
B-B

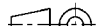

MONTERAS PÅ VÄR
TO BE MOUNTED BY YARD



VY / VIEW C
SCALE 1:2

SVETSBESTÄMMELSER		SVETTSSTANDARD FÖR ROLLS-ROYCE AB	
WELDING RULES		WELDING STANDARD FOR ROLLS-ROYCE AB	
GRUNDMATERIAL		PARENT METAL	
—		—	
AVSPANNINGSLÖSNINGSTEMPERATUR		SE SVETSDATABLAD	
STRESS-RELIEVING HEAT TREATMENT AT		SEE WELDING PROCEDURE SPECIFICATION (WPS)	
SVETSPÅN		SE SVETSDATABLAD	
SEQUENCE OF WELDING		SEE WELDING PROCEDURE SPECIFICATION (WPS)	
TÄTHETSKRAV		—	
SEALING REQUIREMENTS		—	
SVETSTOLERANS		EN ISO 13920-BE	
WELDING TOLERANCE		—	
PROVNINGSGRAF ATTENING		EXTENT OF EXAMINATION	
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SVETSMETOD		WELDING METHOD	
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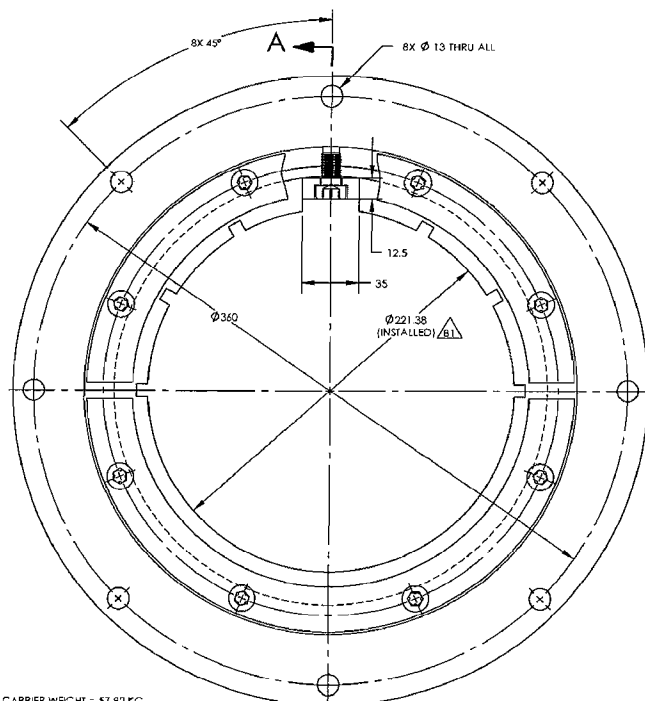


General tolerances ISO 2768-mH	Sharp edges broken 0,2 - 0,5	Surface roughness ISO/R 1302 Ra µm	Fillet radii R 0,8 - 1,6	Weight (kg) 201		
Stern Tube 55A/4-DBG AXELHYLSA						
 Rolls-Royce Rolls-Royce AB S-681 29 KRISTINEHAMN			Origin./Date: Wkg 2010.07.12	Scale: 1:1	Format: A3	Sheet: 1 of 1
			Drawing no: RRM200006467		Revision: A	
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Access List:

RR AB's Info class: Limited

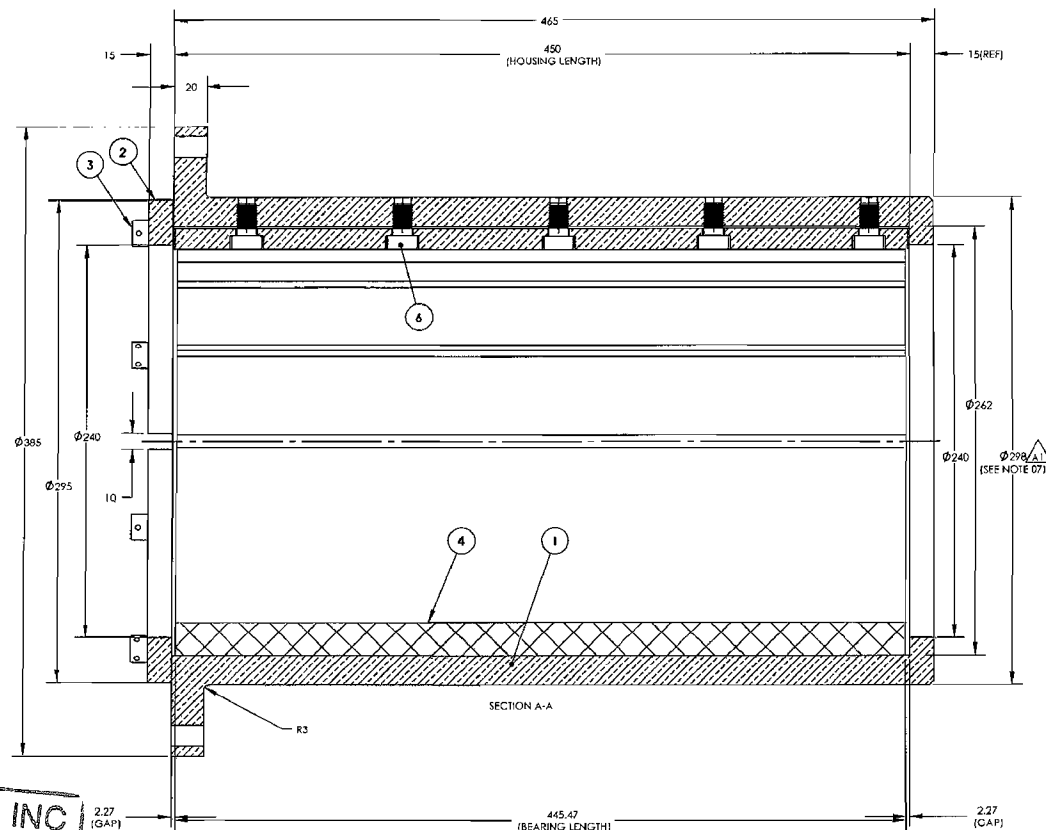
ITEM NO.	QTY.	PARTNO	DESCRIPTION	Material	REMARKS	DRAWING NUMBER
1	1	F-----	COMPAC BEARING	THORNDON COMPAC		TG-21126
2	1	F-----	RETAINING RING	BRONZE	SPLIT	TG-21128
3	1	F-----	KEY	BRONZE		TG-21129
4	5	F-----	CAPSCREW, LOW PROFILE HEX SOCKET HEAD	BRONZE C9540D	DIN 6912-M12X20	TG-21130
5	8	F-----	CAPSCREW, HEX SOCKET HEAD	ASI 316 ST. STEEL	DIN 912-M10 X 30	PURCHASE
6	1	F-----	CARRIER	BRONZE		TG-21127



A ←

THORDON BEARINGS INC
APPROVED
FOR
PRODUCTION

gt mof 2010
APPROVED BY



01. MATERIAL: SEE PARTS LIST
02. DIMENSIONS ARE EXPRESSED IN MM UNLESS NOTED OTHERWISE.
03. DO NOT SCALE THIS DRAWING WORK TO DIMENSIONS SPECIFIED.
04. TOLERANCES FOR ALL DIMENSIONS SHALL BE NONCUMULATIVE.
05. BREAK ALL CORNERS AND DEBURR ALL SHARP EDGES.
06. ALL FILLET AND RADIUS DIMENSIONS ARE NOMINAL UNLESS NOTED OTHERWISE.
07. SHIPSETS #1 THRU 4 SUPPLIED AT Ø295

	<h1>Rolls-Royce</h1>		Date	approved,
			2010-11-10	JH
Sheet	of	Drawing no:	Revision	
1	1	RRM 200 006 474	C	

DO NOT SCALE THIS DRAWING. WORK TO DIMENSIONS SPECIFIED

UNLESS SHOWN OTHERWISE, MACHINING TOLERANCES ARE:

LINEAR UP TO 1m(40") $\pm 0.5 \text{ mm} (\pm 0.020")$

OVER 1m(40') $\pm 1.0 \text{ mm} (\pm 0.040')$

ANGULAR $\frac{1}{0.25^\circ}$

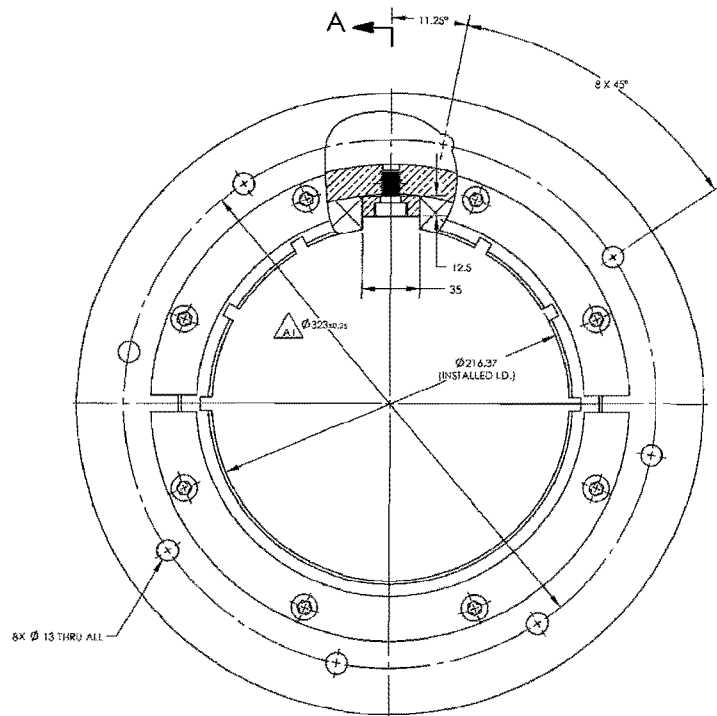
SURFACE FINISH 3.2 μ mRa (125 μ inch)

THORDON MATERIAL SURFACE FINISH TO BE DETERMINED ONLY BY USE OF COMPARATOR

B1	ADDED DIMENSION		10/29/2010	GL	CA	GA
A1	WAS Ø295 & ADDED NOTE 07		10/18/2010	GL	CA	GA
REV	DESCRIPTION		DATE	DWN	CKD	APPY
THORDON BEARINGS INC.						
DUNELTON ONTARIO CANADA						
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OWN /CROSS	SIGN CA/GRV	SIGN MPFL/AJL	SIGN			
C PREF/DI	G LAUGER	G LAUGER				
CUSTOMER/CUENT	DRAWING DATE DATE OF REVISION	HAT NO	SIZ			
SHR/TNTR	04-08-2010	MPFL-330				
THORDON COMPAC AFT BEARING ASSEMBLY			TC-20843	B		
			SHEET FOUR	I	I	I

ALL DIMENSIONAL INFORMATION IS BASED ON A MACHINING TEMPERATURE OF 21 °C, UNLESS STATED OTHERWISE. MACHINE GROOVES ONLY WHERE SHOWN

ITEM NO.	QTY.	PART NO	DESCRIPTION	MATERIAL	REMARKS	DRAWING NUMBER
1	1	F-----	BEARING	THORNDON COMPAC		TQ-21133
2	1	F-----	RETAINING RING	BRONZC		TQ-21138
3	1	F-----	KEY	BRONZE		TQ-21136
4	3	F-----	CAPSCREW, LOW PROFILE HEX SOCKET HEAD	BRONZE C95400	DIN 912-M12X20	TQ-21130
5	8	F-----	CAPSCREW, HEX SOCKET HEAD	AISI 316 ST. STEEL	DIN 912-M10 X 30	PURCHASE
6	1	F-----	CARRIER	BRONZE		TQ-21134



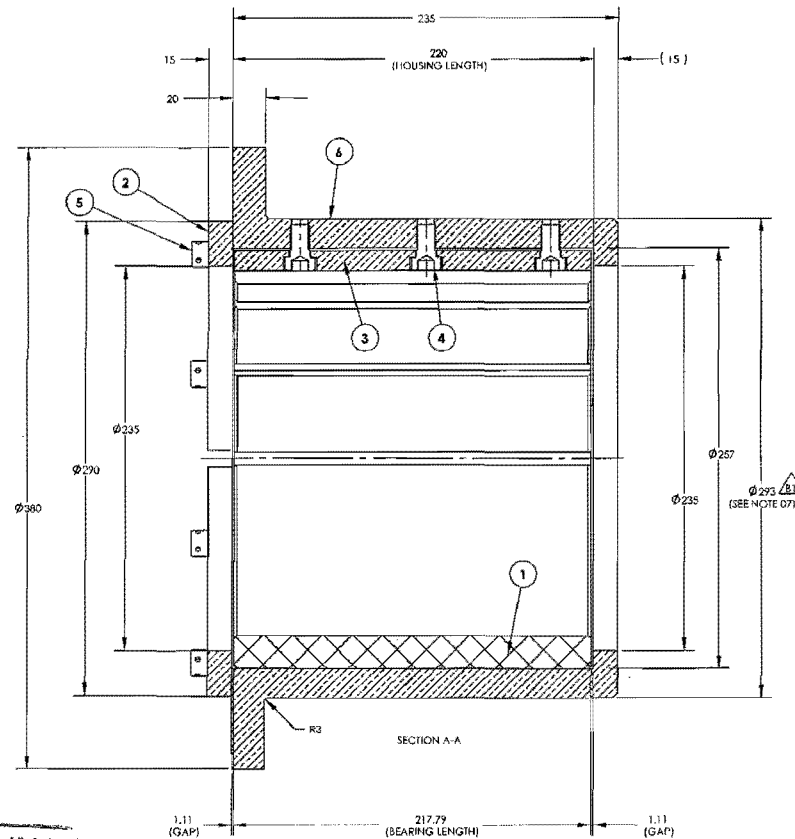
CARRIER WEIGHT = 32.5 KG.
BEARING WEIGHT = 3.5 KG.
MINIMUM INSTALLED CLEARANCE: 1.37
RUNNING CLEARANCE: 0.87
THERMAL EXPANSION ALLOWANCE: 0.19
WATER SWELL ALLOWANCE: 0.31
TEMPERATURE RANGE: -2°C TO 45 °C
SHAFT DIA.: = 215
HOUSING DIA.: = 257
HOUSING LENGTH = 220

GENERAL NOTES:

01. MATERIAL: SEE PARTS LIST
02. DIMENSIONS ARE EXPRESSED IN MM UNLESS NOTED OTHERWISE.
03. DO NOT SCALE THIS DRAWING. WORK TO DIMENSIONS SPECIFIED.
04. TOLERANCES FOR ALL DIMENSIONS SHALL BE NONCUMULATIVE.
05. BREAK ALL CORNERS AND DEBURR ALL SHARP EDGES.
06. ALL FILLET AND RADIUS DIMENSIONS ARE NOMINAL UNLESS NOTED OTHERWISE.
07. SHIPSETS #1 THRU 4 SUPPLIED AT Ø290

THORDON BEARINGS INC
APPROVED
FOR
PRODUCTION

APPROVED BY




Rolls-Royce
Date: 2010-11-10
 Approved: JH
 Sheet: 1 of 1
 Drawing no.: BRM 200 006 475
 Revision: C

B1	WAS Ø29D & ADDED NOTE 07	10/18/2010	CL	GA	GA
A1	B.C. WAS Ø350	10/5/2010	CP	GA	GA
RCV	DISCUSSION	DATE	ENVY	OKO	AMTV

THORDON BEARINGS INC.

BURLINGTON, ONTARIO, CANADA

DO NOT SCALE THIS DRAWING. WORK TO DIMENSIONS SPECIFIED

UNLESS SHOWN OTHERWISE, MACHINING TOLERANCES ARE:


LINEAR UP TO 1m/40° ± 0.5 mm/40°

OVER 1m(40") +/-1.0mm(50.940")

ANGULAR $\frac{1}{2}0.25^\circ$

SURFACE BRUSH 32mm/1in (125g/4.4oz)

THORDON MATERIAL SURFACE FINISH TO BE DETERMINED ONLY BY USE OF COMPARATOR

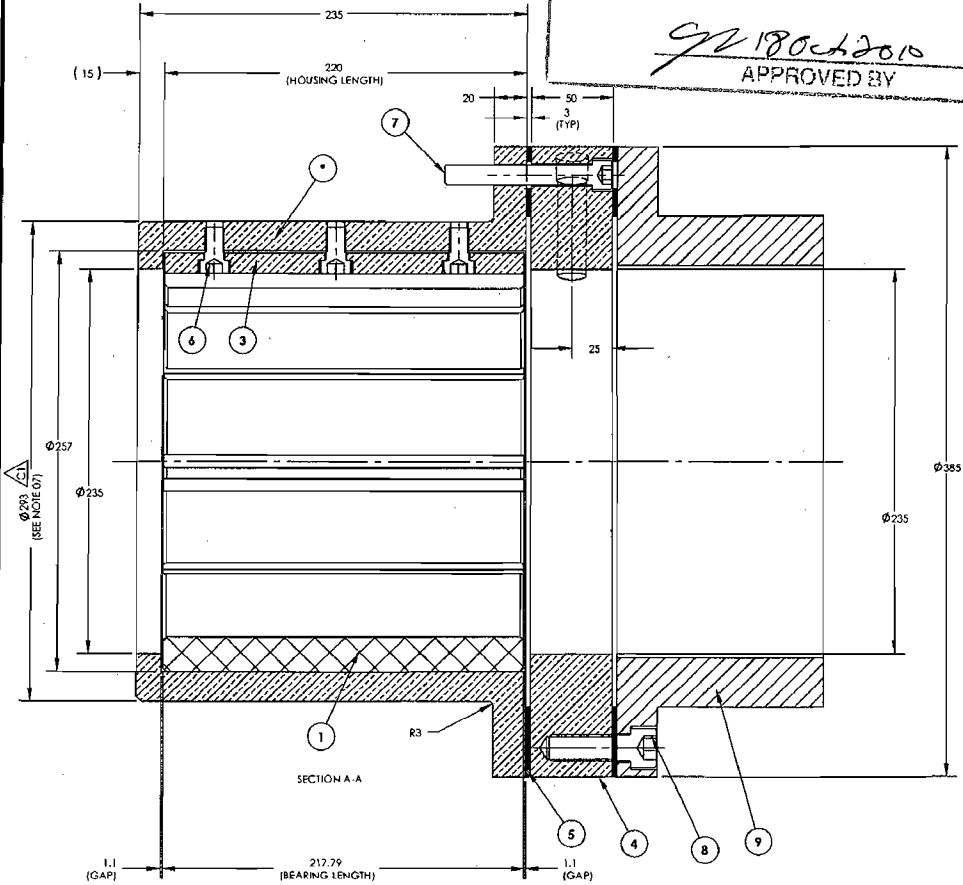
Drawn/DESSE	DESIGN	Check/CHK	DESIGN	APPROVAL	DESIGN	
C.FREDDI		G.AUGER		G.AUGER		
CUSTOMER/CLIENT		Drawing Date DATE DU DESSIN		Weld No.		Size
ROELS ROYCE DUWEL TECHNO		06-AUG-2010		F		C
Title/TITRE		Drawing No. du Dessin				REV
THORDON COMPAC INTERMEDIATE BEARING ASSEMBLY				TG-20844		B
Sheet FEUILLE				1		OF 1 DE 1

F197750331

ALL DIMENSIONAL INFORMATION IS BASED ON A MACHINING TEMPERATURE OF 21 °C, UNLESS STATED OTHERWISE. MACHINE GROOVES ONLY WHERE SHOWN

THORDON BEARINGS INC
APPROVED
FOR
PRODUCTION

9/21/2010
APPROVED BY

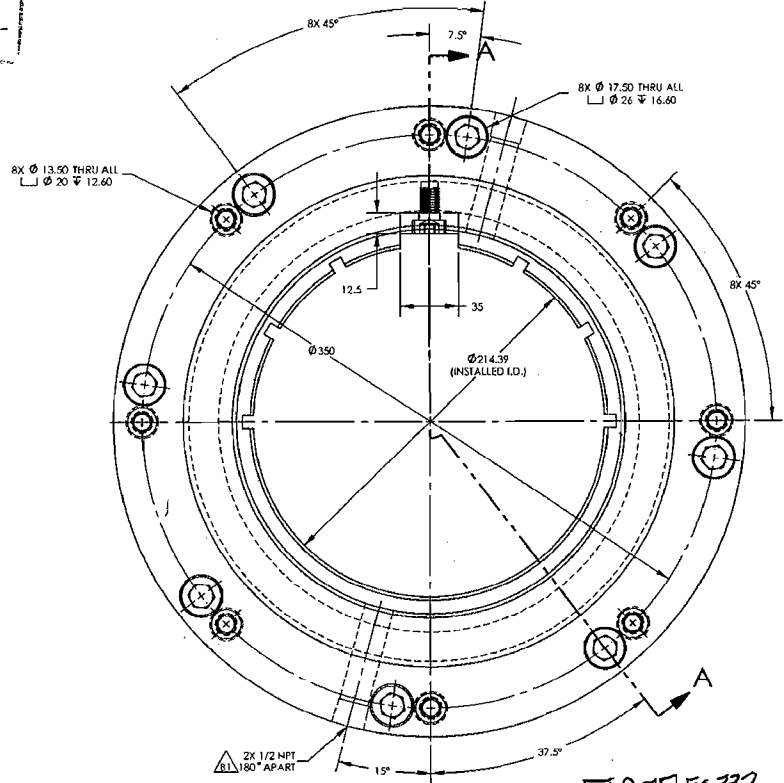


CARRIER WEIGHT = 33.05KG.
BEARING WEIGHT = 3.7KG
MINIMUM INSTALLED CLEARANCE: 1.39
RUNNING CLEARANCE: 0.87
THERMAL EXPANSION ALLOWANCE: 0.20
WATER SWELL ALLOWANCE: 0.32
TEMPERATURE RANGE: -2 °C TO 45 °C
SHAFT DIA.: = 213
HOUSING DIA.: = 257
HOUSING LENGTH = 220

GENERAL NOTES:

01. MATERIAL: SEE PARTS LIST
02. DIMENSIONS ARE EXPRESSED IN MM UNLESS NOTED OTHERWISE.
03. DO NOT SCALE THIS DRAWING. WORK TO DIMENSIONS SPECIFIED.
04. TOLERANCES FOR ALL DIMENSIONS SHALL BE NONCUMULATIVE.
05. BREAK ALL CORNERS AND DEBURR ALL SHARP EDGES.
06. ALL FILLET AND RADII DIMENSIONS ARE NOMINAL UNLESS NOTED OTHERWISE.
07. SHIPSETS #1 THRU 4 SUPPLIED AT Ø290

ITEM NO.	QTY.	PART NO.	Description	Material	REMARKS	DRAWING NUMBER
1	1	F	BEARING	THORDON COMPAC		TG-21140
2	1	F	CARRIER	BRONZE		TG-21141
3	1	F	KEY	BRONZE		TG-21142
4	1	F	RING	BRONZE		TG-21144
5	2	F	GASKET	GARLOK		TG-21145
6	3	F	CAPSCREW, LOW PROFILE HEX SOCKET HEAD	BRONZE C98400	DIN 6112-M12X20	TG-21130
7	8	F	CAPSCREW, HEX SOCKET HEAD	316 ST. STEEL	DIN 912-M12X90	PURCHASE
8	8		CAPSCREW, HEX SOCKET HEAD	AISI 316 ST. STEEL	DIN 912-M16X50 LG	BY CUSTOMER
9	1		MECHANICAL SEAL			BY CUSTOMER



FI97750332

Rolls-Royce		Date	Approved
Sheet of: 1		Drawing No: RRM 200 006 476	Revision: C

DO NOT SCALE THIS DRAWING. WORK TO DIMENSIONS SPECIFIED.

UNLESS SHOWN OTHERWISE, MACHINING TOLERANCES ARE:

LINEAR UP TO 1m (40") ±0.3 mm (0.012")
OVER 1m (40") ±1.0 mm (0.040")

ANGULAR ±0.25°

SURFACE FINISH 3.2µm Ra (125µinches)

THORDON MATERIAL SURFACE FINISH TO BE DETERMINED ONLY BY USE OF COMPARATOR

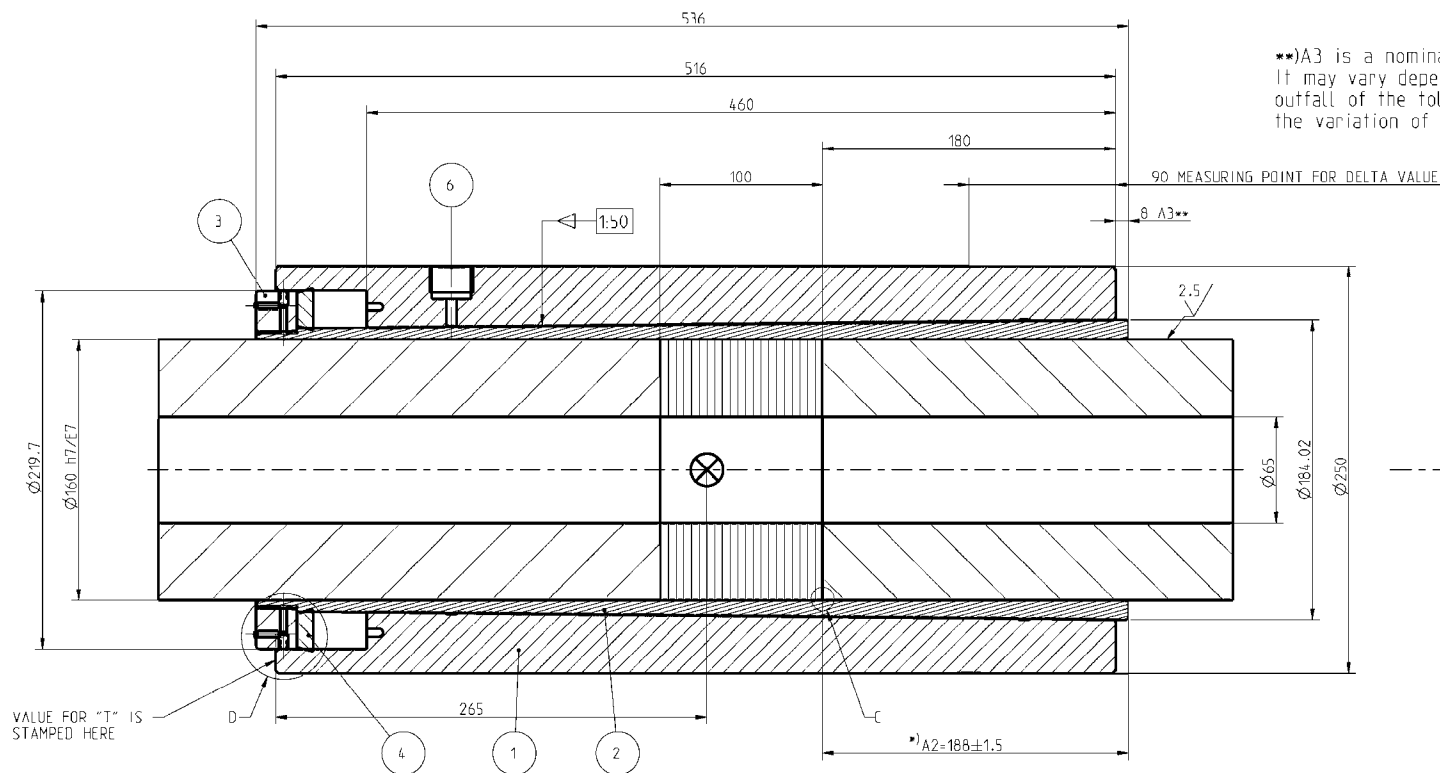
C1	WAS Ø290 & ADDED NOTE: 07	10/18/2010	GL	CA	GA
B1	ADDED NPT	9/22/2010	GL	CA	CA
A1	BOLT MATERIAL WAS BRONZE	8/18/2010	CP	CA	GA
REV	DESCRIPTION	DATE	BY	CHK	APP
THORDON BEARINGS INC. BURLINGTON, ONTARIO, CANADA					
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C. PREP'D	G. GAUGER	G. GAUGER	DATE	DATE	DATE
CUSTOMER/CLIENT	ROLLS ROYCE DUWELTECHNIEK	DRAWING DATE 06-AUG-2010	MRP NO.	F197750332	DWG. NO.
VILLE/STREET	THORDON COMPAC FWD. BEARING ASSEMBLY	DRAWING NO. DUWELTECHNIEK	REV	C	REV
			SHEET	1	OF 1

Permissible machining variations
in dimensions without tolerance
indicated: SS-ISO 2768-m.

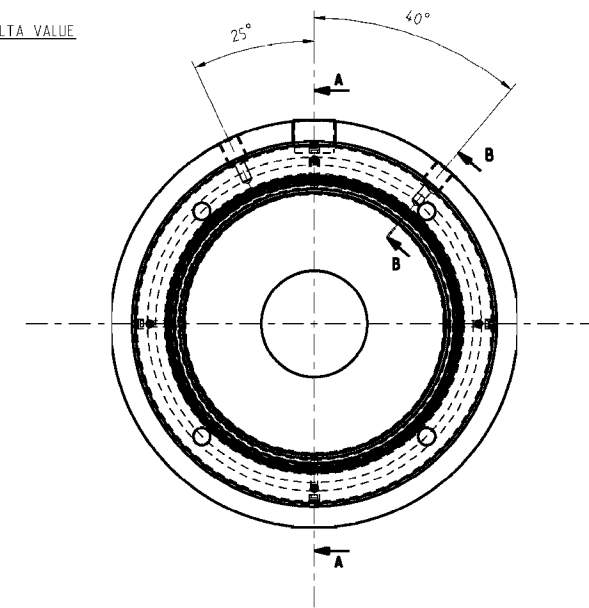


ORIGINAL SIZE:
A2

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**A3 is a nominal dimension.
It may vary depending on the
outfall of the tolerances and
the variation of shaft hole

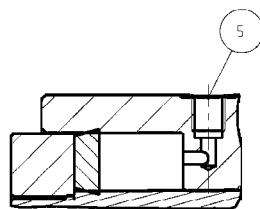


	Date		Approved:
	2011-01-25		JH
Sheet	of	Drawing no.	Revision:
1	1	RRM 200 005 975	B

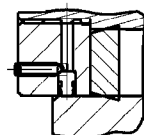
MAX TORQUE CAPACITY= 121 kNm

TOTAL WEIGHT= 115 KG

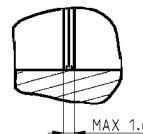
INERTIA WITH RESPECT TO CENTER AXIS= 1.3 kgm²



B-B



D



C

INCREASE OF COUPLING
OUTER DIAMETER

$\Delta = 0.24 \text{ mm}$

*) FINAL POSITIONING OF THE SHAFT (A2):
A2= 180.0+T-27.3
NOTE: VALUE FOR "T" IS STAMPED ON THE COUPLING

2	Torque and delta value changed	100920	MM	ME
Rev. No.	Revision Note	Date	Issued	Approved

1	6	PLUG BSP 3/4"			415182
2	5	PLUG BSP 1/4"			405024
1	4	SEALING	MSC001-60	0.3	38876-160
1	3	NUT	MSC001-30	3.0	38875-160
1	2	INNERSLEEVE	MSC001-44	20.7	3001670
1	1	OUTERSLEEVE	MSC001-11	91.0	28533
Qty.	Item	Name	Material	Weight	PartNo.
SKF PRODUCTS			Date	100430	Scale
OK COUPLING			Issued	SS	Checked AR
ASSEMBLY DRAWING			Project no.	90406	
OKCAX 160/28436			Drawing no.	28436	
Rolls-Royce					Revision 2
SKF COUPLING SYSTEMS AB					

**Rolls-Royce**

HYDRODYNAMIC RESEARCH CENTRE

Pd-n Diagram

Halifax Shipyard

Pe at 25.8 given, prop. factor. given, Curve est

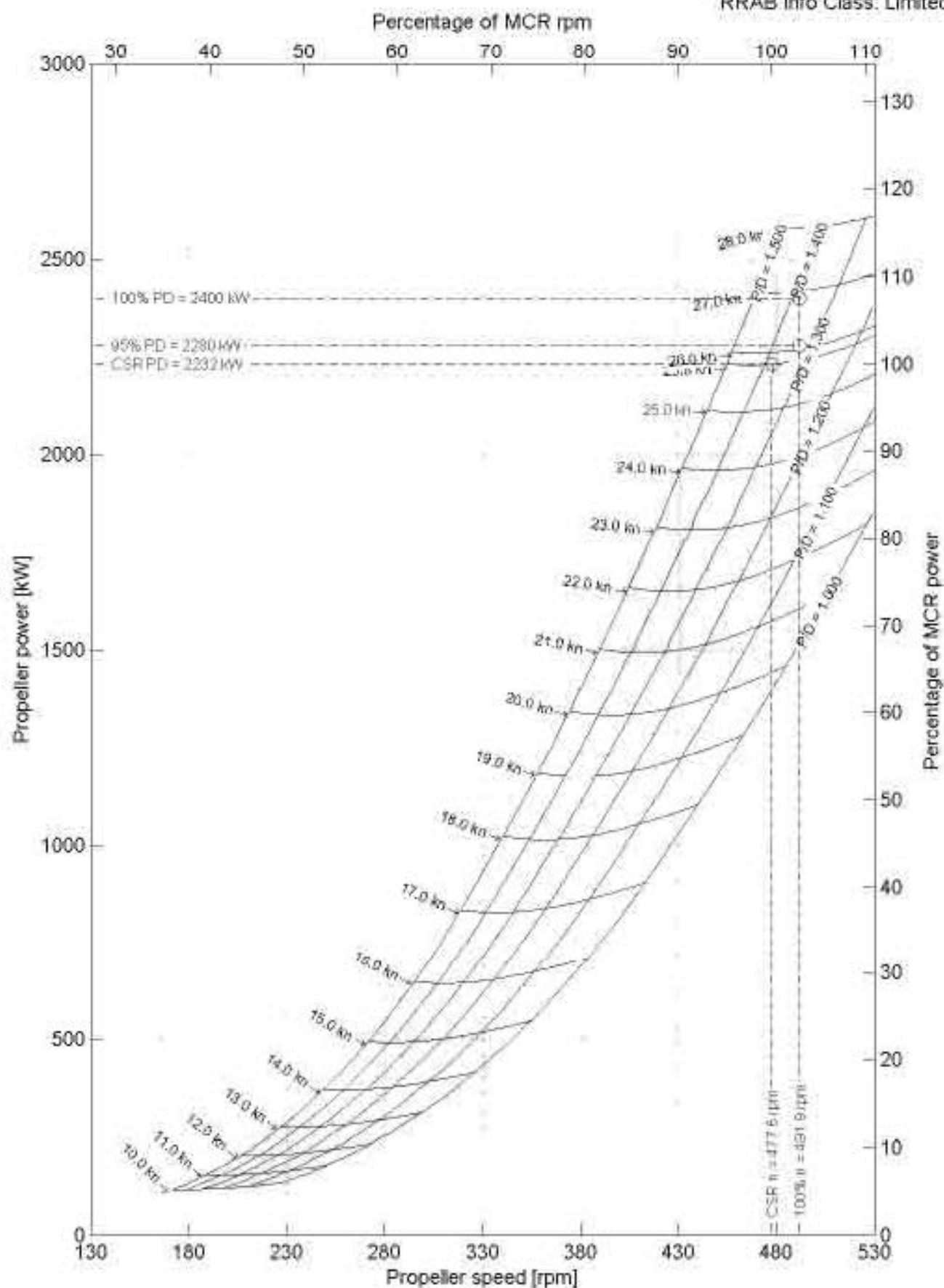
PDA No 42061

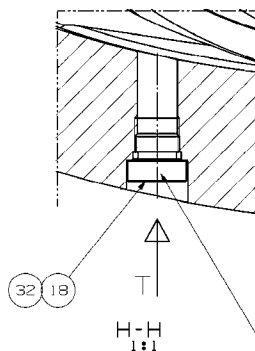
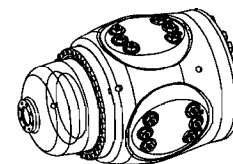
Classification No -

Date 2010-06-04

Title Fgr

RRAB Info Class: Limited





PLUGGEN LASES MED PUNKTSVETS
EFTER ATT AXELN ÄR INSTALLERAD
SYSTEMET OLFJEFYLLT OCH LUFTAT

THE PLUG TO BE LOCKED BY SPOT WELD
AFTER SHAFT IS INSTALLED
THE SYSTEM IS OIL FILLED AND VENTED


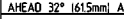
TÄTHETSPROV	PRESSURE TEST
FORE BEARBETNING BEFORE MACHINING	-
EFTER BEARBETNING AFTER MACHINING	X
KONTROLLMEDIUM TEST MEDIUM	OLJA OIL
KONTROLLTRYCK TEST PRESSURE	3 bar
KONTROLLTRYCK I RIKTNINGEN TEST PRESSURE APPLIED IN DIRECTION OF	PILENS TID RIKTNINGEN PILE'S TIME DIRECTION OF
TID TIME	5 h

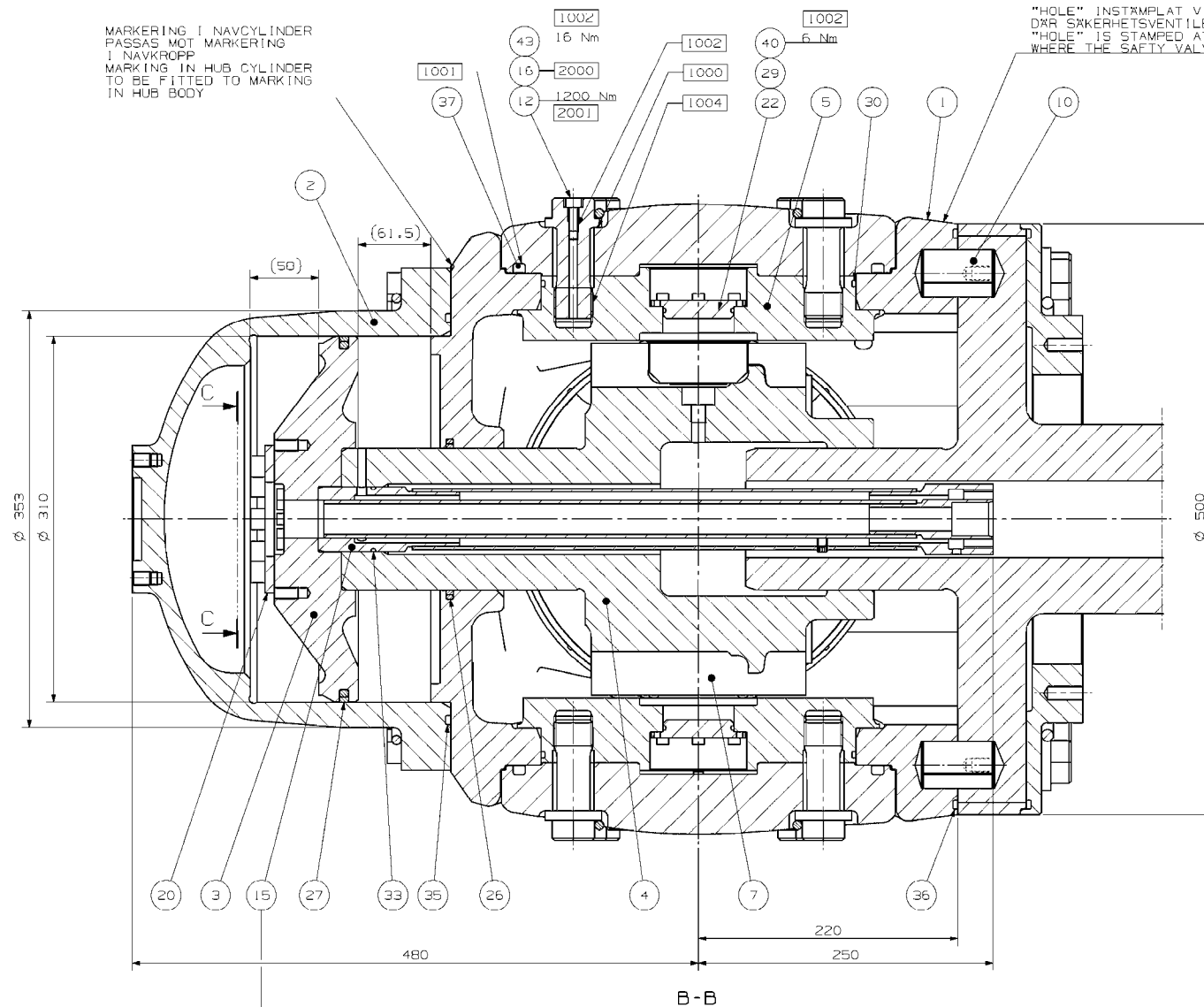
1000	KAMEWA SEALING COMPOUND
1001	TEFLON GREASE
1002	LOCTITE 243
1003	LOCTITE 648
1004	MOLYCOTE G-RAPID


2000	INSTRUCTION FOR LOCKING 998174A
2001	INSTRUCTION FOR TIGHTENING 586431A

Centre of gravity
256 - 300mm

PREVIOUS DRAWING RRM200006186

General tolerances ISO 2768-AS	Sharp edges broken 0.5 - 0.8	Surface roughness Ra 0.8 - 1.6	Heat treat H 0.8 - 1.6	Weight (kg) 4.78		
Propeller Hub 55A/48-B Left AHEAD 32° 161.5mm) ASTERN -30° (58mm)						
 Rolls-Royce Hälsjöberg AB S-201 79 KISTHEDALEN		Origin/Date Wng 2010/07/13		Scale 1:1	Format A1	Sheet 1 of 3
		Drawing no RRM200009345		Revisions A		
Information contained herein is the property of Rolls-Royce AB and may not be copied or communicated to a third party without the prior written consent of Rolls-Royce AB.						



General tolerances ISO 2768-MK	Sharp edges broken 0.3 - 0.5	Surface roughness ISO 1302 Ra 0.8 - 1.6	Heat roll R 0.8 - 1.6	Weight (kg) -	
Propeller Hub 55A/40-B Left AHEAD 32° (61.5mm) ASTERN -30° (58mm)					
<div>Rolls-Royce</div> <div>Rolls-Royce AB S-401 27 10070000000000</div>					
Origin/Date Wing 2008/07/09			Scale 1:2	Format A1	Sheet 2 of 3 Revision A
RRM200009345					
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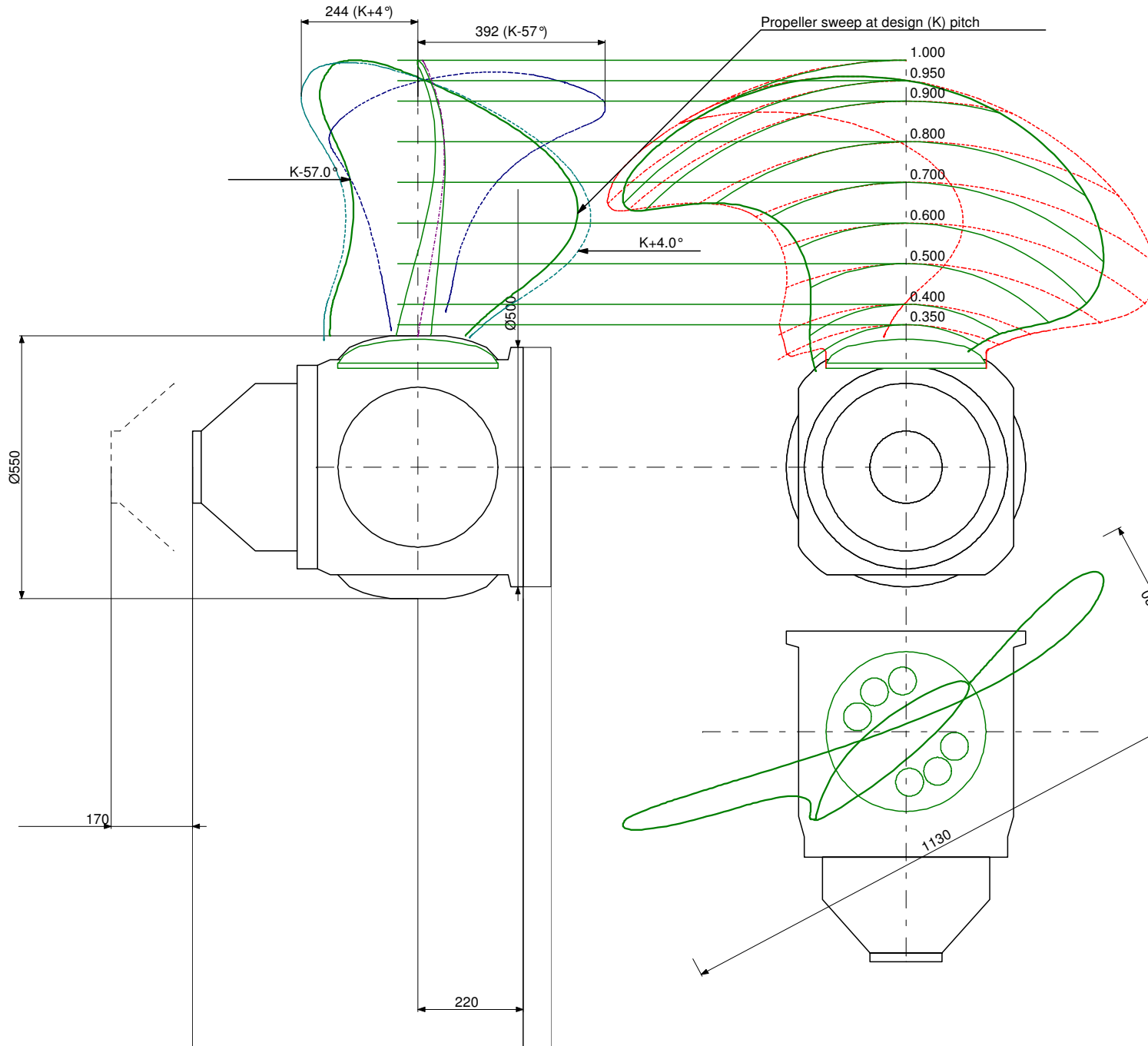


Rolls-Royce

Blade Outline

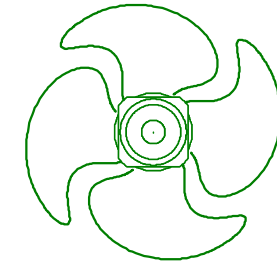
Ref:30-09-0920 10S000239-4/DESIGN

Date 2010-06-01 Time 10:26:03
Issued by
Rolf Fagerberg



r/R		0.35	0.6	0.95
Radius	mm	297.5	510	807.5
L	mm	481	805	698
LF	mm	206	522	2
LA	mm	275	283	696
Pitch	mm	1537	2281	1650
Max thickn.	mm	70	35	11.8

610



Propeller Data

Propeller diameter	(D)	1700 mm
Hub diameter	(d)	550 mm
Number of blades	(Z)	4
Expanded blade area ratio	(AE/A0)	0.757
Pitch ratio at 0.7R	(P0.7/D)	1.347

Data for One Blade

Expanded area	0.430 m ²
Weight	102 kg

K-200	
55A/4D-B-G	R-185033--O

Bild-kort	Utf. Design
—	A
—	B
—	C
—	D
—	E
—	F
—	G
—	H
—	K

Bild-Ändr. kort Revis	Zon Zone	Ändringen omfattar Revision comprises	Datum Date	Uppgj. Drawn	Godk. Approved	Tillåtna måttavvikelser när tolerans ej direkt utsatts på bearbetade detaljer SMS 715 Medel enligt tabell nedan. För rundingsradier, koner och vinkelmått Följ SMS 715 Medel enligt separat standardblad. Machining tolerances for linear dimensions unless otherwise specified for radii and curvatures, bevels and angle measurements, SMS 715 Average according to separate standard sheets must be followed.			
-	a	Texten kompletterad	801010	Deb	-				
-	b	KaMeWa-propeller utgick	860428	BLöw	-				
B	c	Text ändrad + omritad i CAD	920613	Alg	JnH	Basmått Basic size		Måttav- vikelser Tole- ranges	
B	d	Mått 1000 var felaktigt måttsatt	940829	Alg	JnH	Basmått Basic size		Måttav- vikelser Tole- ranges	
B	e	Text ändrad	950228	Alg	JnH	Basmått Basic size		Måttav- vikelser Tole- ranges	
-	f	Removed swedish text	000719	BEK	DB	Basmått Basic size		Måttav- vikelser Tole- ranges	
-	g	Svensk text tillkom	030916	Alg	K0	Basmått Basic size		Måttav- vikelser Tole- ranges	
						Modif. Modifikationen omfattar Modif. Modification comprises			
Bild- kort	Zon Zone	Datum Date	Uppgj. Drawn		Godk. Approved				
Use of tools for torque tightening									

Användning av momentdragningsverktyg

Momentdragningsverktyg användes för förspänning av blad-, axelfläns- och navcylinderskruv.

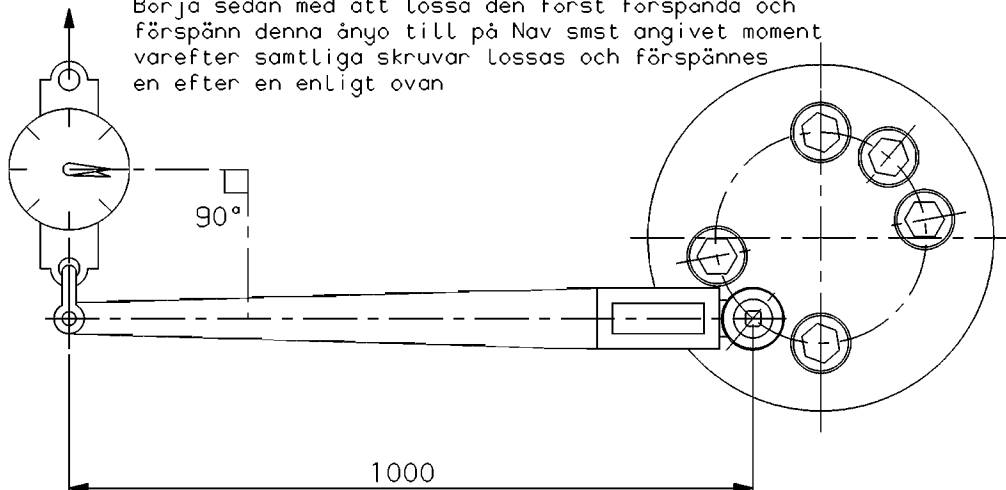
Vid förspänning skall smörjmedel påföras på skruvens gänga och tätningsmassa påföras under skruvskallen (se Nav smst).

Skruvorna skall förspännas två gånger.

- Kontrollera att skruven löper lätt i gängan. Ansätt samtliga skruvar med handverktyget.
- OBS! Mutterdragare (pneumatisk, hydraulisk eller elektrisk) får ej användas!
Montera verktygen för momentdragning enligt förebild.

- Förspänn skruvarna korsvis och avläs på dynamometern det på ritning Nav smst angivna momentet.

- Vänta i 15 minuter
Börja sedan med att lossa den först förspända och förspänn denna ånyo till på Nav smst angivet moment varefter samtliga skruvar lossas och förspännes en efter en enligt ovan



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KaMeWa

Use of tools for torque tightening

Tools for torque tightening are to be used pre-stressing of blade-, shaft flange- and hub cylinder screws.

Lubricant is to be used on the threads of the screw and sealing compound under the screw head when pre-stressing (see hub assembly drawing).


The screws are to be pre-stressed twice.

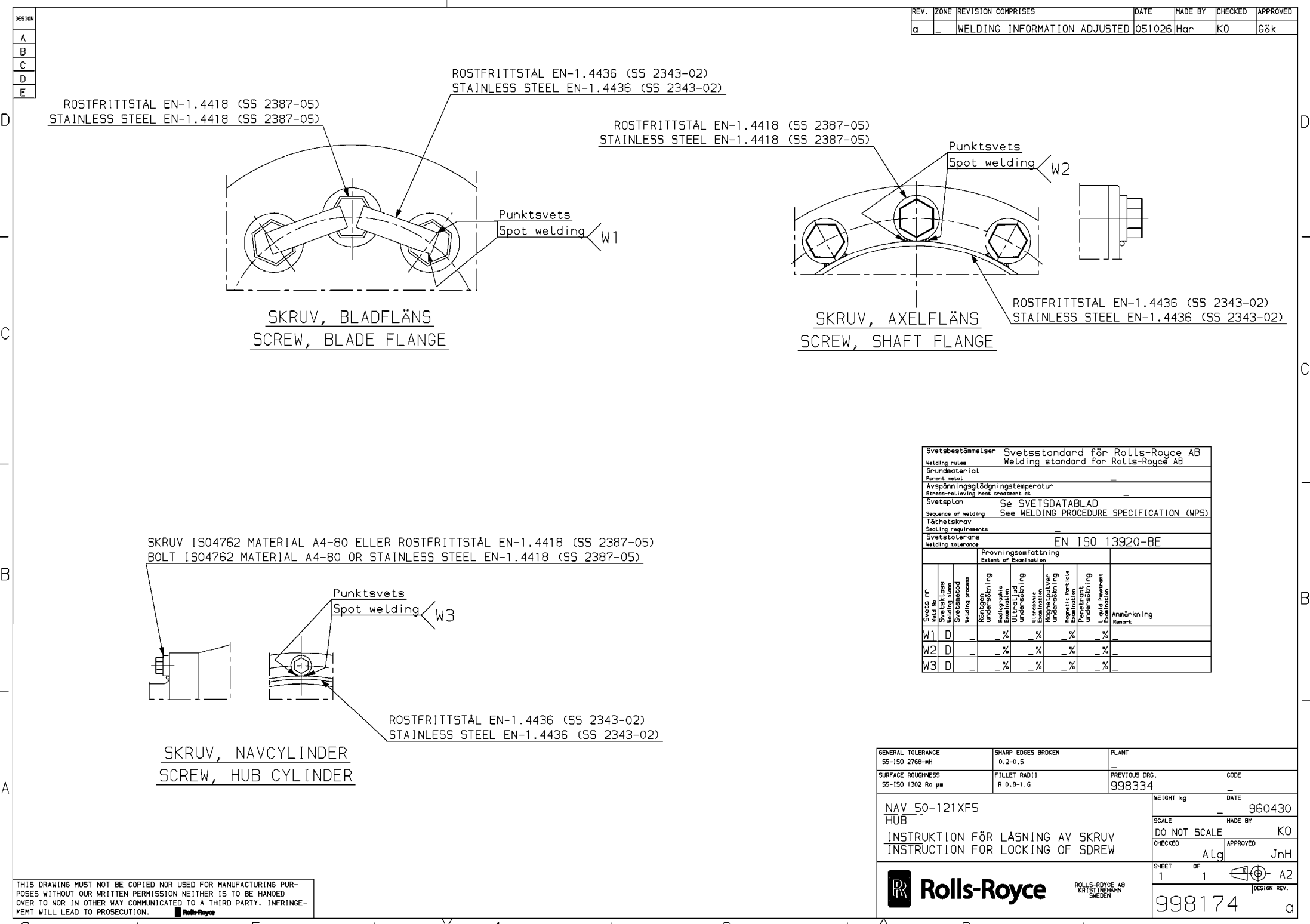
- Check that the screw runs easily in the thread. Tighten all the screws with a hand tool.

Note! Wrench (pneumatic, hydraulic or electric) may not be used!
torque tightening according to instructions.

- Pre-stress the screws crosswise and read on the dynamometer the torque stated on the hub assembly drawing.

- Wait in 15 minutes
Then begin untightening the screw first pre-stressed and pre-stress this again to the torque stated on the hub assembly drawing and then untighten all screws and pre-stress again one after each other according to above.

Det.nr Item no.	Ant. No. off	Benämning Description	Referens Reference	Material Material	Anmärkning Remark
Antäggning Plant	—	—	Best. nr/Prod. gr. nr. Order No./Prod. gr. No.	—	Tot. vikt Tot. weight kg
Uppgj. Drawn	Deb	Kontr. Checked	IP	Godk. Approved	Lös
			Ytjämnhet enligt SMS 672 Ra µm <input checked="" type="checkbox"/> <input checked="" type="checkbox"/> <input checked="" type="checkbox"/> Surface texture ISO/R 1302 Ra µm <input checked="" type="checkbox"/> <input checked="" type="checkbox"/> <input checked="" type="checkbox"/>		
Skala Scale —			Datum Date 800312		
Blad Sheet 1			av of 1		
Föreg. ritn. Previous drg. 577077			Ucf. Design Andr. Revis. g		
INSTR. FÖR DRAGNING AV SKRUV INSTR. FOR TIGHTENING OF SCREW			586431		



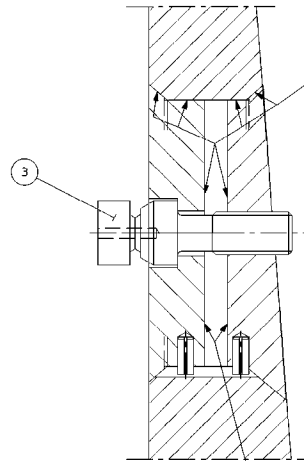
Rev. nr	Rev. nr	Rev. nr	Rev. nr
A	Det01-05	126	1 sats/blad
B			
C			
D			
E			
F			
G			
H			
I			

1. Avslipning av plugg utföres vid verkstad (Køllewa, Kristinehamn).
Grinding of plug to be carried out at the workshop.

2a,b,c. Fastsättning av plugg utföres vid varv.
Fastening of plug to be carried out at the shipyard.

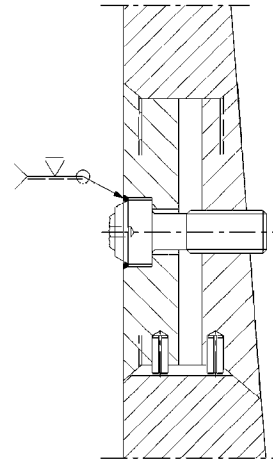
2a. Montering av pluggdetaljer.
Mounting of plug details.

Insmörjes med Køllewa Bolthead Sealing Compound eller någon rostskyddsolja före montage.
To be greased with Køllewa Bolthead Sealing Compound or some corrosion protecting oil before fitting.

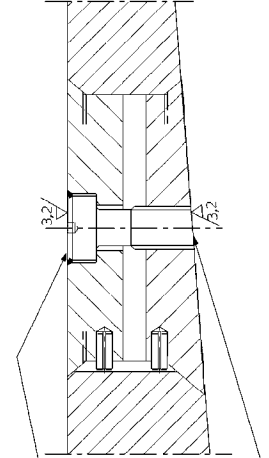


OBS! Propellerbladets klassnummer på insidan.
Observe the identification number of the propeller blade.

2b. Avdragnig av brottskruv och svetslåsning av skruvskalle.
Cracking and locking of crack-bolt.



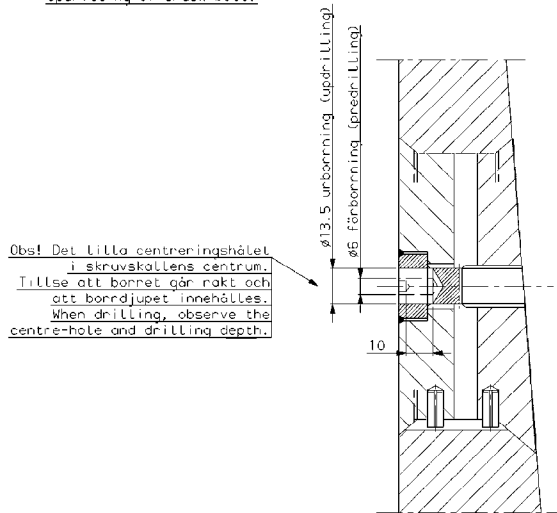
2c. Avslipning av brottskruv.
Grinding of crack-bolt.



Avslipnas jäms med pluggytan.
Flush to plug surface.

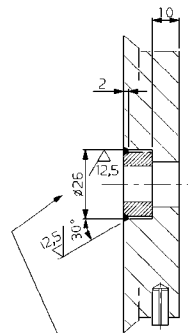
3a,b,c. Borttagning av plug.
Removal of plug.

3a. Uborrning av brottskruv.
Uddrilling of crack-bolt.



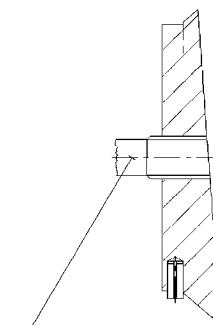
OBS! Det lilla centreringshålet i skruvskallens centrum.
Tillse att borret går rakt och att borrhjulet innehålls.
When drilling, observe the centre-hole and drilling depth.

3b. Bortvarvning av skruvskalle.
Upturning of crack-bolt head.



Svarta inte djupare än att skruvskallen lossnar.
Don't turn deeper than loosening crack-bolt head.

3c. Borttagning av gängad skruvdel.
Removal of threaded screw part.



Kvartsittande del av brottskruv uråtgås.
Threaded screw part to be removed.

4. Återinsättning av plugg.
Refitting plugs.

Vid återinsättning av demonterade pluggar tillses att de ligger jäms med blodytan.
Nya brottskravar, det nr 3, som skall finnas som reserv ombord på fartyget, användes.

Det. nr 4 är inte reservdel.

F.ö. förfäres enl. anvisning 2a,b,c.
"Fastsättning av plug utföres vid varv."

When refitting dismantled plugs check that the plugs are flush to blade surface.
Use new crack-bolts, item no 3, to be kept onboard the vessel as spare part.

Item no 4 is not spare part.

Otherwise to be made according to 2a,b,c.
"Fastening of plug to be carried out at the shipyard."

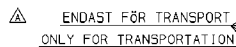
Max. blodtjocklek: 130
Max. blade thickness: 130

Drilling of Liftinghole	Borrn. av Lyfthål och				
Protecting sleeve	05	1 Skyddshylsa	144113A		
Screw	4	1 6K.HÅLSKR. M16x130-8.8	1504762		
Crack-bolt	3	1 Brottskruv	518926B	Avesta	248 SV
Plug	02	1 Lyfthålsplugg	144116A	Avesta	248 SV
Plug	01	1 Lyfthålsplugg	144115A	Avesta	248 SV

Drilling of Liftinghole	Borrn. av Lyfthål och				
Protecting sleeve	05	1 Skyddshylsa	144113A		
Screw	4	1 6K.HÅLSKR. M16x130-8.8	1504762		
Crack-bolt	3	1 Brottskruv	518926B	Avesta	248 SV
Plug	02	1 Lyfthålsplugg	144116A	Avesta	248 SV
Plug	01	1 Lyfthålsplugg	144115A	Avesta	248 SV

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Drilling of Liftinghole	Borrn. av Lyfthål och				
Protecting sleeve	05	1 Skyddshylsa	144113A		
Screw	4	1 6K.HÅLSKR. M16x130-8.8	1504762		
Crack-bolt	3	1 Brottskruv	518926B	Avesta	248 SV
Plug	02	1 Lyfthålsplugg	144116A	Avesta	248 SV
Plug	01	1 Lyfthålsplugg	144115A	Avesta	248 SV

AF

OD-BOX DATA
STROKE=175mm
WEIGHT=50kg
MAX OIL FLOW=50L/min

PROVING ENLIGHT QI-02-133-20
TESTING ACCORDING TO QI 02 133 20

DB

8

1

7 ✓

6

1

5

1

4

1

1

1

2

1

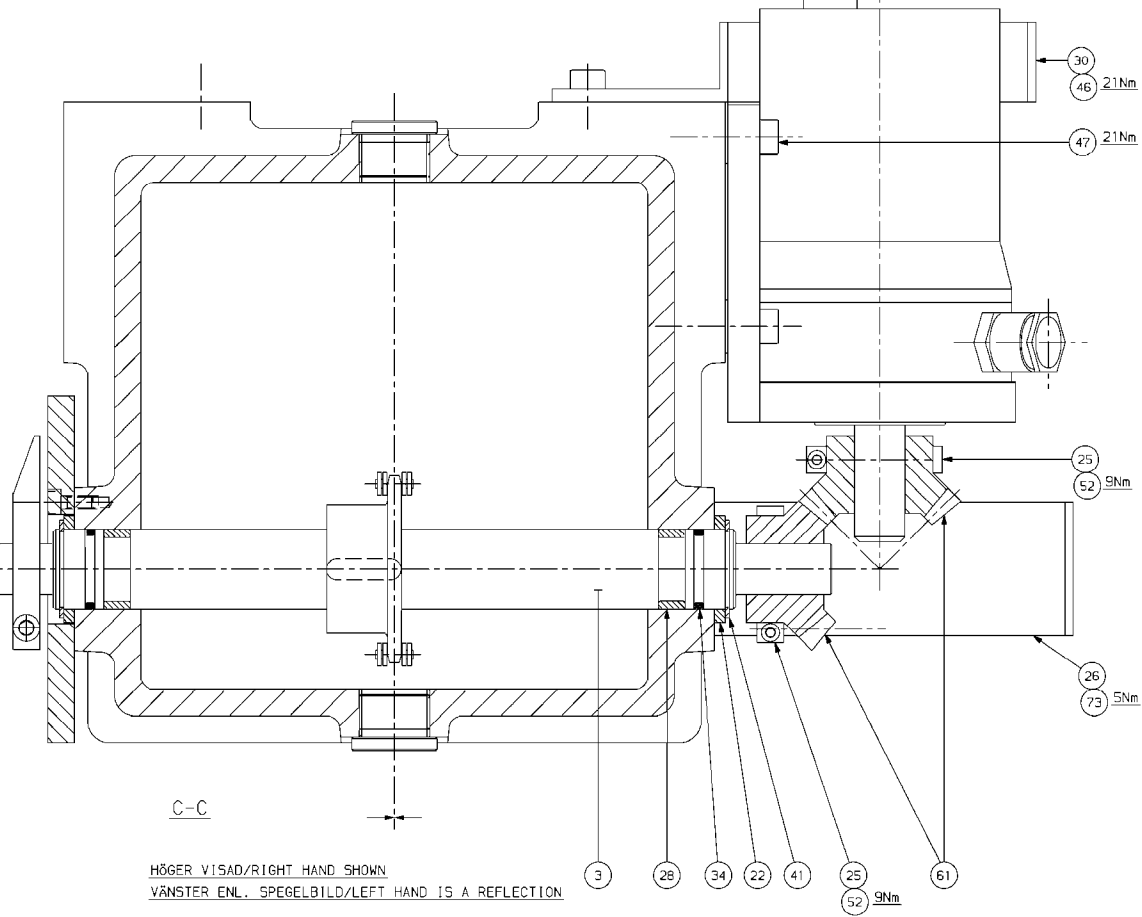
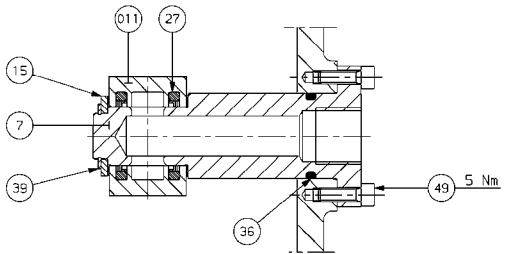
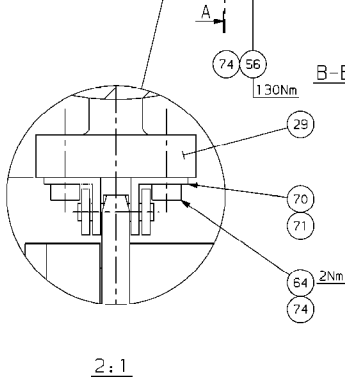
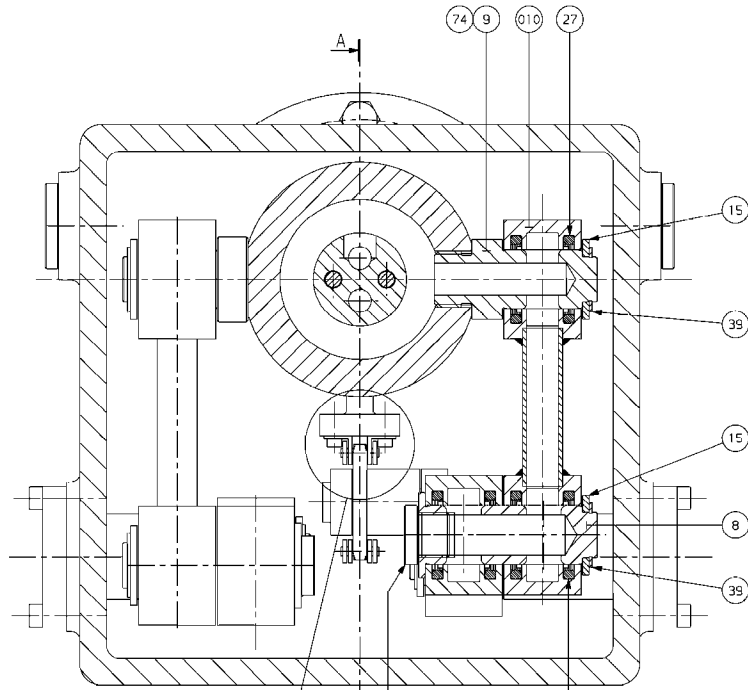
A

Blad Sheet	Utf. Design
A	
B	
C	
D	
E	
F	
G	
H	
K	

Tilläggs måttavvikelse för tolerans ej direkt utsett på beskrivande detalj, en 300 715 Högst enligt totalt mått. För rullningens fall, för och vinkel, alla mått 300 715 Högst enligt specifik standard. Nothing tolerances for linear dimensions unless otherwise specified. For right and curves service and original measurements, 300 715 Average according to separate standard should be followed.

Basmått Basic size	Måttav- vikelse Toler- ances	Basmått Basic size	Måttav- vikelse Toler- ances
- 3	±0,1	(1000) - 2000	±1,2
(3) - 6	±0,1	(2000) - 4000	±2
(6) - 30	±0,2	(4000) - 6000	±3
(30) - 120	±0,3	(6000) - 12000	±4
(120) - 315	±0,5	(12000) - 16000	±5
(315) - 1000	±0,6	(16000) - 20000	±6

Ändr. Redig. Kon. Modifikation efter. Datum. Utgåva. Godk. Approved.



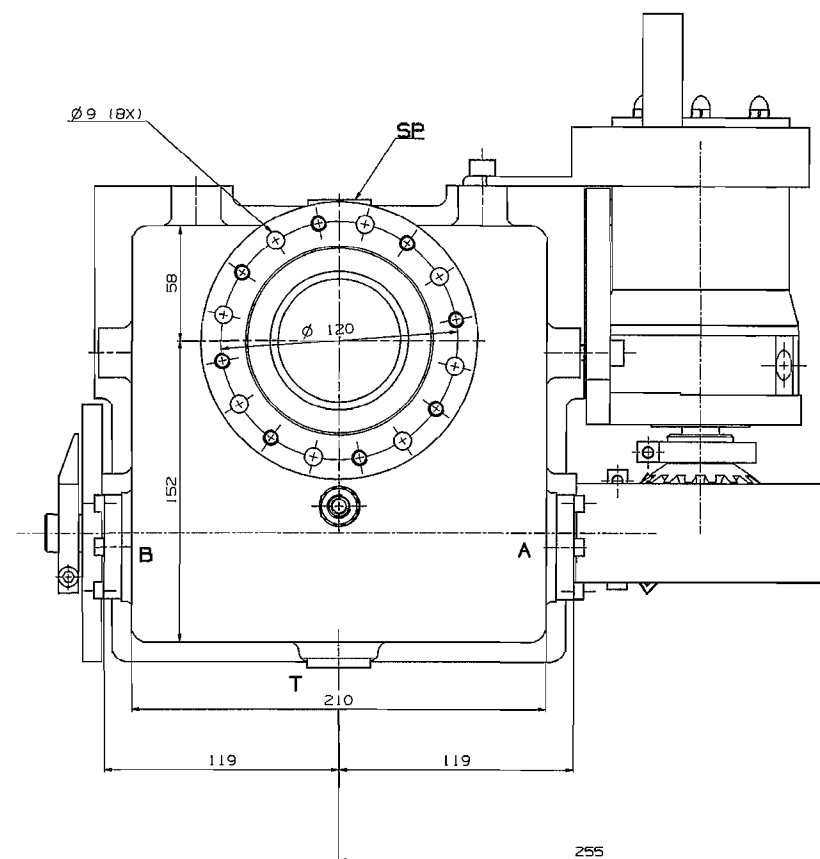
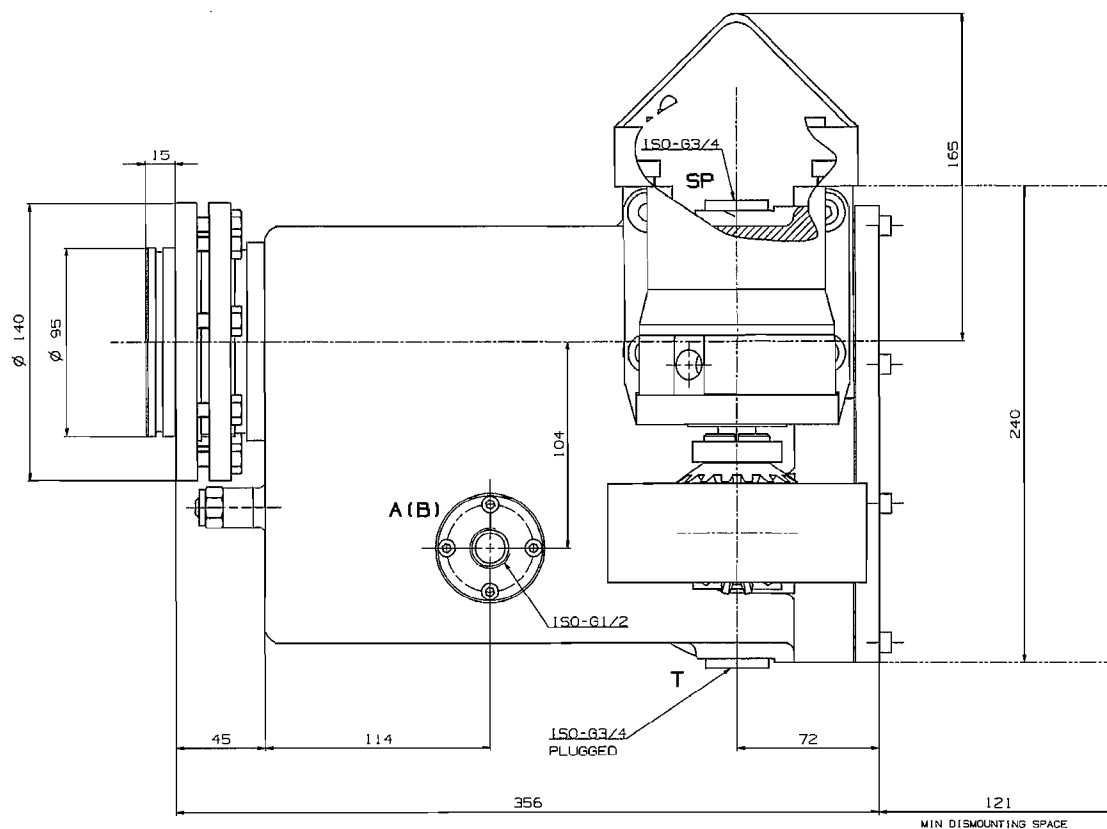
HÖGER VISAD/RIGHT HAND SHOWN
VÄNSTER ENL. SPEGELBILD/LEFT HAND IS A REFLECTION

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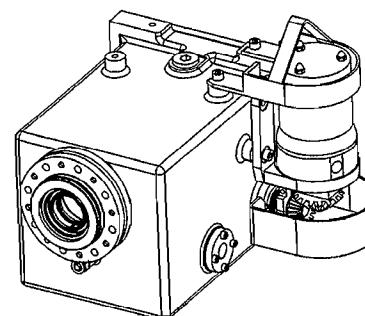
Det. nr. Item No.	Ändr. Rev.	Benämning Description	Referens Reference	Material Material	Anmärkning Remarks
Ändrings Plan			Best. nr./Prod. nr. or Order No./Prod. No.		Stk. Vikt Qty. Weight kg
Utgåva Drawn	Gök	Ändr. Checked	Godk. Approved	LL	Yttextur enligt 300 672 R _a 3,2 µm Surface texture
 KAMEWA SWEDEN			TO-BOX 35 FA - OD-BOX 35 FA - SAMMANSTÄLLNING ASSEMBLY		
Skala Scale 1:1 Blad Sheet 2			Skala Scale 1:1 Blad Sheet 3		
214000			A		

AA

A



DRY WEIGHT APPROX. 63 KG





R-R AB'S INFO CLASS LIMITED	ACCESS LIST R-R AB
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ROLLS-ROYCE AG	

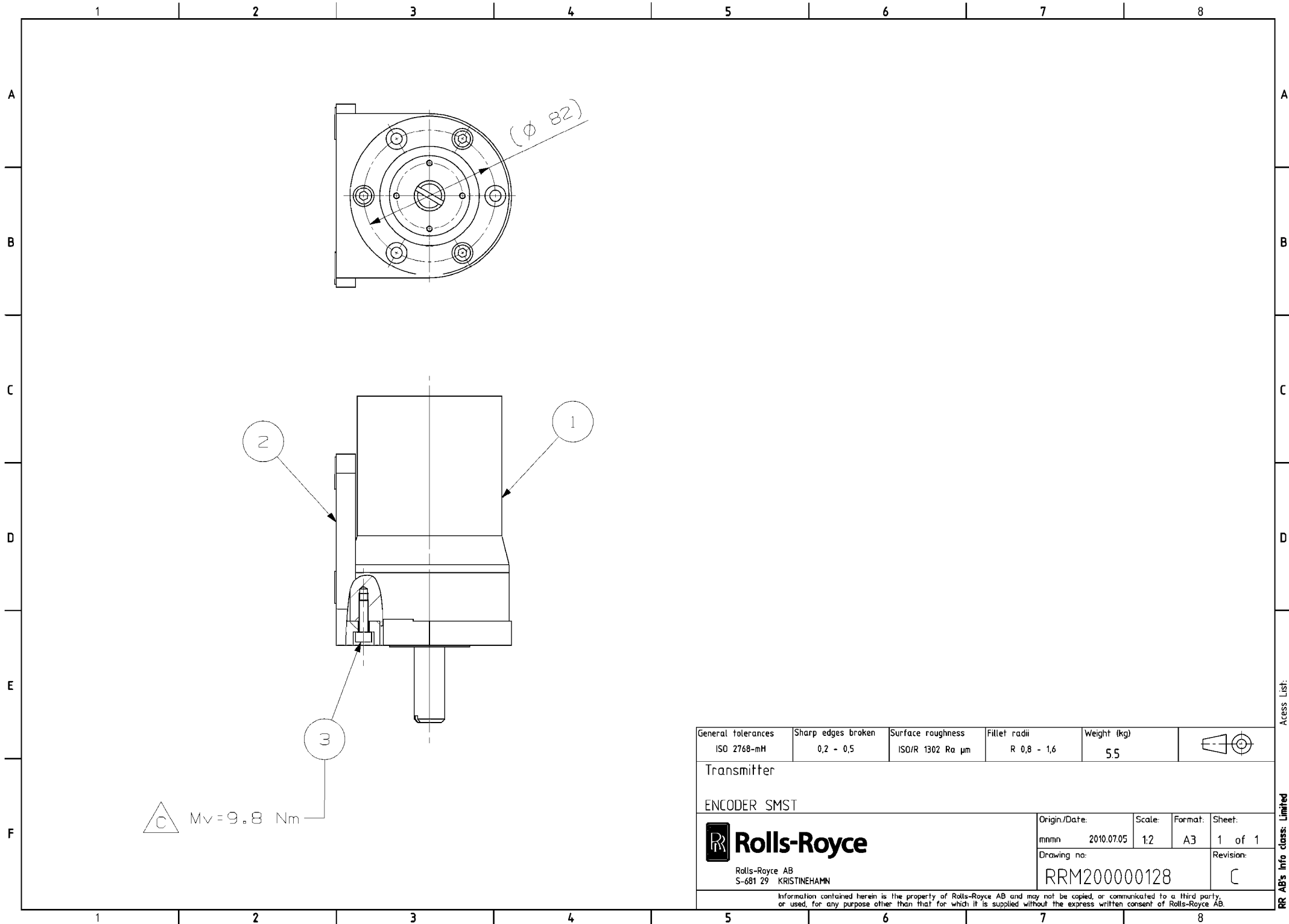
DESCRIPTION	ITEM NO.	QC OF	SHEET DESCRIPTION	REFERENCE	MATERIAL/REMARK
	55-150	2768	MM SHARP EDGES BROKEN 0.2-0.5	PLANT	
	SURFACE ROUGHNESS	SS-150	1302	QC	µm
			FILLET RADIUS	R 0.8-1.6	
	T.O.:- BOX Ø 35 FA			PREVIOUS DRG.	CODE
	O.D.:- BOX			WEIGHT KG	DATE
	DIMENSIONS/ROUTING			SCALE	080714
	DIMENSION DRAWING			1:1.3	MADE BY
				CHECKED	APPROVED
				ERK--	Ans--
				SHEET OF	1/1
				ROLLS-ROYCE AB	CRISTINA HANSEN
				SKETCH	
					154903

[illegible]

HEX HEAD SCREW	2	2	6K.SKRUV M6x16	ISO4017	A4-80 2343
LINK ARM, BLANK	1	1	LINK ARM, XMNE	21/741A	(1.44701
DESCRIPTION	ITEM NO.	QTY	SWEDISH DESCRIPTION	REFERENCE	MATERIAL/REMARK

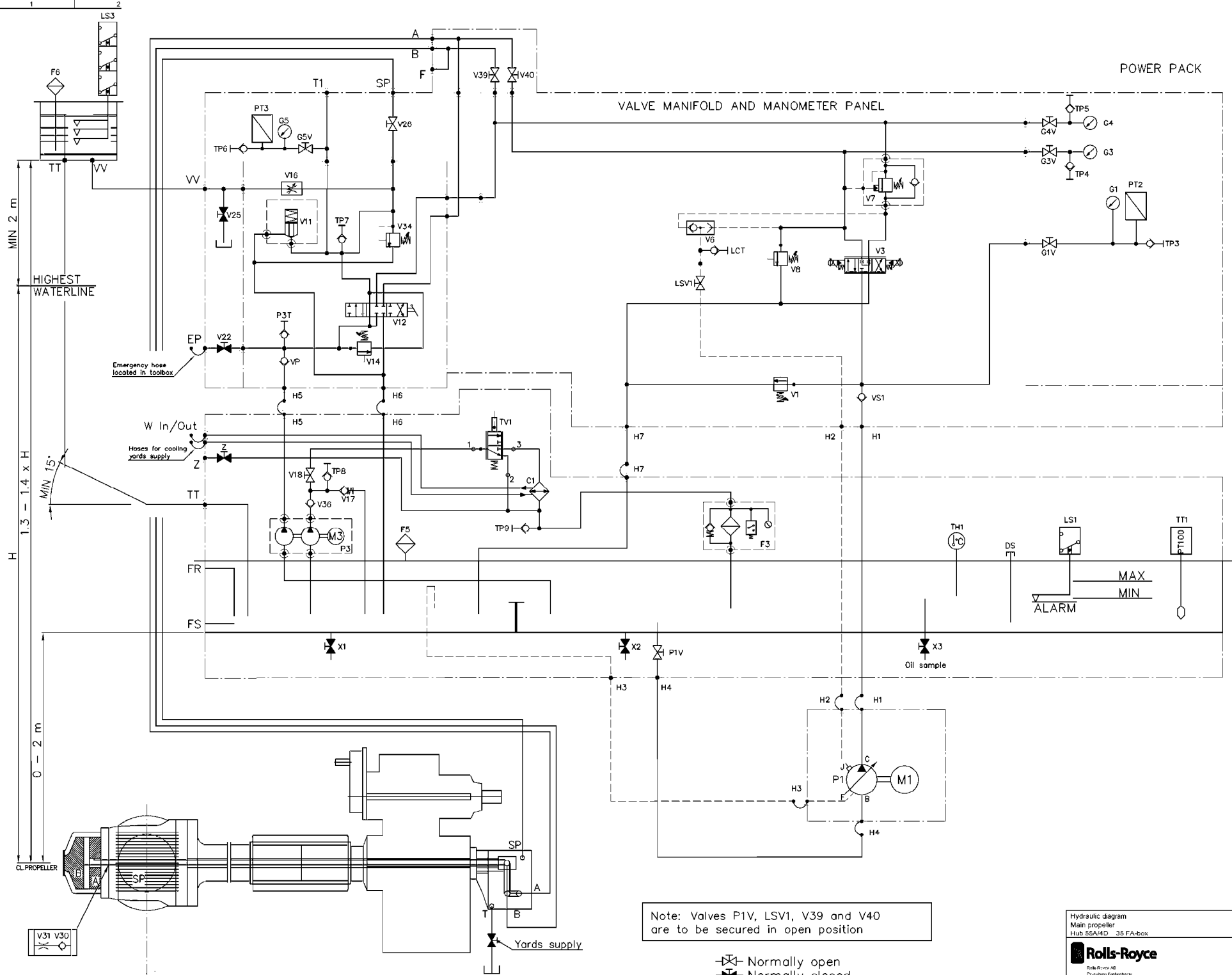
GENERAL TOLERANCES SS-150 2768-m 0.2-0.5		SHARP EDGES BROKEN 0.2-0.5		MOUNT	
SURFACE ROUGHNESS SS-150 1302 Ra µm		FILLET RADI R 0.6-1.6		PREVIOUS DRG. CODE	
45 S3		WEIGHT kg		DATE 07.12.2011	
LANKARM, BEARBETTING		SCALE 1:1		MADE BY J	
LINK ARM, MACHINING		CHECKED Enl		APPROVED Tr	
ROLLS-ROYCE AB KRISTINEHAMN SWEDEN		DRYLY I		  217740	

RR AB'S INFO CLASS	ACCESS LIST
Restricted	RR AB
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	ROLLS-ROYCE AB



Access List:

RR AB's Info class: Limited



Note: Valves P1V, LSV1, V39 and V40 are to be secured in open position

Normally open
 Normally closed

Hydraulic diagram		2. Hand		3. Hand	
Main propeller		Hub 55A/4D		35 FA-box	
Rolls-Royce AB		Rolls-Royce AB		Rolls-Royce AB	
2015-04-26		2015-04-26		2015-04-26	
DMN200000689		D		D	

A	List of components	
	C1	Cooler
	DS	Dip stick
	F3	Oil circulation filter
	F5	Air breather filter main tank
	F6	Air breather filter gravity tank
B	G1	Pressure gauge system pressure
	G1V	Shut off valve
	G3	Pressure gauge conn A astern pitch
	G3V	Shut off valve
	G4	Pressure gauge conn B ahead pitch
	G4V	Shut off valve
	G5	Pressure gauge static pressure
C	G5V	Shut off valve
	LCT	Test point
	LS1	Level switch main tank
	LS3	Level switch gravity tank
	LSV1	Shut off valve, load sensing line pump P1
	P1	Pump unit 1
D	P1V	Shut off valve, suction line pump P1
	P3	Static pressure / cooling filtration pump
	P3T	Test point
	PT2	Pressure transmitter system pressure
	PT3	Pressure transmitter static pressure
	TH1	Thermometer main tank
	TP3-TP9	Test point
E	TT1	Temperature sensor main tank
	TV1	Temperature control valve
	V1	Safety valve
	V3	Proportional control valve
	V6	Shuttle valve
	V7	Counter balance valve
	V8	Pressure relief valve (astern manoeuvre)
	V11	Pressure valve for static pressure
F	V12	Selector valve for emergency control
	V14	Pressure relief valve for emergency control
	V16	Throttle valve
	V17	Pressure valve for by-pass filter
	V18	Shut off valve
	V22	Shut off valve
G	V25	Shut off valve
	V26	Shut off valve
	V30	Check valve
	V31	Nozzle
	V34	Pressure relief valve
	V36	Check valve
	V39	Shut off valve
H	V40	Shut off valve
	VS1	Check valve
	VP	Check valve
	X1	Shut off valve
	X2	Shut off valve
	X3	Shut off valve (oil sample)
I	Z	Shut off valve
J		
K		
L		

Pressure valves setting values (MPa)		
V1	13	(Safety valve)
PR	12	(Pressure regulator, pump)
LSR	2	(Load sensing regulator, pump)
V7	15,5	(Counter balance valve)
V8	6	
V11	0,15	
V14	6	
V17	0,5	
V34	0,4	

OD-Box connections		
A	ISO G1/2"	
B	ISO G1/2"	
SP	ISO G3/4"	
T	ISO G3/4"	

External hoses (Yard supply)		
Location	Inner dia. min	Design press. (MPa)
H1 to H1	3/4"	13
H2 to H2	1/4"	13
H3 to H3	1/2"	0,6
H4 to H4	1 1/4"	0,6
H5 to H5	1/2"	6
H6 to H6	1"	0,6
H7 to H7	1"	0,6

External tube (yard supply)				
Location	Material	Inner dia. min (mm)	Thickness min (mm)	Design press. (MPa)
A to A	Steel	25	2	13
B to B	Steel	25	2	13
SP to SP	Steel	20	2	0,6
T	Steel	20	2	0,6
VV to VV	Steel	16	1,8	0,6
TT to TT	Steel	40	2	0,6
-	-	-	-	-
-	-	-	-	-
-	-	-	-	-
-	-	-	-	-
-	-	-	-	-
Max tube length=10m, if longer please contact RR Recommended tube material quality acc. to St 37.4 acc. to DIN 2391 C and DIN 1630 Min. tubewall thickness acc. to LRS regulations part 5 chapl. 12 table 12.2.4				

Hydraulic system

Main data:
Max working pressure 13 MPa (pitch setting system) (Design pressure)
Max oil flow 35 lit/min, Total oil volume 160 lit
Calculated pitch setting time 14 sec. with one pumpunit in service

Hydraulic power pack

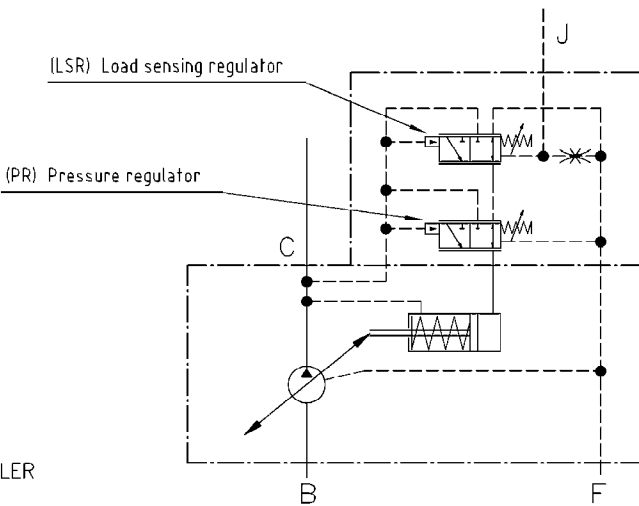
Pump unit P1
Load sensing variable piston pump, Vickers type PVM020
Capacity 35 lit/min at 1750 RPM

El-motor P1
Mez type 7BA132M04, 8,6kW at 1750 RPM, 600V, 60Hz, 3 Phases
Full load current 10,1 A, Starting current 68 A,

Pump unit P3
Gera double pump, Settima DG33 010 + 006
Capacity 17 + 10 lit/min at 1720 RPM

El-motor P3
Mez type 7AA90L04, 1,8 kW at 1720 RPM, 600V, 60Hz, 3 Phases
Full load current 2,3 A, Starting current 12 A,

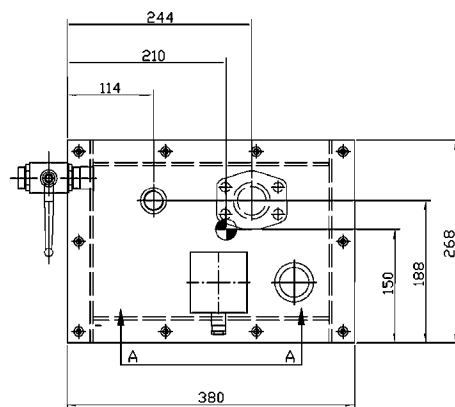
Cooler C1
Type H8A-IG16-9, Cooling capacity 3 kW, Cooling water req. 0.6 m3/h
Sea water at max 32 °C, dp water 5 kPa



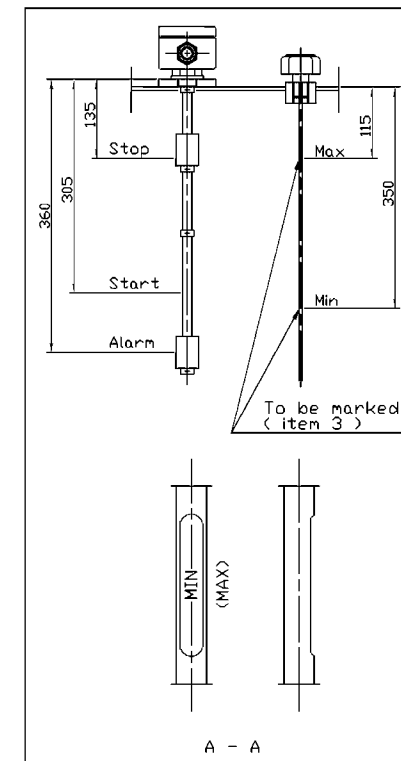
LOAD SENSING VARIABLE DISPLACEMENT PISTON PUMP


NOTE: THERE SHOULD ALWAYS BE FLEXIBLE HOSES ATTACHED TO THE COOLER

NOTE: OIL ALWAYS TO BE FILLED BY USING CONNECTION Z



Total weight incl. oil about 42 kg.
Total weight excl. oil about 25 kg.
"VV" gravity tank pressure ISO G 3/4.
"TT" overflow tube SAE 1 1/2".



8	-	Colour			See hydraulic diagram	
7	1	Shut-off valve 1/2"	8090-08-08 DN15		Specna	
6	1	O-ring	47,22x3,53		Specna	
5	4	Hex. socket cap screw	M12x45	12,9	ISO 4762	
4	1	Flange for welding	AFS-106ST	48,5x38	Specna	
3	1	Air breather whit dip stick	SES2-M-500		Parker	
2.1	1	Adapter	G8113		Specna	
2	1	Level switch	MS2009-S-Va/Ti-AL22-IM00-L3/3		Barksdale	
1	1	Oil tank 20 lit.	G09179		Specna	
Item	Qty	Description	Reference	Material	Remark	
General tolerances		Sharp edges broken	Surface roughness	Filet radi	Weight (kg)	
ISO 2768-mS		2 - 4,5	ISO/0 1912 Ra µm	R 1,8 - 1,6		

Hydraulic System
Main propeller
Gravity tank 20 lit.

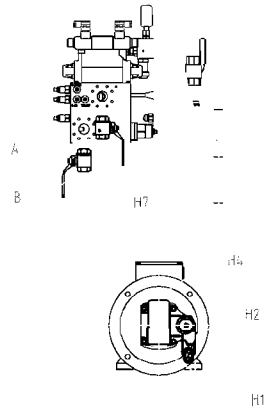


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TAN 2010-10-12	1:5	A2	1 of 1
Drawing no			Revision
RRM200011521			A

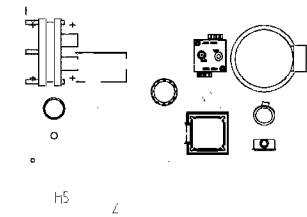
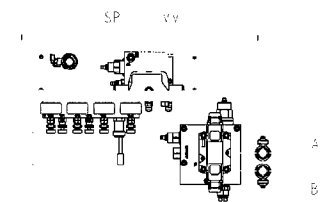
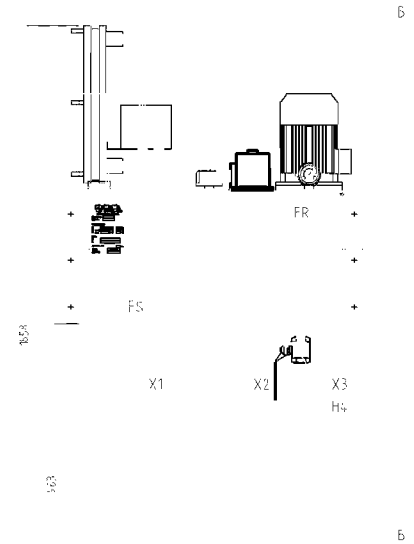
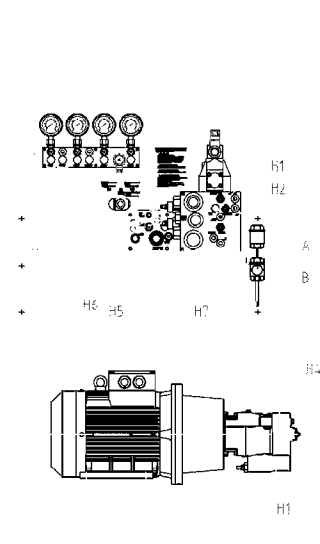
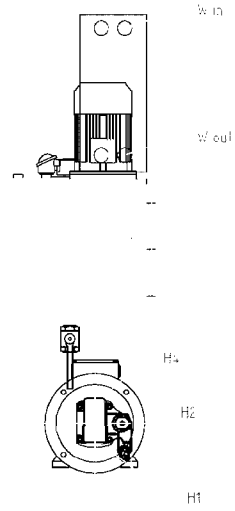
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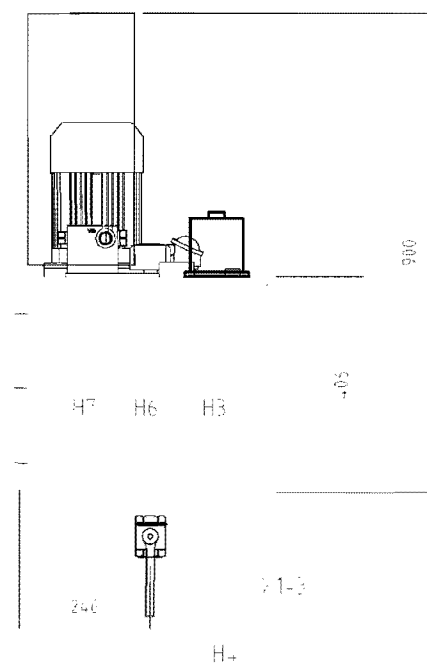
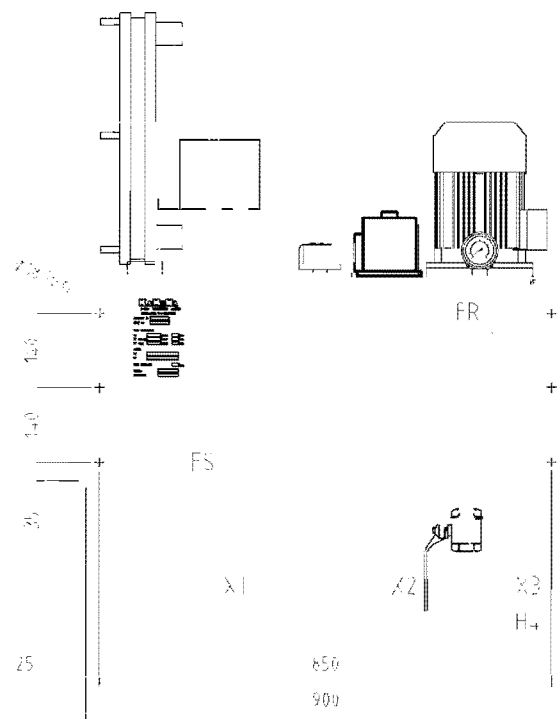
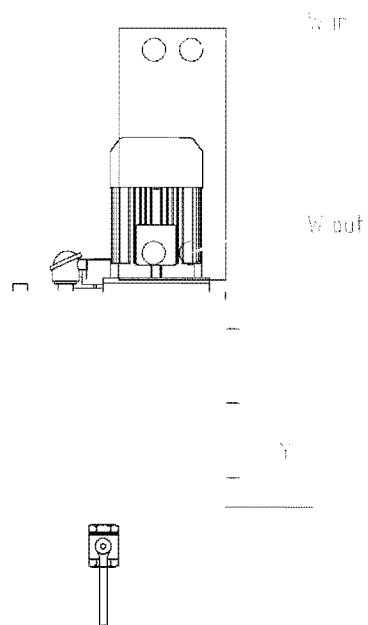
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View A

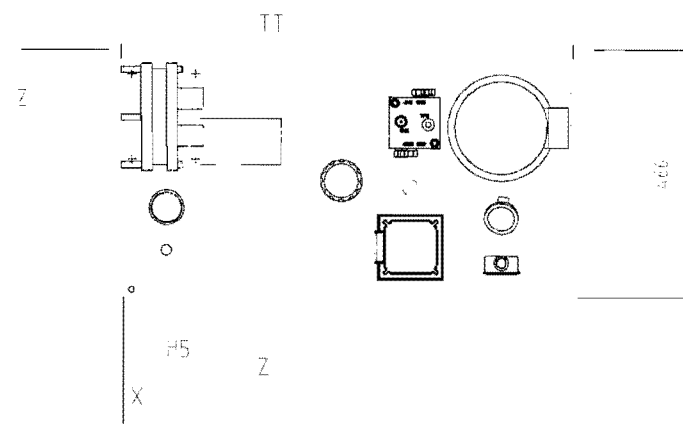


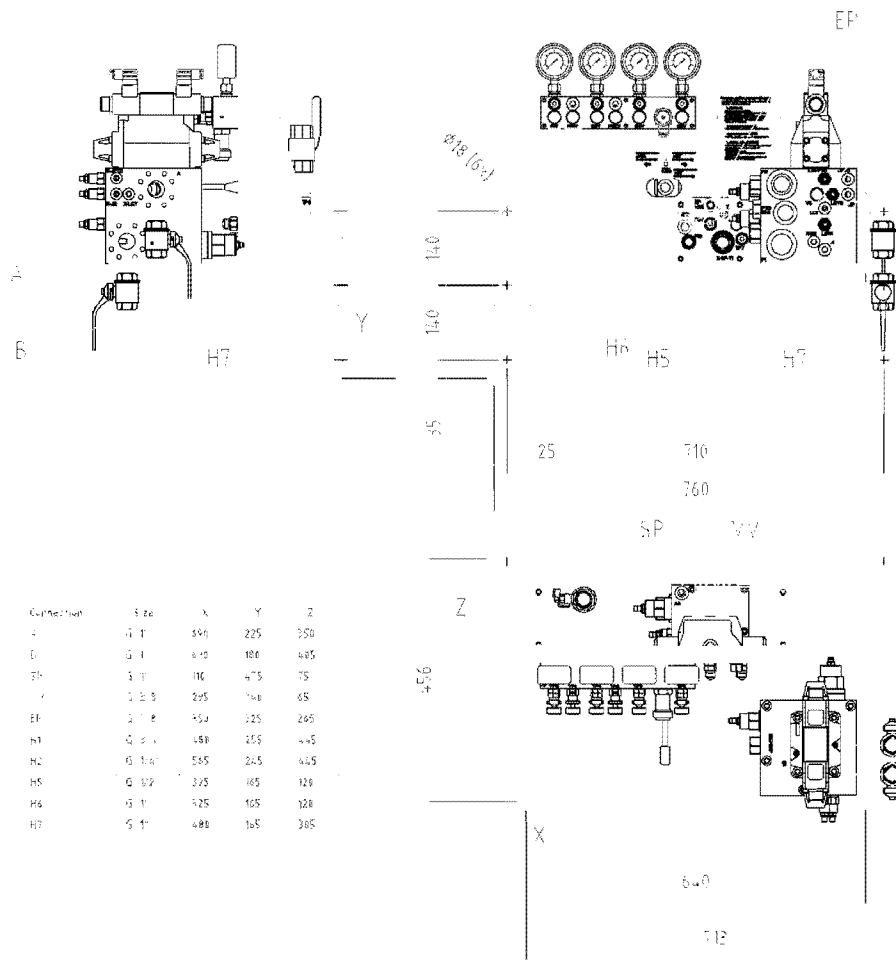
View B



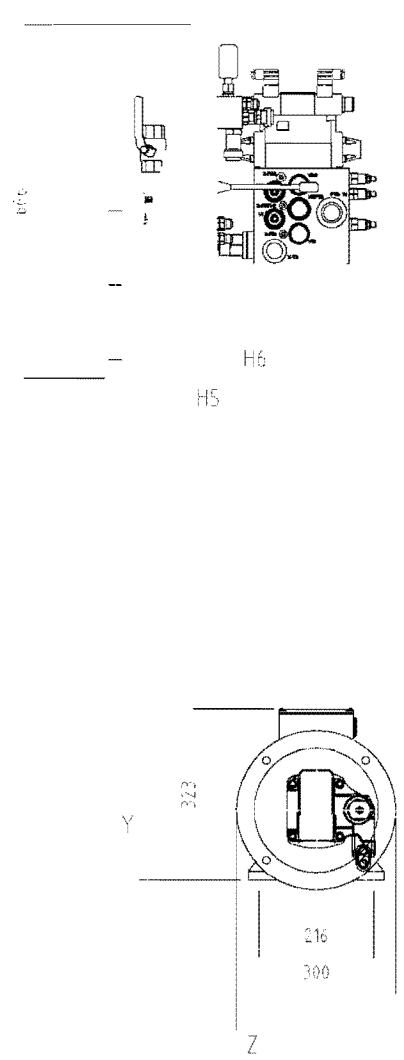


Connection	Size	X	Y	Z
TT	G 2"	85	435	295
CI Water In	G 1 1/2"	150	860	90
CI Water Out	G 1 1/2"	150	480	90
Z	G 3/4"	190	435	490
X1	G 1 1/2"	135	-100	760
X2	G 1 1/2"	485	-100	360
X3	G 1 1/2"	685	-100	360
FS	G 1"	135	55	100
FR	G 1"	745	305	335
H3	G 1/2"	15	745	30
H4	G 1 1/2"	605	-100	245
H5	G 1/2"	60	435	375
H6	G 1"	15	745	165
H7	G 1"	15	745	90

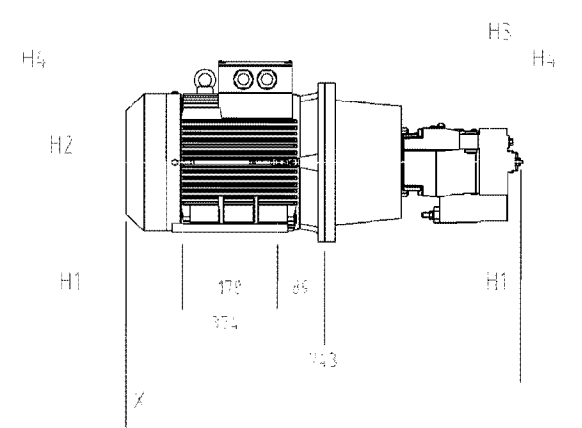


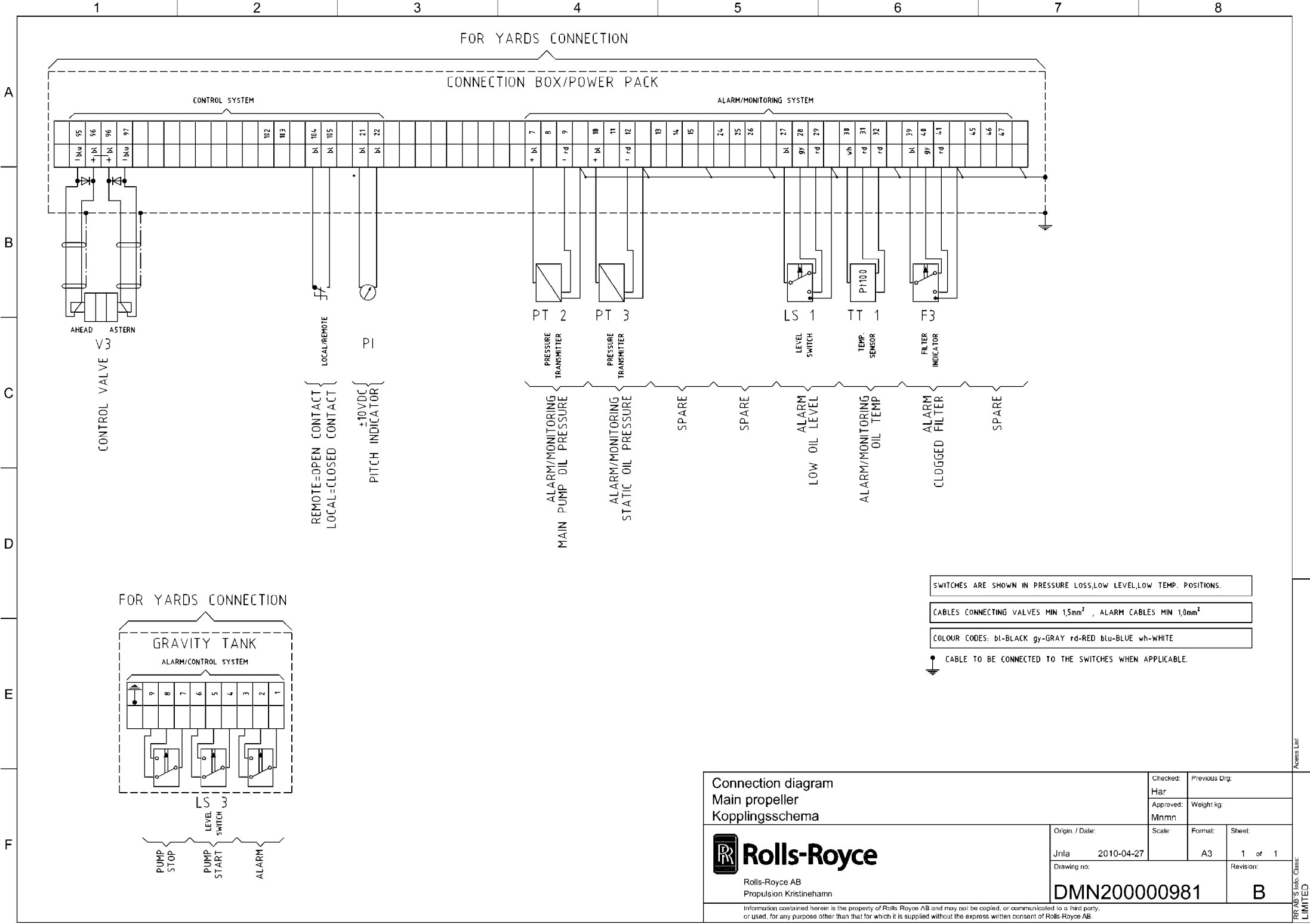


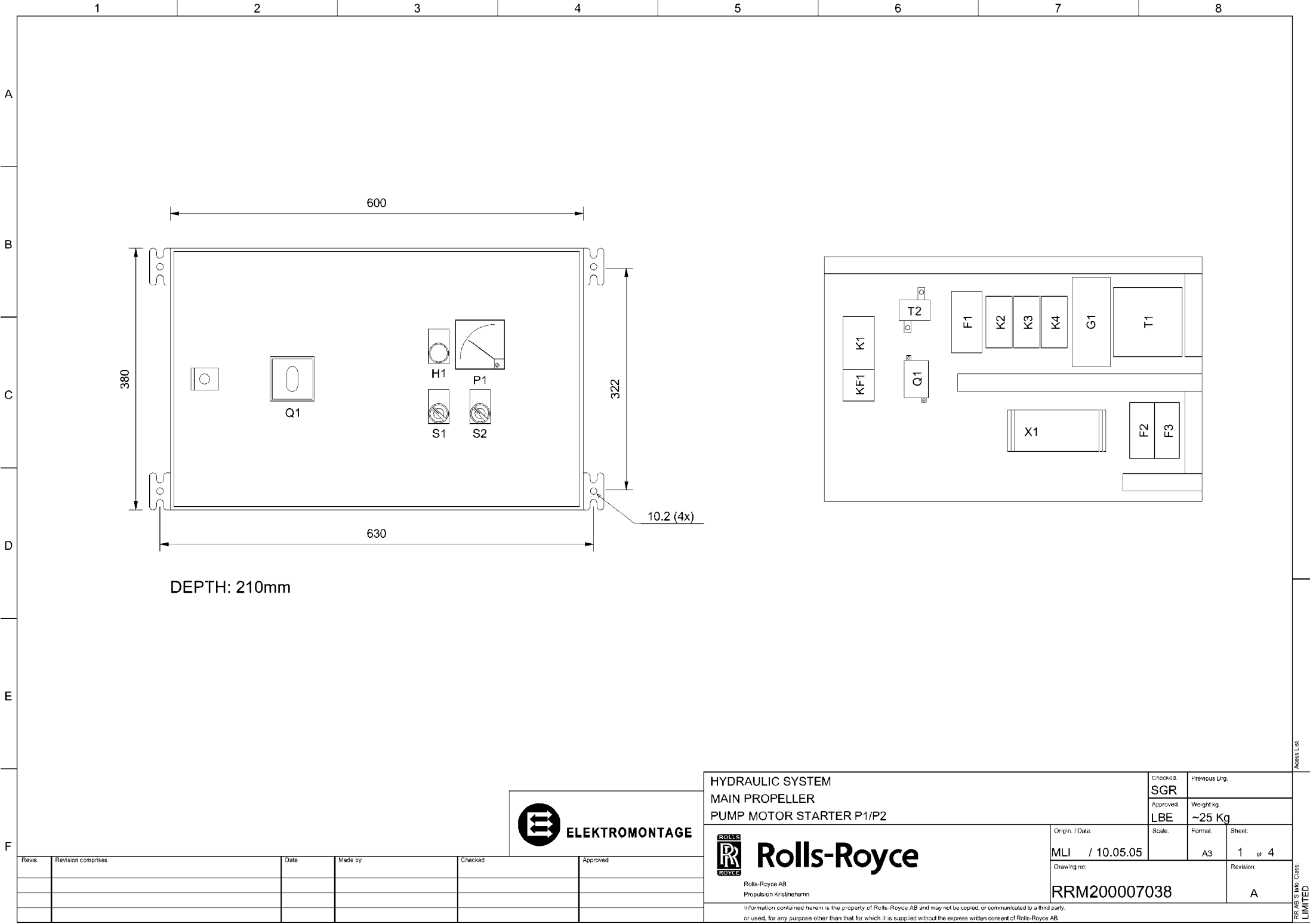
Connection	Size	X	Y	Z
H1	G 1"	580	225	350
H2	G 1"	640	180	405
H3	G 1"	710	475	75
H4	G 1 1/2"	825	740	65
EP	G 1"	580	225	295
H7	G 1"	640	255	445
H2	G 1 1/4"	585	245	445
H5	G 1/2"	325	165	128
H6	G 1"	525	105	128
H7	G 1"	680	165	385



Connection	Size	X	Y	Z
H1	G 1 1/4"	640	70	180
H2	G 1 1/4"	640	90	280
H3	G 1 1/2"	570	200	160
H4	SAE 1 1/4"	498	195	150






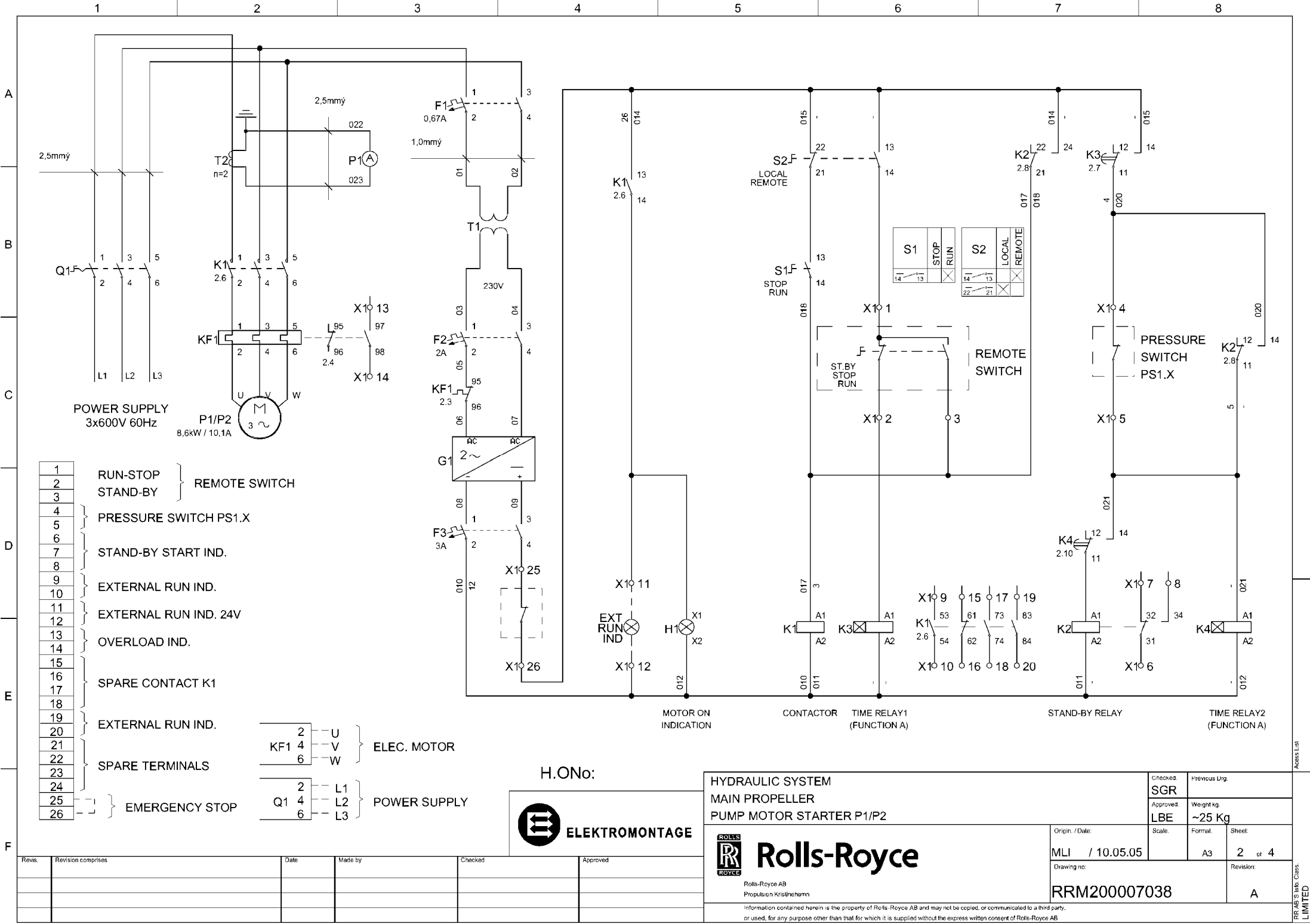


DEPTH: 210mm



HYDRAULIC SYSTEM				Checked: SGR	Previous Usg.			
MAIN PROPELLER				Approved: LBE	Weight kg. ~25 Kg			
PUMP MOTOR STARTER P1/P2				Origin. / Date: MLI / 10.05.05	Scale:	Format: A3	Sheet: 1 of 4	
<div><div><div>Rolls-Royce</div><div>AB</div></div></div> <div>Rolls-Royce AB Propulsion Kristinehamn</div>				Drawing no: RRM200007038			Revision: A	
				Information contained herein is the property of Rolls-Royce AB and may not be copied, or communicated to a third party, or used, for any purpose other than that for which it is supplied without the express written consent of Rolls-Royce AB				


RR AB Style Cass. LIMITED



- | | | |
|----|-----------------------|---------------|
| 1 | RUN-STOP
STAND-BY | REMOTE SWITCH |
| 2 | | |
| 3 | | |
| 4 | PRESSURE SWITCH PS1.X | |
| 5 | | |
| 6 | | |
| 7 | STAND-BY START IND. | |
| 8 | | |
| 9 | | |
| 10 | EXTERNAL RUN IND. | |
| 11 | | |
| 12 | | |
| 13 | EXTERNAL RUN IND. 24V | |
| 14 | | |
| 15 | | |
| 16 | OVERLOAD IND. | |
| 17 | | |
| 18 | | |
| 19 | SPARE CONTACT K1 | |
| 20 | | |
| 21 | | |
| 22 | EXTERNAL RUN IND. | |
| 23 | | |
| 24 | | |
| 25 | SPARE TERMINALS | |
| 26 | | |
| 27 | | |
| 28 | EMERGENCY STOP | |
| 29 | | |
| 30 | | |

- | | | |
|---|-----|--------------|
| 2 | -U | ELEC. MOTOR |
| 4 | -V | |
| 6 | -W | |
| 2 | -L1 | POWER SUPPLY |
| 4 | -L2 | |
| 6 | -L3 | |

H.ONo:

 **ELEKTROMONTAGE**

HYDRAULIC SYSTEM MAIN PROPELLER PUMP MOTOR STARTER P1/P2		Checked: SGR	Previous Urg.
Origin. / Date: MLI / 10.05.05		Approved: LBE	Weight kg. ~25 Kg
Drawing no. RRM200007038		Scale: A3	Sheet: 2 of 4
Revision: A		RR-AS Style Cases LIMITED	

Rolls-Royce AB
Propulsion Kristinehamn

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	1	2	3	4	5	6	7	8
A	Item.	Quant.	Description	Type	Manufacturer	Note		
		1	CABINET 600X380X210	AE1039.500	RITTAL			
		4	WALL BRACKETS	SZ2508/4	RITTAL			
	F1	1	MOTOR CIRCUIT BR. 0.63-1A	GV2RT05	TELEMECANIQUE			
B	F2	1	MINIATURE CIRCUIT BREAKER	C60N 2P C2A	MERLIN GERIN			
	F3	1	MINIATURE CIRCUIT BREKAER	C32H DC 2P C3A	MERLIN GERIN			
	G1	1	POWER SUPPLY 230/24V 3A	CP SNT 70W 24V 3A	WEIDM\$LLER			
	H1	1	LENSE YELLOW LED	ZB4BV053	TELEMECANIQUE			
C	H1	1	YELLOW LED PILOT LIGHT BODY	ZB4BVB5	TELEMECANIQUE			
	K1	1	CONTACTOR 16A 24VDC	LC1D16BD	TELEMECANIQUE			
	K1	1	AUX. CONTACT BLOCK 3NO+1NC	LADN31	TELEMECANIQUE			
	K2	1	RELAY 3-POLE 24VDC	C3A30D24D	RELECO			
D	K2	1	SOCKET FOR 11-PIN RELAY	S3MP	RELECO			
	K3	1	MULTIFUNCTIONAL TIME RELAY	PU2R3	GROUZET			
	K3	1	SOCKET FOR 11-PIN RELAY	S3MP	RELECO			
	K4	1	MULTIFUNCTIONAL TIME RELAY	PU2R3	GROUZET			
E	K4	1	SOCKET FOR 11-PIN RELAY	S3MP	RELECO			
	KF1	1	OVERCURRENT RELAY 12-18A	LRD21	TELEMECANIQUE			
	P1	1	AMMETER	IQ72 25/5A	CEWE INSTRUMENT			
	Q1	1	LOAD BREAK SWITCH 40A 3P	OT 40 F3	ABB CONTROL			
F	Q1	1	HANDLE	OHBS2AJ	ABB CONTROL			
	Q1	1	EXTENDED SHAFT 330mm	OXS6X330	ABB CONTROL			
	S1	1	HANDLE 2-POS, BLACK	ZB4BD2	TELEMECANIQUE			
	S1	1	CONTACT BODY 1NO	ZB4BZ101	TELEMECANIQUE			
G	S2	1	HANDLE 2-POS, BLACK	ZB4BD2	TELEMECANIQUE			
	S2	1	CONTACT BODY 1NO	ZB4BZ101	TELEMECANIQUE			
	S2	2	COMPLEMENTARY BLOCK 1NC	ZBE102	TELEMECANIQUE			
					HYDRAULIC SYSTEM MAIN PROPELLER PUMP MOTOR STARTER P1/P2			
					Checked: SGR Approved: LBE Weight kg: ~25 Kg			
					Origin: / Date: MLI / 10.05.05 Scale: Format: A3 Sheet: 3 of 4			
					Drawing no: RRM200007038 Revision: A			
					Information contained herein is the property of Rolls-Royce AB and may not be copied, or communicated to a third party, or used, for any purpose other than that for which it is supplied without the express written consent of Rolls-Royce AB.			
					Access List			
					LIMITED			

	1	2	3	4	5	6	7	8
A	Item.	Quant.	Description	Type	Manufacturer	Note		
	T1	1	TRANSFORMER 690/230,24V	SUS120B 375+25VA	NORATEL			
	T2	1	CURRENT TRANSFORMER	MAK 50/5A 45/14	CEWE INSTRUMENT			
	X1	26	TERMINAL 2,5mm	WDU 2,5	WEIDM\$LLER			
B								
C								
D								
E								
F								

Revis.

Revision comprises

Date

Made by

Checked

Approved

ELEKTROMONTAGE

HYDRAULIC SYSTEM
MAIN PROPELLER
PUMP MOTOR STARTER P1/P2

ROLLS
ROYCE

Rolls-Royce AB
Propulsion K/Sinehamm

Rolls-Royce

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Origin. / Date:
MLI / 10.05.05

Drawing no:
RRM200007038

Checked:
SGR

Approved:
LBE

Scale:

Previous Urg.

Weight kg.
~25 Kg

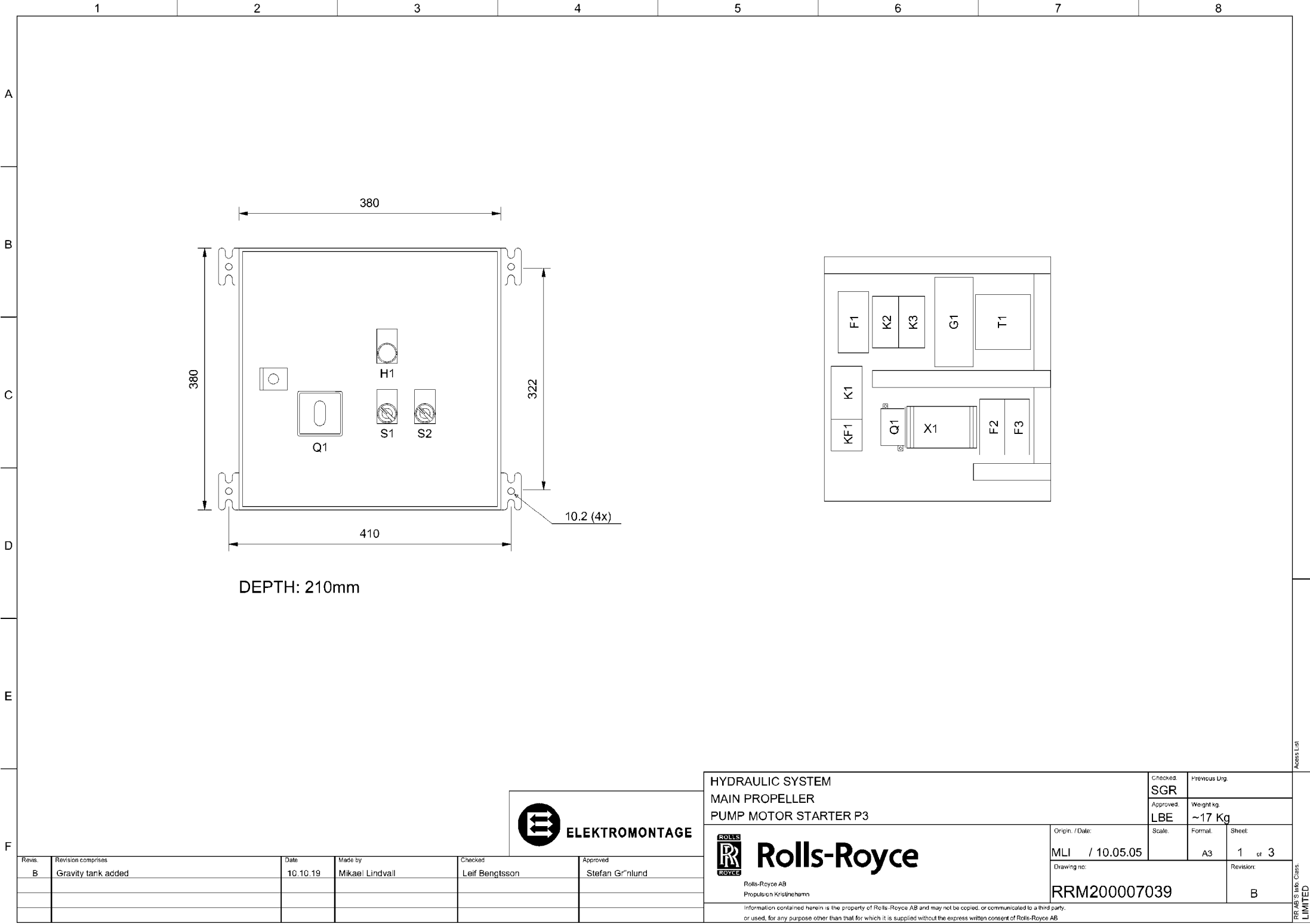
Format:
A3

Sheet:
4 of 4

Revision:
A

Access List

RR-AB Ship Case. LIMITED



A

B

C

D

E

F

DEPTH: 210mm



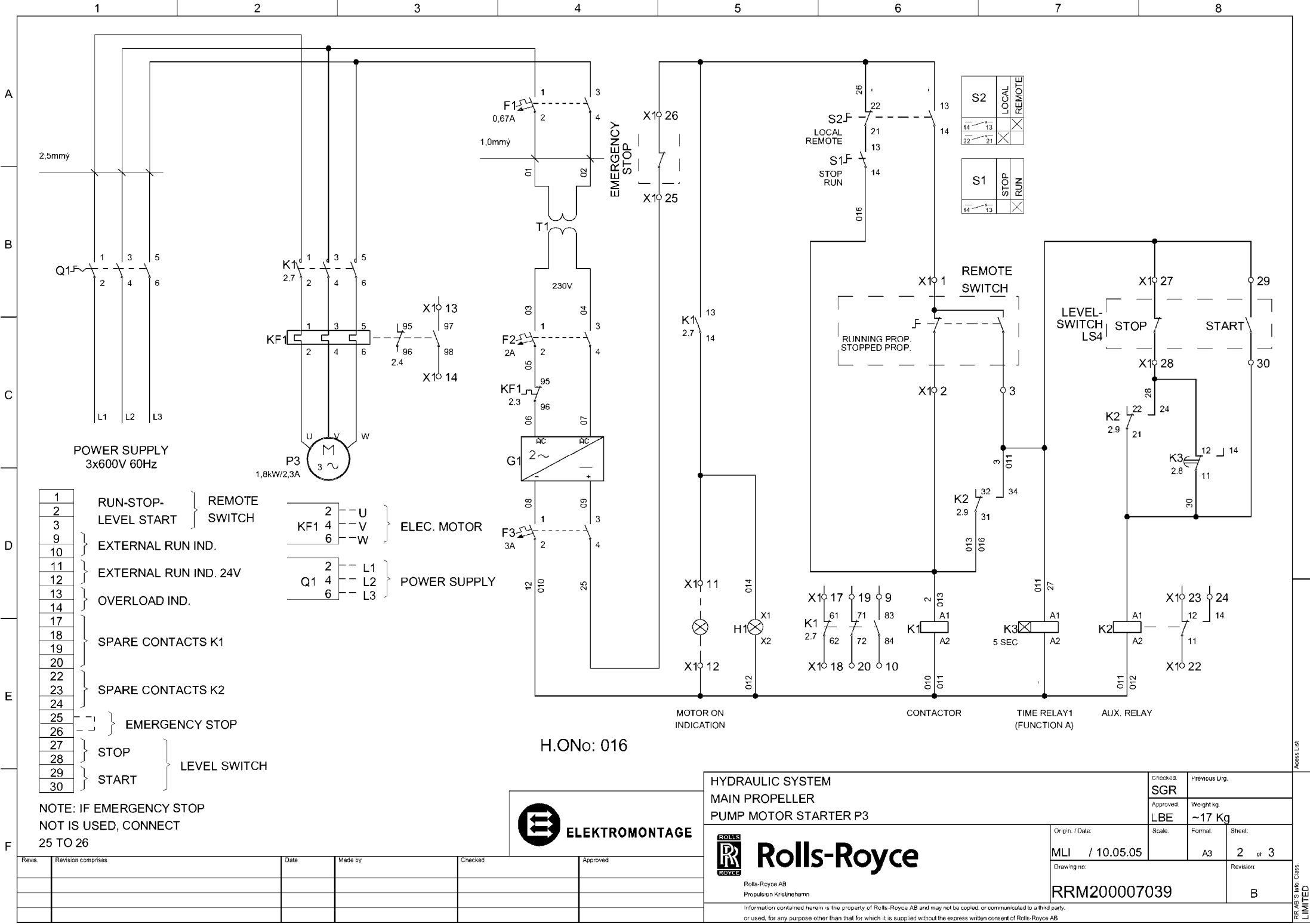
Revis.	Revision comprises	Date	Made by	Checked	Approved
B	Gravity tank added	10.10.19	Mikael Lindvall	Leif Bengtsson	Stefan Grönlund

HYDRAULIC SYSTEM MAIN PROPELLER PUMP MOTOR STARTER P3		Checked: SGR	Previous Urg.	
		Approved: LBE	Weight kg. ~17 Kg	
		Scale:	Format: A3	Sheet: 1 of 3
Origin: / Date: MLI / 10.05.05		Drawing no.: RRM200007039		Revision: B
 Rolls-Royce AB Propulsion Kristinehamn		Information contained herein is the property of Rolls-Royce AB and may not be copied, or communicated to a third party, or used, for any purpose other than that for which it is supplied without the express written consent of Rolls-Royce AB		

Access List

RR-AB Ship Cases

LIMITED



- | | | |
|----|-------------------------|-----------------|
| 1 | RUN-STOP- | } REMOTE SWITCH |
| 2 | LEVEL START | |
| 3 | | |
| 9 | } EXTERNAL RUN IND. | |
| 10 | | |
| 11 | | |
| 12 | } EXTERNAL RUN IND. 24V | |
| 13 | | |
| 14 | | |
| 17 | } SPARE CONTACTS K1 | |
| 18 | | |
| 19 | | |
| 22 | } SPARE CONTACTS K2 | |
| 23 | | |
| 24 | | |
| 25 | } EMERGENCY STOP | |
| 26 | | |
| 27 | | |
| 28 | } STOP | |
| 29 | | |
| 30 | | |
| | } LEVEL SWITCH | |

NOTE: IF EMERGENCY STOP
NOT IS USED, CONNECT
25 TO 26



ELEKTROMONTAGE

Revis.	Revision comprises	Date	Made by	Checked	Approved

HYDRAULIC SYSTEM
MAIN PROPELLER
PUMP MOTOR STARTER P3



Rolls-Royce

Rolls-Royce AB
Propulsion K/Sineham

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Checked: SGR

Previous Urg.

Approved: LBE

Weight kg. ~17 Kg

Scale: A3

Format: 2

Sheet: of 3

Origin: / Date: MLI / 10.05.05

Drawing no: RRM200007039

Revision: B

Access List

PR-AB Style Cases. LIMITED

	1	2	3	4	5	6	7	8
A	Item.	Quant.	Description	Type	Manufacturer	Note		
		1	CABINET 380x380x210	AE1380.500	RITTAL			
		4	WALL BRACKETS	SZ2508/4	RITTAL			
	F1	1	MOTOR CIRCUIT BR. 0.63-1A	GV2RT05	TELEMECANIQUE			
	F2	1	MINIATURE CIRCUIT BREAKER	C60N 2P C2A	MERLIN GERIN			
B	F3	1	MINIATURE CIRCUIT BREKAER	C60H DC 2P C3A	MERLIN GERIN			
	G1	1	POWER SUPPLY 230/24V 3A	CP SNT 70W 24V 3A	WEIDM\$LLER			
	H1	1	LENSE YELLOW LED	ZB4BV053	TELEMECANIQUE			
	H1	1	YELLOW LED PILOT LIGHT BODY	ZB4BVB5	TELEMECANIQUE			
	K1	1	CONTACTOR 9A 24VDC	LC1D09BD	TELEMECANIQUE			
C	K1	1	AUX. CONTACT BLOCK 2NO+2NC	LADN22	TELEMECANIQUE			
	K2	1	RELAY 3-POLE 24VDC	C3A30D24D	RELECO			
	K2	1	SOCKET FOR 11-PIN RELAY	S3MP	RELECO			
	K3	1	MULTIFUNCTIONAL TIME RELAY	PU2R3	CROUZET			
	K3	1	SOCKET FOR 11-PIN RELAY	S3MP	RELECO			
D	KF1	1	OVERCURRENT RELAY 1,6-2,5A	LRD07	TELEMECANIQUE			
	Q1	1	LOAD BREAK SWITCH 16A 3P	OT16F3	ABB CONTROL			
	Q1	1	HANDLE	QHBS2AJ	ABB CONTROL			
	Q1	1	EXTENDED SHAFT 330mm	OXS6X330	ABB CONTROL			
	S1	1	HANDLE 2-POS. BLACK	ZB4BD2	TELEMECANIQUE			
E	S1	1	CONTACT BODY 1NO	ZB4BZ101	TELEMECANIQUE			
	S2	1	HANDLE 2-POS. BLACK	ZB4BD2	TELEMECANIQUE			
	S2	1	CONTACT BODY 1NO	ZB4BZ101	TELEMECANIQUE			
	S2	1	COMPLEMENTARY BLOCK 1NC	ZBE102	TELEMECANIQUE			
	T1	1	TRANSFORMER 690/230,24V	SUS120B 375+25VA	NORATEL			
	X1	22	TERMINAL 2,5mm	WDU 2,5	WEIDM\$LLER			

Revis.


Revision comprises

Date


Made by

Checked

Approved

ELEKTROMONTAGE

HYDRAULIC SYSTEM
MAIN PROPELLER
PUMP MOTOR STARTER P3

Rolls-Royce

Rolls-Royce AB
Propulsion K/strömehamn

Origin. / Date:
MLI / 10.05.05

Drawing no.
RRM200007039

Checked:
SGR

Approved:
LBE

Previous Urg.

Weight kg.
~17 Kg

Scale:

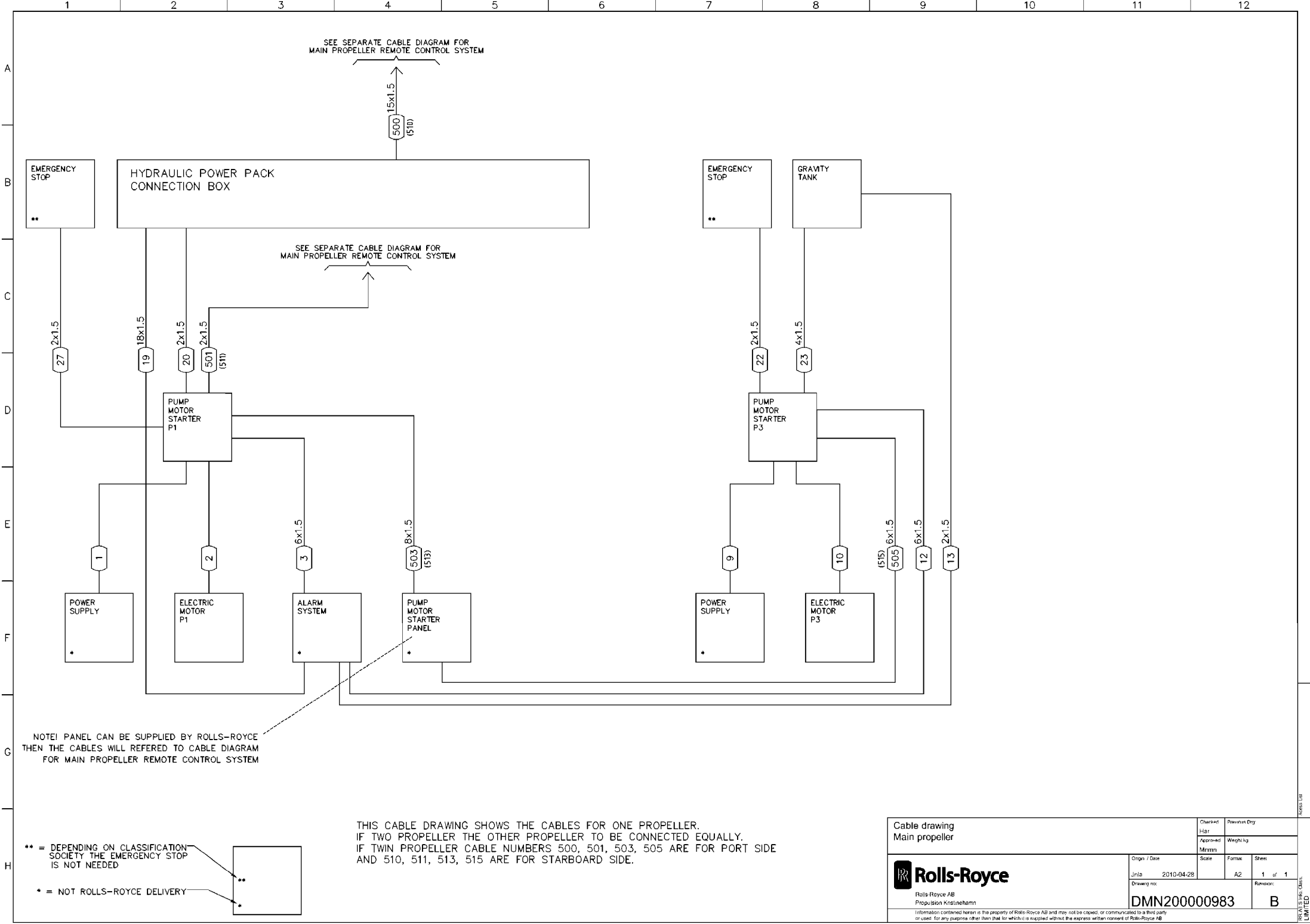
Format:
A3

Sheet:
3 of 3

Revision:
B

Access List

Rolls-Royce AB
Propulsion K/strömehamn
LIMITED




NOTE! PANEL CAN BE SUPPLIED BY ROLLS-ROYCE THEN THE CABLES WILL REFERED TO CABLE DIAGRAM FOR MAIN PROPELLER REMOTE CONTROL SYSTEM

** = DEPENDING ON CLASSIFICATION SOCIETY THE EMERGENCY STOP IS NOT NEEDED

* = NOT ROLLS-ROYCE DELIVERY

THIS CABLE DRAWING SHOWS THE CABLES FOR ONE PROPELLER. IF TWO PROPELLER THE OTHER PROPELLER TO BE CONNECTED EQUALLY. IF TWIN PROPELLER CABLE NUMBERS 500, 501, 503, 505 ARE FOR PORT SIDE AND 510, 511, 513, 515 ARE FOR STARBOARD SIDE.

Cable drawing
Main propeller

**Rolls-Royce**
Rolls-Royce AB
Propulsion Kristinehamn

Origin / Date
Jnlja 2010-04-28
Drawing no:
DMN200000983

Checked
Här
Approved
Mmm

Scale
A2

Format
A2

Sheet
1 of 1
Revision:
B

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REV: AS S-16-00-0001
LIMITED

A

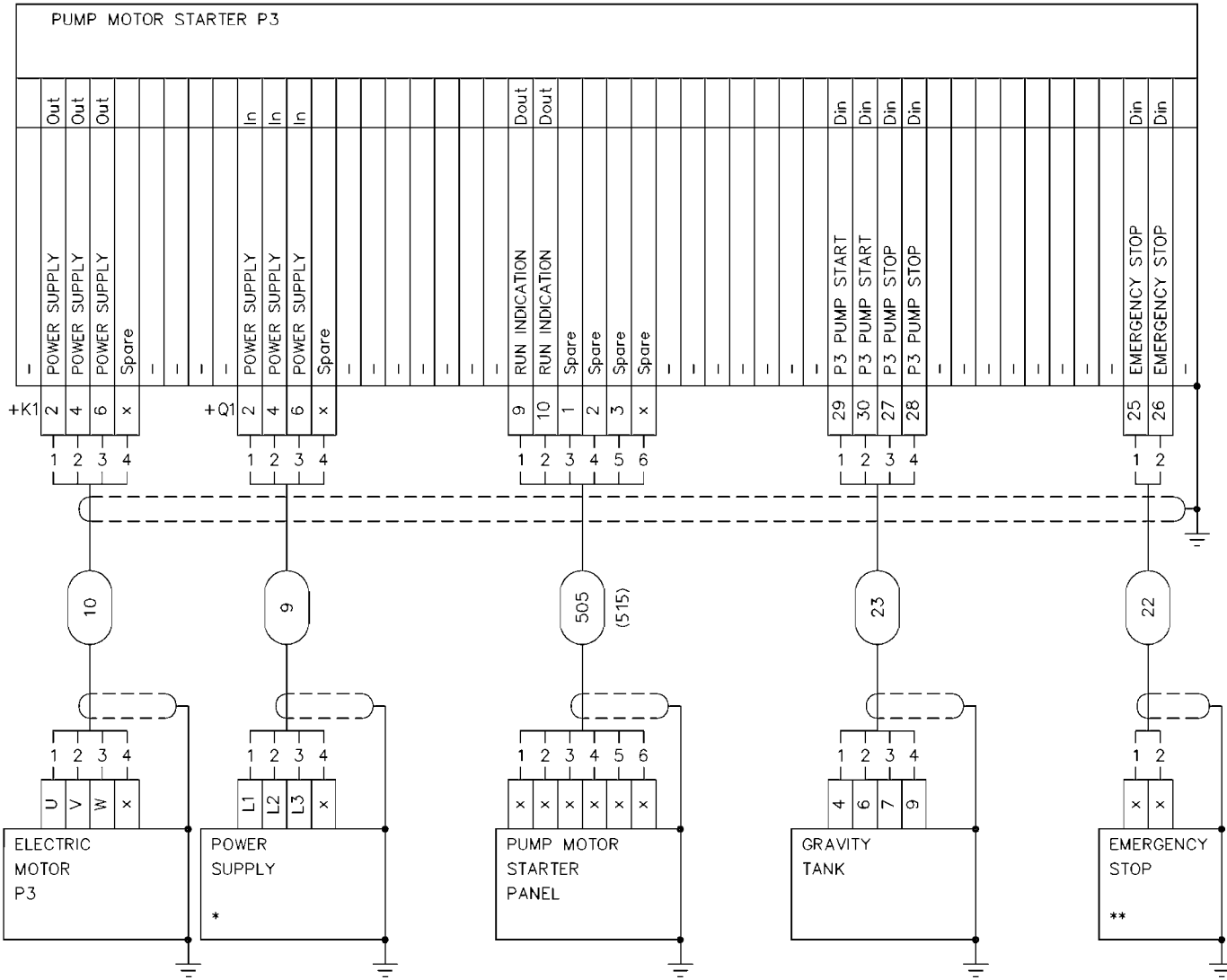
B

C

D

E


F



* NOT ROLLS ROYCE DELIVERY

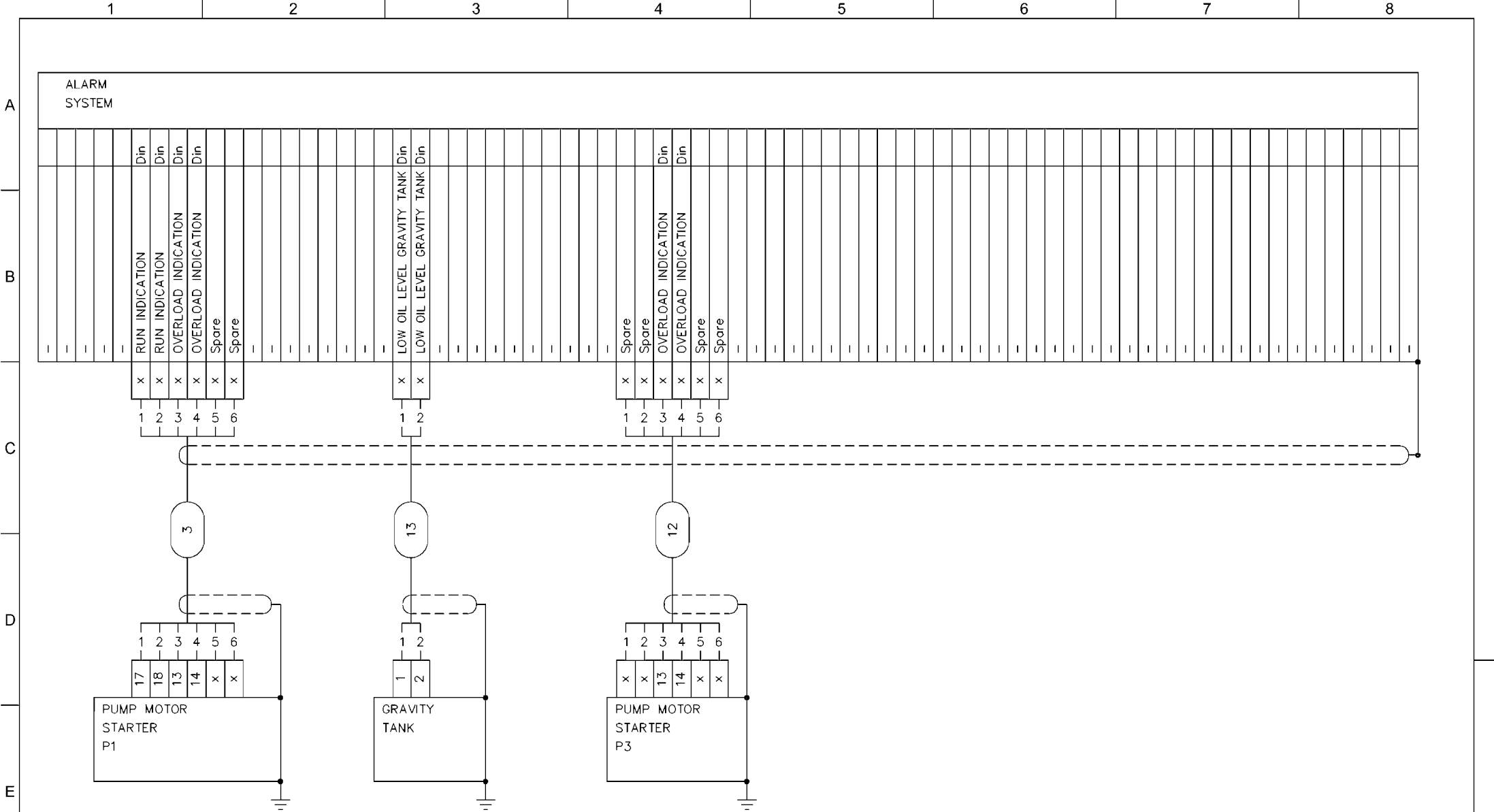
** DEPENDING ON CLASSIFICATION SOCIETY THE EMRGENCY SWITCH IS NOT NEEDED.
IF SO CONNECT 25 TO 26.

THIS CABLE CONNECTION DRAWINGS SHOWS CONNECTION FOR A ONE PROPELLER SYSTEM.
IF TWIN PROPELLER INSTALLED, THE PORT AND STBD PROPELLER SYSTEMS ARE CONNECTED EQUALLY.
IF TWIN PROPELLER CABLE NUMBERS 505 ARE FOR PORT SIDE
AND 515 ARE FOR STARBOARD SIDE.


Cable connection drawing Main propeller		Checked: Har	Previous Drg:	
		Approved: Mnmn	Weight kg:	
 Rolls-Royce Rolls-Royce AB Propulsion Kristinehamn	Origin. / Date: Jnla 2010-04-27	Scale: A3	Format: 3 or 4	Sheet: B
	Drawing no: DMN200000984			Revision: B
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Access List

RR AB S Info. Class:
LIMITED



THIS CABLE CONNECTION DRAWINGS SHOWS CONNECTION FOR A ONE PROPELLER SYSTEM.
IF TWO PROPELLER INSTALLED, THE PORT AND STBD PROPELLER SYSTEMS ARE CONNECTED EQUALLY.

Cable connection drawing Main propeller		Checked: Har		Previous Drg:	
		Approved: Mnmn		Weight kg:	
 Rolls-Royce Rolls-Royce AB Propulsion Kristinehamn	Origin. / Date: Jnlä 2010-04-27		Scale:	Format: A3	Sheet: 4 of 4
	Drawing no. DMN200000984			Revision: B	
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RR AB S Info. Class.
 LIMITED

	1	2	3	4	5	6	7	8			
A	No.	SUPERVISION OF	LOCATION	TO LOW	TO HIGH	TYPE	FUNCTION	MAKER	SETTING POINT	DELAY SEC.	NOTE
	1										
	2										
	3										
	4										
	5										
	6										
	7										
B	8										
	9										
	10	Overload P1	PMS			R	Overload on pump motor starter for P1	R-R AB			NC
	11										
	12	Overload P3	PMS			R	Overload on pump motor starter for P3	R-R AB			NC
	13										
	14										
	15										
C	16										
	17	Pressure transmitter PT2	PP			A	Alarm/monitoring oil pressure in mainpump system	Hydac	low 0,8 MPa	10	4-20 mA (0-25MPa)
	18	Pressure transmitter PT3	PP			A	Alarm/monitoring static oil pressure in hub	Hydac	low 0,08 MPa	10	4-20 mA (0-1,6MPa)
	19										
	20	Temperature sensor TT1	PP			S	Alarm/monitoring oil temperature	Thermotech	high 65°C	10	Pt100
	21	Level switch LS1	PP	X		L	Alarm low oil level	Barksdale		10	NC
	22	Level switch LS3	GT			L	Alarm low oil level, start, stop static pressure pump	Barksdale		10	NC, NO & NC
	23										
D	24	Pressure switch F3	PP		X	P	Alarm clogged filter F3	Hydac	Fixed	10	NC
	25										
	26										
E	TYPE: P=PRESSURE SWITCH R=RELAY, VOLTAGE FREE CONTACT L=LEVEL SWITCH A=ANALOGIC TRANSMITTER T=TEMPERATURE SWITCH E=ELECTRIC SWITCH D=DIFFERENTIAL PRESSURE SWITCH S=TEMPERATURE SENSOR M=ELECTRIC MOTOR V=HYDRAULIC VALVE		LOCATION: CU=CENTRAL UNIT CLOSED LOOP PMS=PUMP MOTOR STARTER PP=HYDRAULIC POWER PACK DOT=DRAIN OIL TANK GT=GRAVITY TANK JCU=JOYSTICK CENTRAL UNIT OD=OD-BOX NOTE: NO=NORMALY OPEN NC=NORMALY CLOSED								
F											

Remote supervision
Main propeller
Alarmlista

Rolls-Royce

Rolls-Royce AB
Propulsion Kristinehamn

Origin. / Date:
Jnla 2010-04-27

Drawing no.
DMN200000982

Checked:
Har

Approved:
Mnmn

Scale:
A3

Previous Drg.

Weight kg:

Sheet:
1 of 1

Revision:
B

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Access List

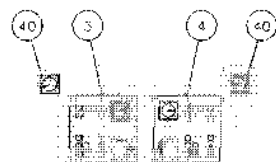
RR AB S Info. Class
LIMITED

Access List

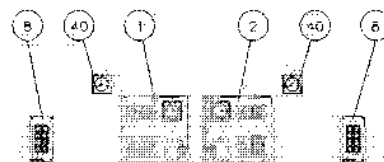
RR AB S Inf. Class:
LIMITED

BRIDGE

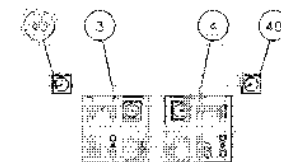
PORT ANNEX



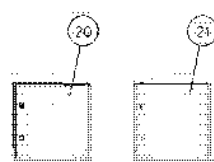
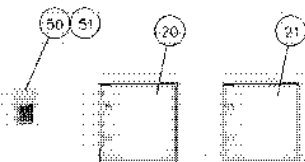
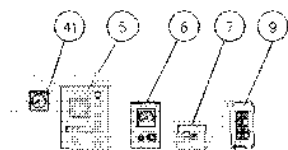
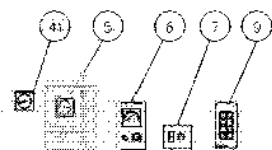
MAIN BRIDGE



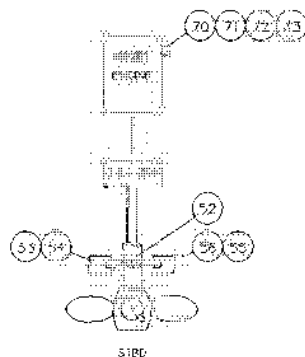
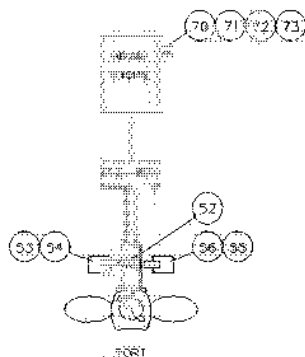
STAR ANNEX



CONTROL ROOM



ENGINE ROOM

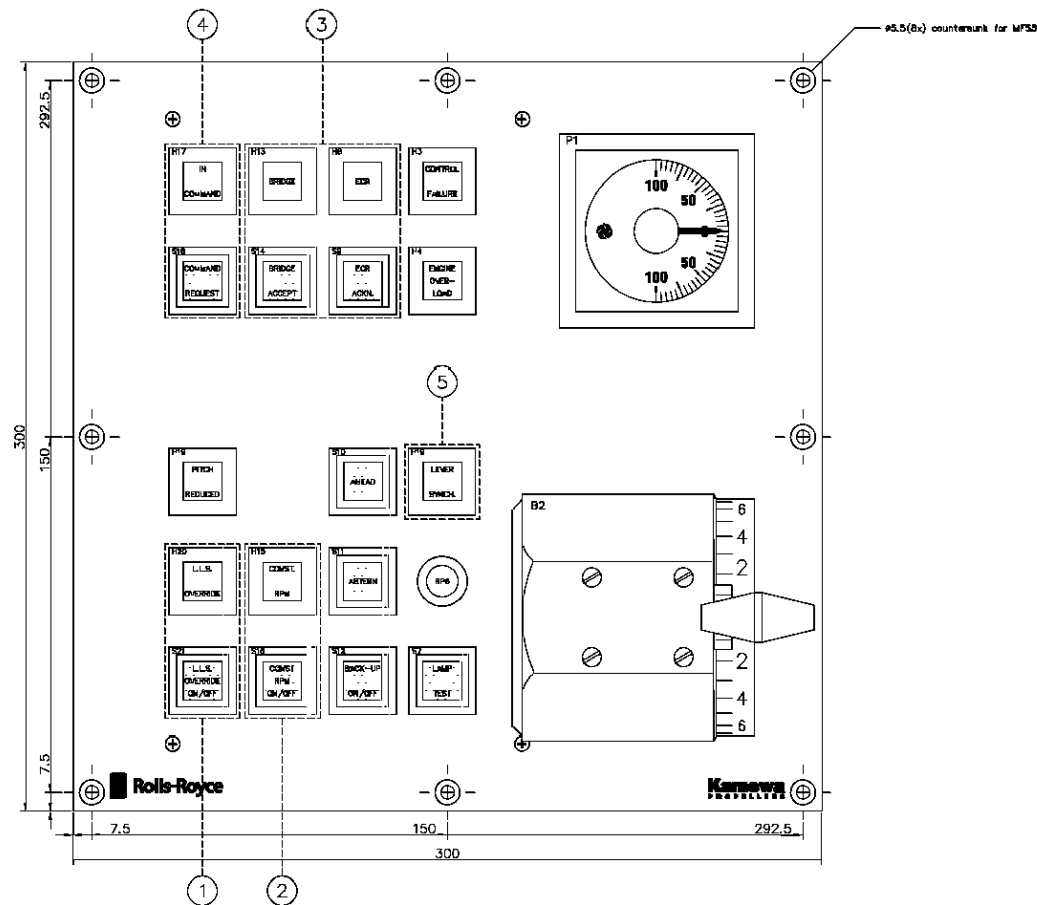


(100) SPARE PARTS

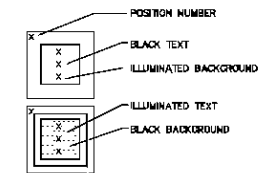
NOTES

- Item 1: Option 1,2,3,4,5
- Item 2: Option 1,2,3,4,5
- Item 3: Option 1,2,3, 456
- Item 4: Option 1,2,3, 456

Cable connection diagram		Revision	
Kamewa Basic		1	
Rolls-Royce		1	
RRM200005995		A	



YELLOW LAMP: H-5,8,15,19,20
 RED LAMP: H-3,4
 BLUE LAMP:
 GREEN LAMP: H-13,17
 TRANSPARENT LAMP:
 YELLOW PUSH-BUTTON:
 RED PUSH-BUTTON:
 BLUE PUSH-BUTTON: S-12
 GREEN PUSH-BUTTON:
 TRANSPARENT PUSH-BUTTON: S-7,9,10,11,14,16,18,21
 BLACK LENS (DUMMY):
 PUSH-BUTTON COVER:
 PROTECTION COVER (SILICON):
 SWITCH:

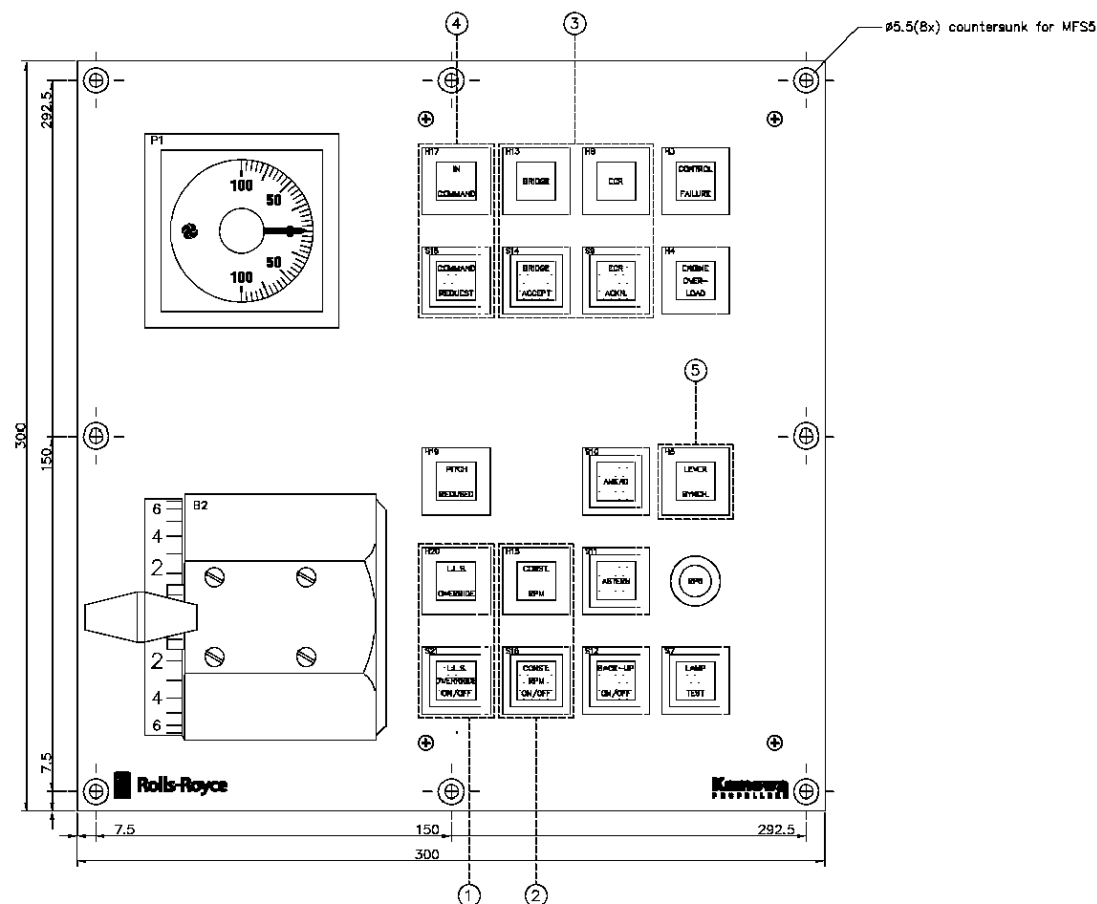


HEIGHT OVER PANEL: 180mm
 MAX DEPTH: 100mm
 WEIGHT: 3.3kg
 PROTECTION DEGREE: IP65
 PANEL SURFACE: BLACK ANODIZED
 SCREEN PRINT COLOUR: YELLOW
 LOGO COLOUR: WHITE
 INSTRUMENT COLOUR: BLACK/YELLOW
 CUT OUT IN DESK: 270 x 270 mm(H x W)

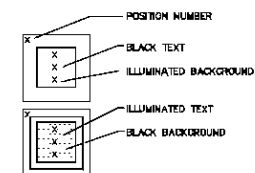
FUNCTIONAL OPTIONS

- ① LOAD CONTROL
- ② CONSTANT RPM. (COMBINATOR)
- ③ MANOEUVRE RESPONSIBILITY, BRIDGE CONTROL ROOM
- ④ MANOEUVRE RESPONSIBILITY, BRIDGE ANNEX
- ⑤ LEVER SYNCHRO LAMP

Only printed labels, Surface Protection: 26-400 1200 (H x W) mm	Optional: Temperature: -10 to +22 °C	Supply voltage: 24V DC	Position: 1 of 1
Control panel, layout			
Kamewa Main Propeller, Base bridge			
Rolls-Royce		Project: RRM200005922	Project by: KKS
Rolls-Royce AB Propulsion Systems Division		Design: 11/104 Drawing no: 221.038.20710	Version: 1.1 Sheet: 1 of 1
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YELLOW LAMP: H-5,8,15,19,20
 RED LAMP: H-3,4
 BLUE LAMP:
 GREEN LAMP: H-13,17
 TRANSPARENT LAMP:
 YELLOW PUSH-BUTTON:
 RED PUSH-BUTTON:
 BLUE PUSH-BUTTON: S-12
 GREEN PUSH-BUTTON:
 TRANSPARENT PUSH-BUTTON: S-7,9,10,11,14,16,18,21
 BLACK LENS (DUMMY):
 PUSH-BUTTON COVER:
 PROTECTION COVER (SILICON):
 SWITCH:

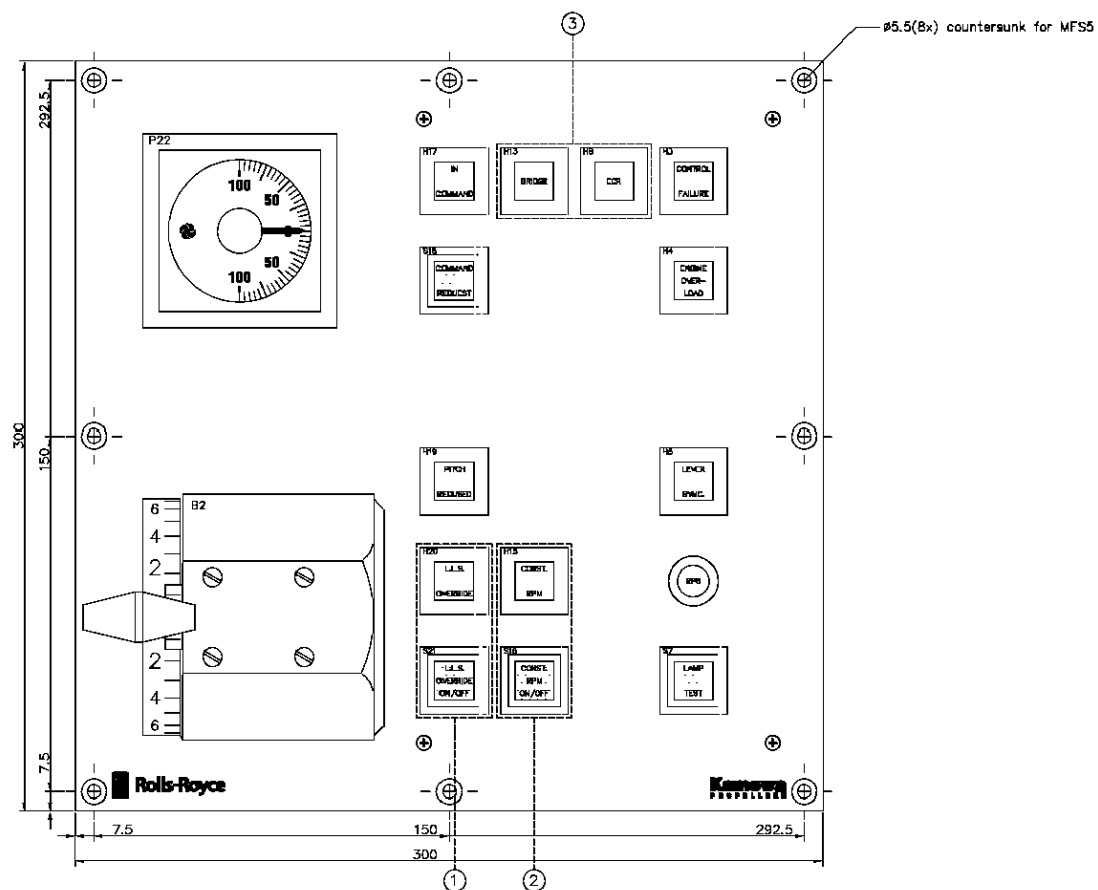


HEIGHT OVER PANEL: 180mm
 MAX DEPTH: 100mm
 WEIGHT: 3.3kg
 PROTECTION DEGREE: IP65
 PANEL SURFACE: BLACK ANODIZED
 SCREEN PRINT COLOUR: YELLOW
 LOGO COLOUR: WHITE
 INSTRUMENT COLOUR: BLACK/YELLOW
 CUT OUT IN DESK: 270 x 270 mm(H x W)

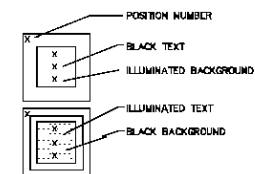
FUNCTIONAL OPTIONS

- ① LOAD CONTROL
- ② CONSTANT RPM. (COMBINATOR)
- ③ MANOEUVRE RESPONSIBILITY, BRIDGE CONTROL ROOM
- ④ MANOEUVRE RESPONSIBILITY, BRIDGE ANNEX
- ⑤ LEVER SYNCHRO LAMP

Only panel shown. Surface Roughness: 25-40/125 Ra 1.6mm	Customer Reference: 15-000 22 001	Supply origin bracket: 12-0-0	
Control panel, layout	Checked: KKS21	Position: 0/0	
Kamewa Main Propeller, Base bridge	Approved: KKS21	Project: 1	
	Origin: China	Part no:	Sheet:
Version: 2023/09/20	1-1	A1	1 of 1
Drawing no:		Revision:	
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YELLOW LAMP: H-5,8,15,19,20
 RED LAMP: H-3,4
 BLUE LAMP:
 GREEN LAMP: H-13,17
 TRANSPARENT LAMP:
 YELLOW PUSH-BUTTON:
 RED PUSH-BUTTON:
 BLUE PUSH-BUTTON:
 GREEN PUSH-BUTTON:
 TRANSPARENT PUSH-BUTTON: S-7,16,18,21
 BLACK LENS (DUMMY):
 PUSH-BUTTON COVER:
 PROTECTION COVER (SILICON): S-7,16,18,21
 SWITCH:

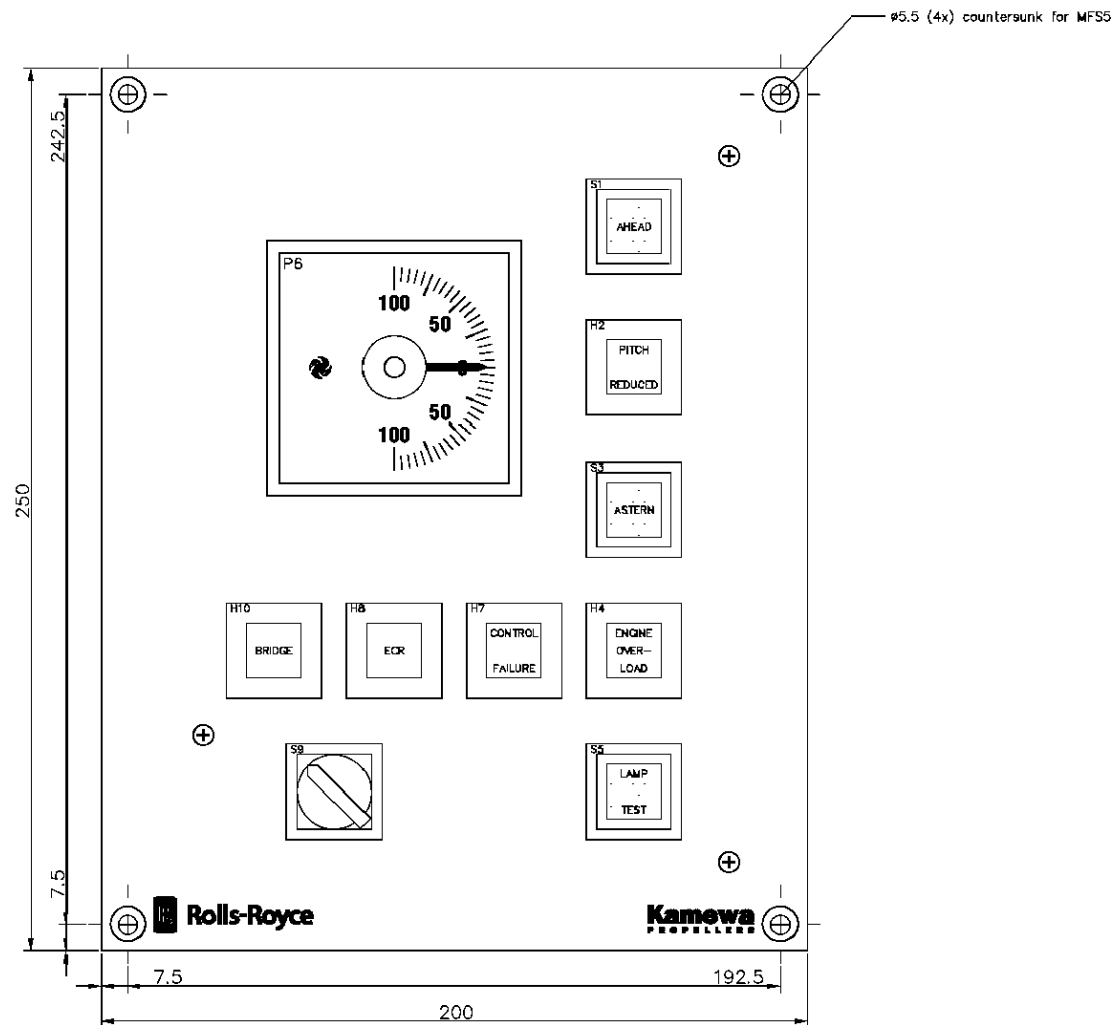


HEIGHT OVER PANEL: 160mm
 MAX DEPTH: 100mm
 WEIGHT: 3.2kg
 PROTECTION DEGREE: IP66
 PANEL SURFACE: BLACK ANODIZED
 SCREEN PRINT COLOUR: YELLOW
 LOGO COLOUR: WHITE
 INSTRUMENT COLOUR: BLACK/YELLOW
 CUT OUT IN DESK: 270 x 270 mm(H x W)

FUNCTIONAL OPTIONS

- ① LOAD CONTROL
- ② CONSTANT RPM, (COMBINATOR)
- ③ MANOEUVRE RESPONSIBILITY, BRIDGE CONTROL ROOM

Only panel shown. Surface Roughness: 25-60 1250 Ra 15 µm	General Tolerances: ISO 2768	Sharp edges broken: 2.5-3.0	Position Dep.
Control panel, layout			
Kamewa Main Propeller, Basic bridge wing			
Rolls-Royce	Drawn by: 19/04 2013/03/2013	Scale: 1:1	Format: A1
Rolls-Royce AB Propulsion Technology Division	Checked by: KKS	Drawn by: KKS	Format: A
RRM200005950			
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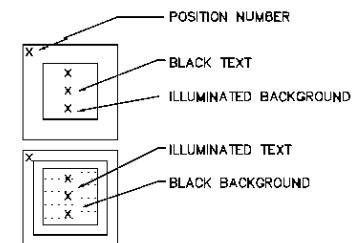


YELLOW LAMP: H-2,10
 RED LAMP: H-4,7
 BLUE LAMP:
 GREEN LAMP: H-8
 TRANSPARENT LAMP:

YELLOW PUSH-BUTTON:
 RED PUSH-BUTTON:
 BLUE PUSH-BUTTON:
 GREEN PUSH-BUTTON:
 TRANSPARENT PUSH-BUTTON: S-1,3,5

BLACK LENS (DUMMY):
 PUSH-BUTTON COVER:
 PROTECTION COVER (SILICON):

SWITCH: S-9

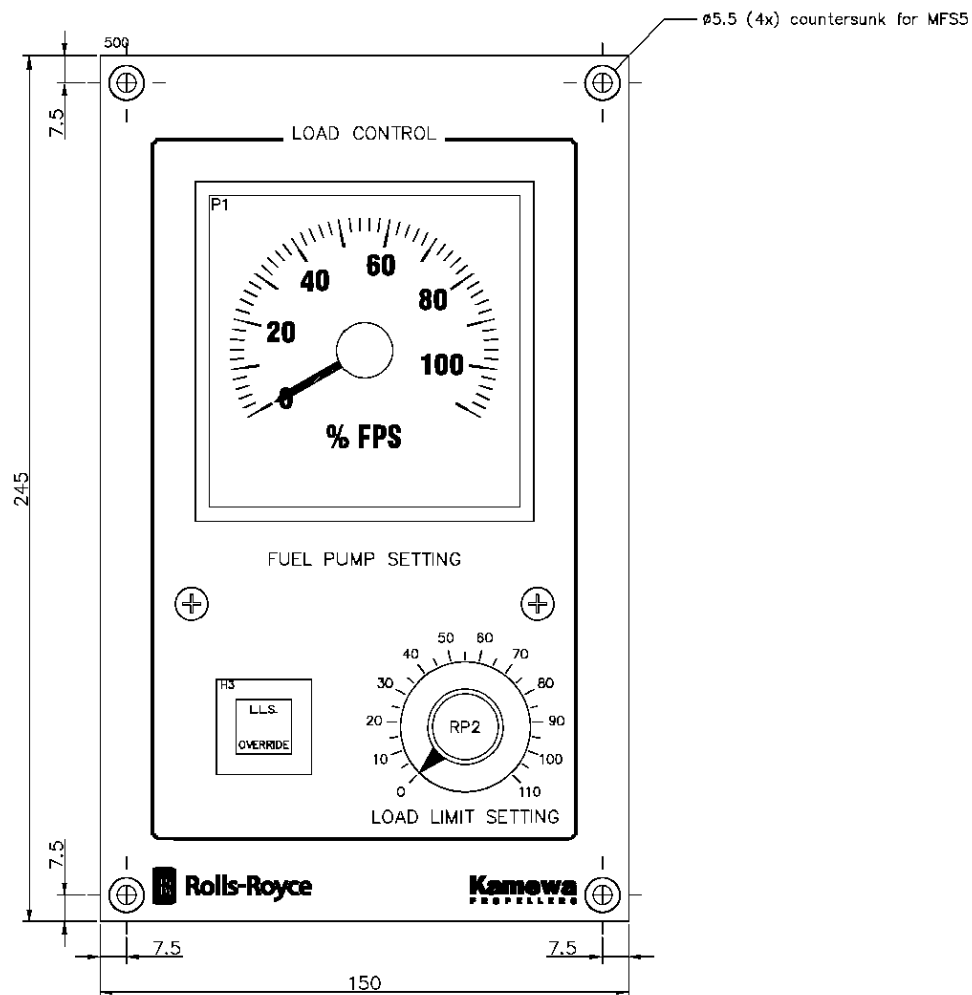


HEIGHT OVER PANEL: 15mm
 MAX DEPTH: 100mm
 WEIGHT: 3Kg
 PROTECTION DEGREE: IP52
 PANEL SURFACE: BLACK ANODIZED
 SCREEN PRINT COLOUR: YELLOW
 LOGO COLOUR: WHITE
 INSTRUMENT COLOUR: WHITE/BLACK
 CUT OUT IN DESK: 220x170mm (H x W)

Order panel plates, Surface Roughness: SIS-ISO 1305 Ra 1.6 µm	General Tolerances: SIS-ISO 2768-M	Sharp edges broken: 0.2x0.5	Checked KJ201	Perforce Drg
Control panel, layout			Approved KJ35	Weight kg
Kamewa Main Propeller, ECR Basic			Scale	Format
 Rolls-Royce AG Propulsion Krefeld/Helm			Origin / Date WKM 22.03.2010	Sheet 1 of 4
Drawing no. RRM200005951			Scale 1:1	Revisions A
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Rolls-Royce AG, Krefeld
 47805 Krefeld
 Germany

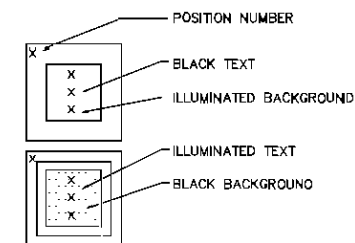


YELLOW LAMP: H-3
 RED LAMP:
 BLUE LAMP:
 GREEN LAMP:
 TRANSPARENT LAMP:

YELLOW PUSH-BUTTON:
 RED PUSH-BUTTON:
 BLUE PUSH-BUTTON:
 GREEN PUSH-BUTTON:
 TRANSPARENT PUSH-BUTTON:

BLACK LENS (DUMMY):
 PUSH-BUTTON COVER:
 PROTECTION COVER (SILICON):

SWITCH:



HEIGHT OVER PANEL: 23mm
 MAX DEPTH: 180mm
 WEIGHT: 1kg
 PROTECTION DEGREE: IP52
 PANEL SURFACE: BLACK ANODIZED
 SCREEN PRINT COLOUR: YELLOW
 LOGO COLOUR: WHITE
 INSTRUMENT COLOUR: WHITE/BLACK
 CUT OUT IN DESK: 215 x 120 mm(H x W)

Order panel plates, Surface Roughness: SIS-ISO 1305 Ra 1.6 µm	General Tolerances: SIS-ISO 2768-M	Sharp edges broken: 0.2x0.5	Checked: KK201	Performs Drg: 129011
Control panel, layout			Approved: KK35	Weight kg:
Kamewa Main Propeller, load control panel			Origin / Date:	Scale:
Rolls-Royce			KK172 23.09.2009	1:1
Rolls-Royce AB Propulsion Kretzschmar			Drawing no:	Format:
RRM200001864			Sheet:	1 of 3
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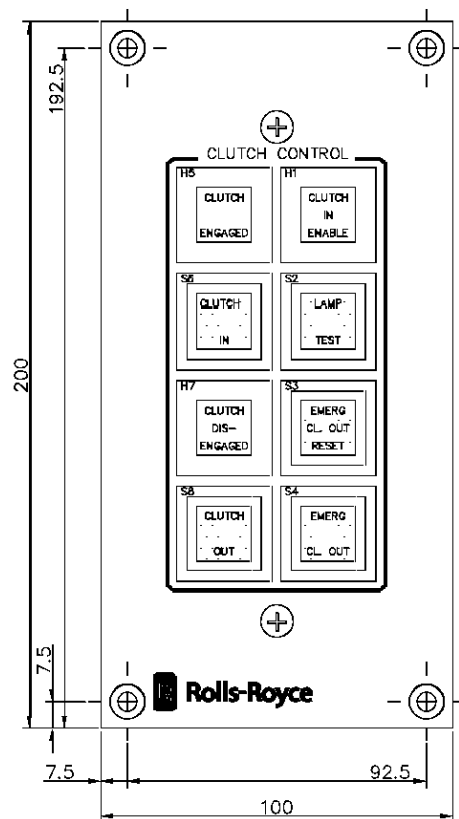
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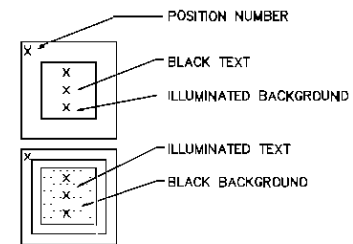
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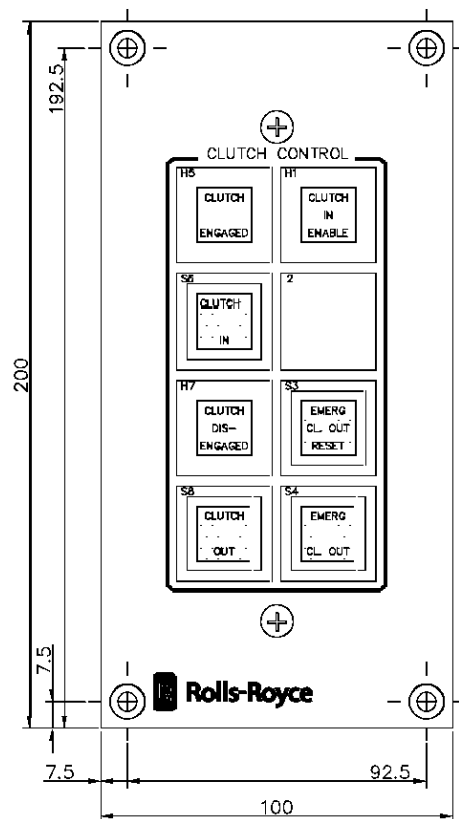


YELLOW LAMP: H-7
 RED LAMP:
 BLUE LAMP:
 GREEN LAMP: H-1,5
 TRANSPARENT LAMP:
 YELLOW PUSH-BUTTON:
 RED PUSH-BUTTON: S-3,4
 BLUE PUSH-BUTTON:
 GREEN PUSH-BUTTON:
 TRANSPARENT PUSH-BUTTON: S-2,4,6
 BLACK LENS (DUMMY):
 PUSH-BUTTON COVER: S-4
 PROTECTION COVER (SILICON):
 SWITCH:



HEIGHT OVER PANEL: 5 mm
 MAX DEPTH: 180 mm
 WEIGHT: 1 kg
 PROTECTION DEGREE: IP 65
 PANEL SURFACE: BLACK, ANODIZED
 SCREEN PRINT COLOUR: YELLOW
 LOGO COLOUR: WHITE
 INSTRUMENT COLOUR: BLACK/YELLOW
 CUT OUT IN DESK: 170 x 70 mm(H x W)

Order panel plates, Surface Roughness: SIS-ISO 1305 Ra 1.6 µm	General Tolerances: SIS-ISO 2768-M	Sharp edges broken: 0.2x0.6	Checked: KKS	Positioning: KKS
Control panel, wiring			Approved: KKS	Weight kg:
Kamewa Main Propeller, Basic Bridge Clutch Control panel			Scale:	Format:
Rolls-Royce Rolls-Royce AB Propulsion Kette/Division			Origin / Date: WKM 31.03.2010	Sheet: 1 of 3
Drawing no: RRM200005928			Scale: 1:1	Format: A2
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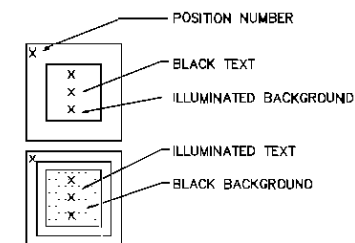


YELLOW LAMP: H-7
 RED LAMP:
 BLUE LAMP:
 GREEN LAMP: H-1,5
 TRANSPARENT LAMP:

YELLOW PUSH-BUTTON:
 RED PUSH-BUTTON: S-3,4
 BLUE PUSH-BUTTON:
 GREEN PUSH-BUTTON:
 TRANSPARENT PUSH-BUTTON: S-4,6

BLACK LENS (DUMMY): 2
 PUSH-BUTTON COVER: S-4
 PROTECTION COVER (SILICON):

SWITCH:



HEIGHT OVER PANEL: 5 mm
 MAX DEPTH: 180 mm
 WEIGHT: 1 kg
 PROTECTION DEGREE: IP 65
 PANEL SURFACE: BLACK, ANODIZED
 SCREEN PRINT COLOUR: YELLOW
 LOGO COLOUR: WHITE
 INSTRUMENT COLOUR: BLACK/YELLOW
 CUT OUT IN DESK: 170 x 70 mm(H x W)

Order panel plates, Surface Roughness: SIS-ISO 1305 Ra 1,6 µm	General Tolerances: SIS-ISO 2768-M	Sharp edges & broken: 0,2-0,6	Checked: KK35	Perforate Drg:
Control panel, wiring			Approved: KK201	Weight kg:
Kamewa Main Propeller, Basic ECR Clutch Control panel			Scale:	Format:
Origin. / Date:			Sheet:	1 of 3
Rolls-Royce Rolls-Royce AB Propulsion Kretzschmar			WKM 30.03.2010 Drawing no:	Revisions:
			RRM200005952	A
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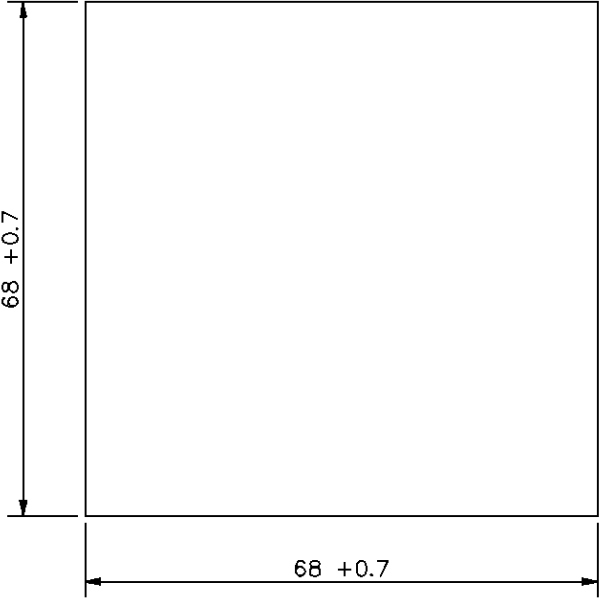
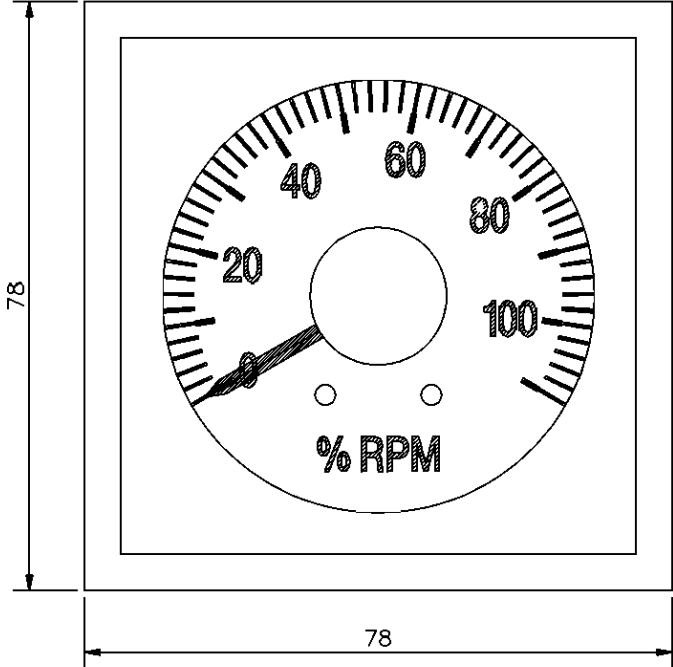
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H

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PANEL CUT OUT

HEIGHT OVER PANEL: 6 mm
MAX DEPTH: 100 mm
WEIGHT: 0.23 Kg
PROTECTION DEGREE: IP66
SURFACE: BLACK
SCALE/TEXT: YELLOW

INSTRUMENT: DEIF DLQW72-pc-PY
ILLUMINATION: 24VDC
MEASURING RANGE: 0-10V, 0-110 %RPM
SCALE DRAWING: 1113500131

<div>KAMEWA</div> <div>KRISTINEHAMN SWEDEN</div>	Electronic control Standard MAIN PROPELLER _ _ _ _ RPM Indicator DLQW72		Drawn	Checked	Approved	Scale	Form
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			128952				Design
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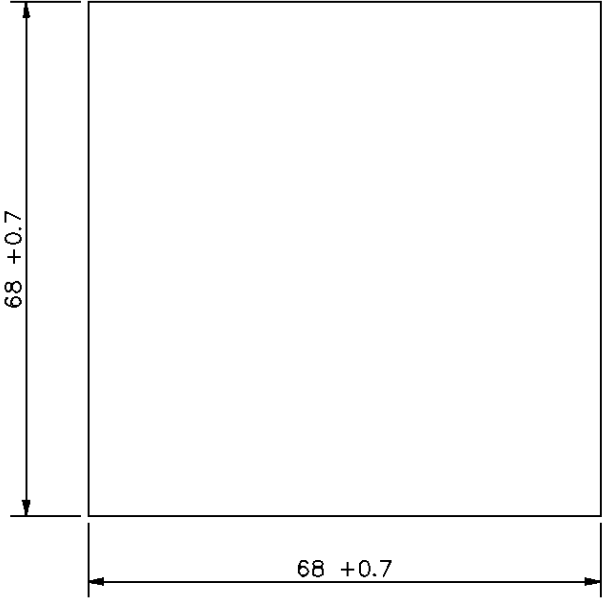
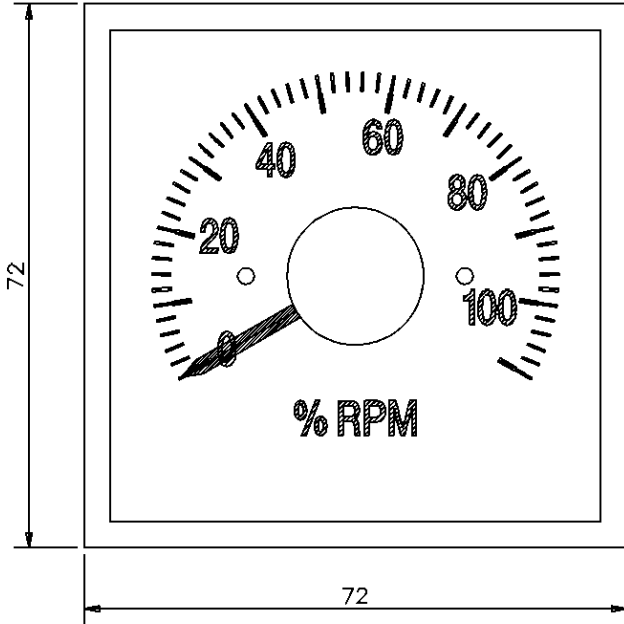
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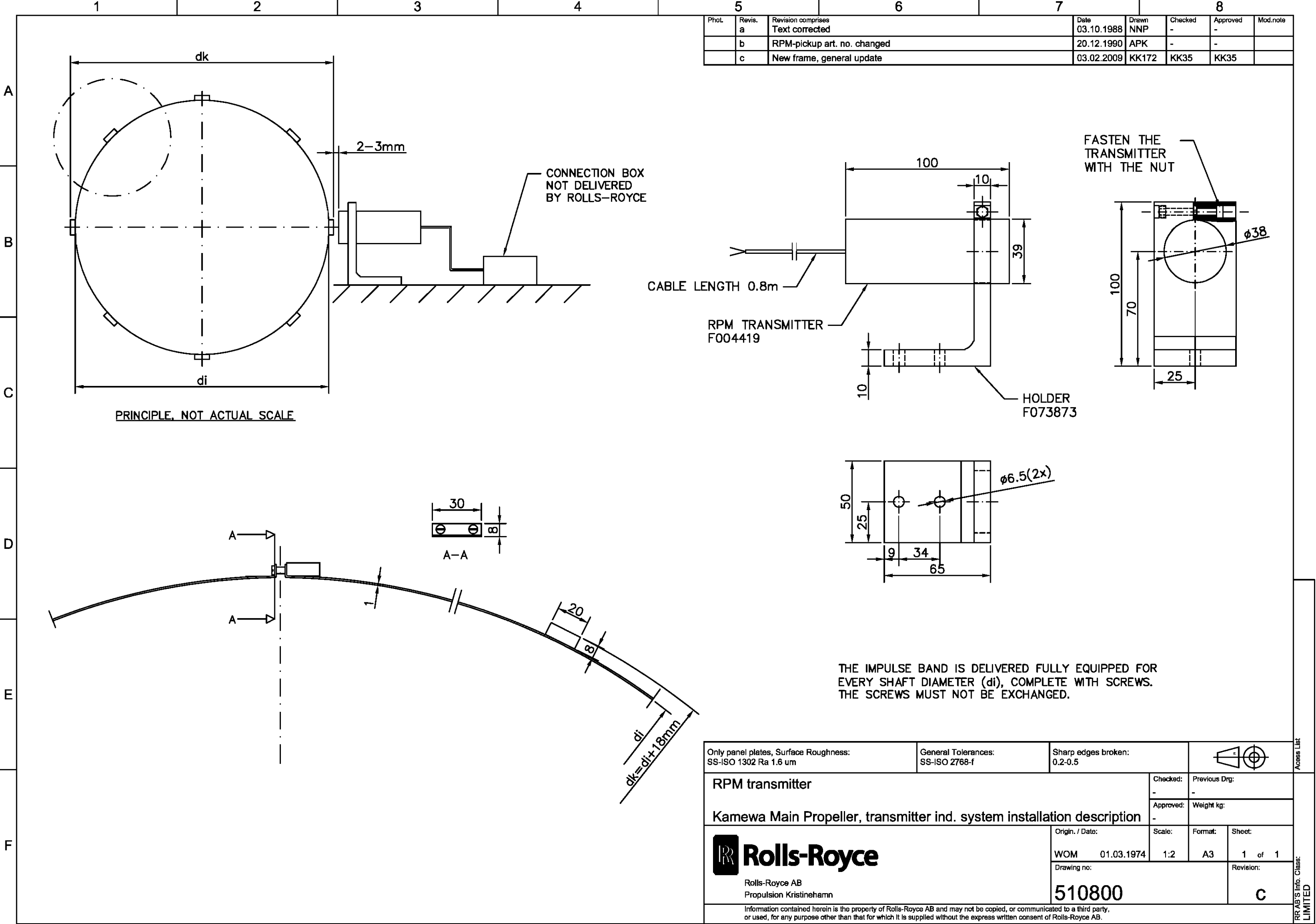


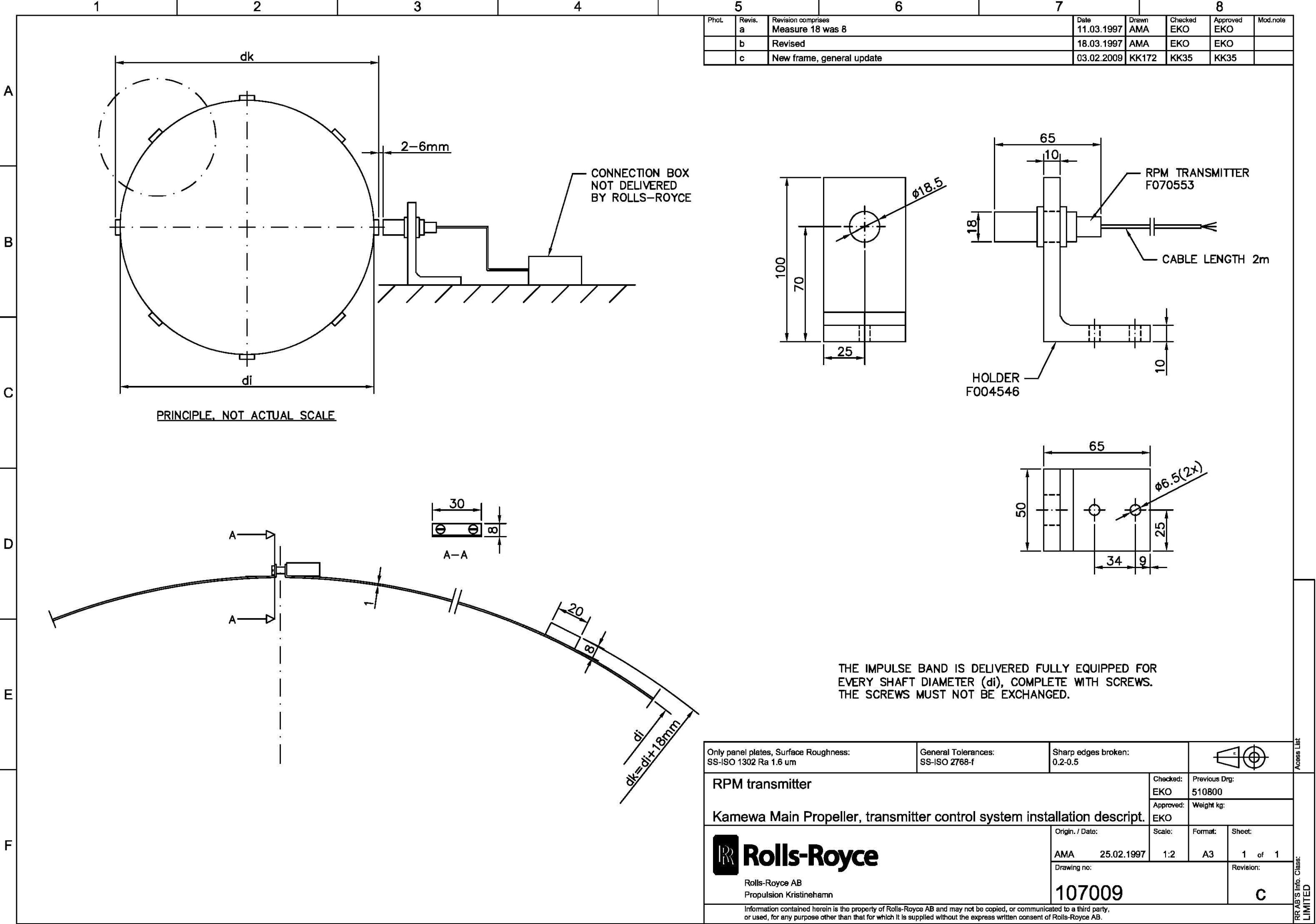
PANEL CUT OUT

HEIGHT OVER PANEL: 6 mm
MAX DEPTH: 100 mm
WEIGHT: 0.23 Kg
PROTECTION DEGREE: IP52
SURFACE: WHITE
SCALE/TEXT: BLACK

INSTRUMENT: DEIF DQ72-c-NB
ILLUMINATION: None
MEASURING RANGE: 0-10V, 0-110 %RPM
SCALE DRAWING: 1114010129

<div>KAMEWA</div> <div>KRISTINEHAMN SWEDEN</div>	Electronic control Standard MAIN PROPELLER _ _ _ _ RPM Indicator DQ72		Drawn	Checked	Approved	Scale	Form
			Jnm	Ena	Ena	1:1	A3
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			020121			1	1
			128967				Design
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Produced by: SS Approved by: Nna
Creation date: 2005-05-31

Revision: Sign:
Revision date:

Revision

Document No.	Rev.	Date	Section	Description	Approved



Subsupplier Manuals

Title	Document Number	Rev
SKF		
The SKF OKCX Coupling for Shafts Mounting and Dismounting Instruction	49990-E	
High Pressure Pump Assembly	49035-E	
Service Guide High Pressure Stripped Pump	49036-E	
Service Guide Pneumatic Logic Air Motor	49037-E	
B+V Industrietechnik GmbH		
Installation of the seal Simplan Seal Typ:SIC-P	Enclosed	
Instruction Manual Simplan Seal Typ:SIC-P	Enclosed	
Removal of split ring Simplan Seal Typ:SIC-P	Enclosed	
Thordon		
Compac Propeller Shaft Bearing Specification	49892-E	
Marine Bearing Installation Manual	48081-E	
Corrpro		
Instruction Manual (Analog) Propeller Shaft Grounding and Monitoring Assembly	49884-E	
Oil Tech		
Water Oil Cooler PWO Installation and Service Instructions	49995-E	

The SKF OKCX coupling for shafts 100-900 mounting and dismounting instruction

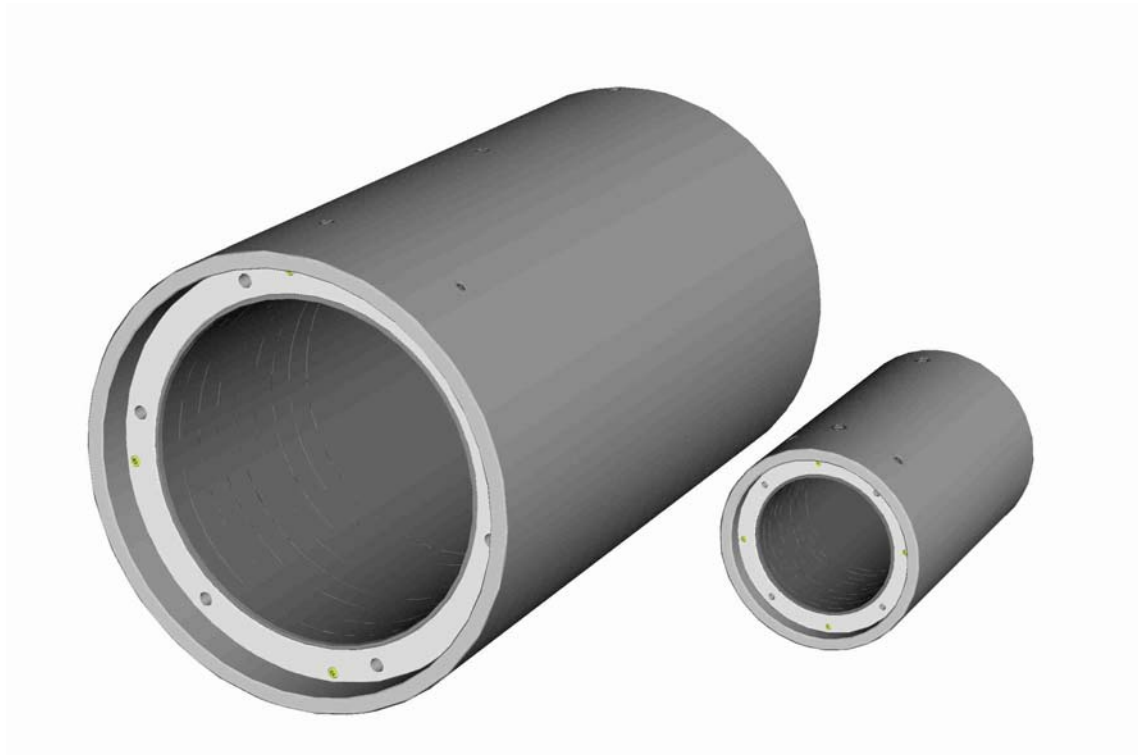
Instruction No.:

81569

Edition: A

Edition Date:

2006-02-17



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2	THE PRINCIPLE OF THE COUPLING	4
3	OIL RECOMMENDATION	5
4	DESIGNATION OF THE COUPLING	5
5	COUPLING DETAILS	6
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7	MOUNTING INSTRUCTIONS	9
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9	REPLACING THE OIL CHAMBER SEALING	15
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1 CAUTIONS AND PERSONAL SAFETY

- When using the hydraulic equipment and injectors, always wear eye protection and gloves.
- When handling the coupling with crane, make sure that the lifting device is adapted to the weight of the coupling.
- Use the correct oil as shown in the instructions.
- Use all equipment strictly in accordance with the instructions, or the instructions supplied by the equipment manufacturer.
- Inspect all equipment for damage before use.
- As a precaution, when mounting/dismounting the coupling, the area in front of and behind the coupling must be kept clear of all personnel.

2 THE PRINCIPLE OF THE COUPLING

The OKCX type coupling consists basically of two sleeves of high quality steel, a thin inner sleeve and a thick outer sleeve.

The outer surface of the inner sleeve is slightly tapered and the bore of the outer sleeve has a corresponding taper.

The inner sleeve bore is somewhat larger than the diameter of the shafts, so that the sleeve can be passed over them with ease.

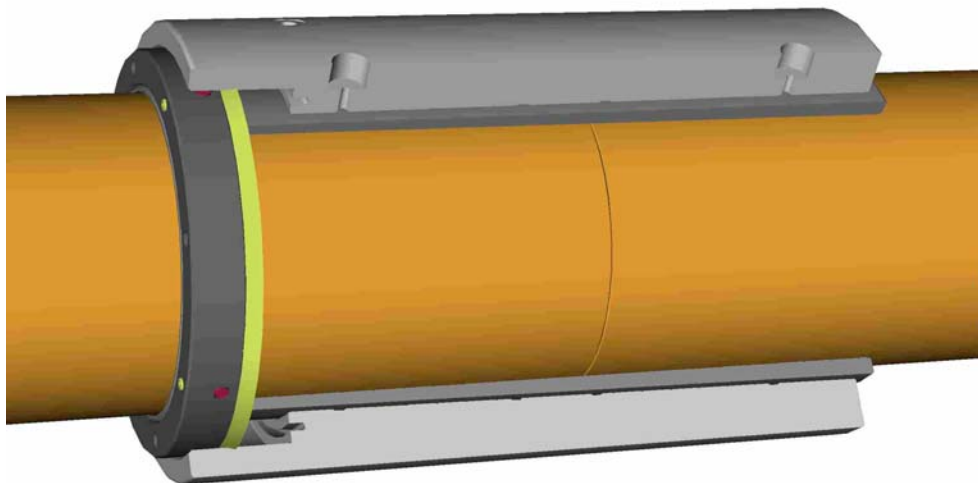
The coupling is mounted by driving the outer sleeve up on the taper of the inner sleeve using the hydraulic unit incorporated in the coupling.

This action compresses the inner sleeve onto shaft creating a powerful interference fit.

To allow this drive-up, the friction of the matching tapered surfaces is overcome by injecting oil at high pressure between them, where it forms a load-carrying film separating the two components.

When the outer sleeve has reached the correct drive up position, the injection pressure is released and the oil is drained off between the mating tapered surfaces, restoring normal friction between the sleeves.

Dismounting the coupling is equally simple. Oil is injected between the coupling sleeves to overcome the friction. As a result of the taper, the compressive force has an axial component which causes the outer sleeve to slide down the taper, forcing the oil out of the hydraulic unit.



3 OIL RECOMMENDATION

The oil to be used for the injector should have a viscosity of 300 mm²/s (300cS) at the temperature of the coupling. If the oil used for mounting is too thick, there is a risk that it will remain between the sleeves, resulting in a considerably deteriorated grip. The adequate viscosity will generally be obtained with sufficient accuracy if the oil is chosen as follows:

<i>Temperature range</i>		<i>Viscosity in SAE</i>	
0	- 8°C	Motor Oil	SAE 10 W
8	- 18°C	Motor Oil	SAE 20 W
18	- 27°C	Motor Oil	SAE 30
24	- 32°C	Motor Oil	SAE 40
32	- 38°C	Motor Oil	SAE 50

4 DESIGNATION OF THE COUPLING

The coupling is designated as "Type "OKCX", "OKCEX", "OKCAX" or "OKCKX". OKCEX and OKCAX are elongated and OKCKX is shortened compared with standard OKCX.

Coupling sizes are specified using the following system:

OKCX (EX, AX, KX), shaft diameter / drawing number.

For example: OKCX 280/xxxxx

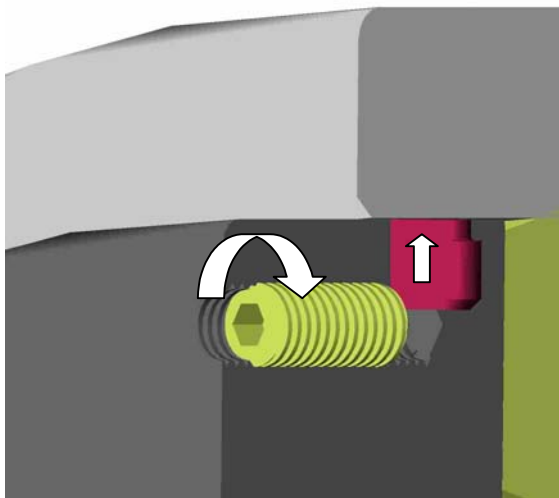
COUPLING DETAILS

For details see enclosed assembly drawing.

5 COUPLING DETAILS

5.1 Locking device

The couplings are provided with a locking device which prevents the outer sleeve from being driven up unintentionally on the inner sleeve during transport and when the coupling is positioned on the shaft. After the coupling has been installed it prevents the nut from turning due to centrifugal force. The locking device is located in the nut and consists of four S6SS screws and four plugs. When tightening the screws in an axial direction the plugs are vertically pressed against the internal diameter of the hydraulic chamber creating a lock function.



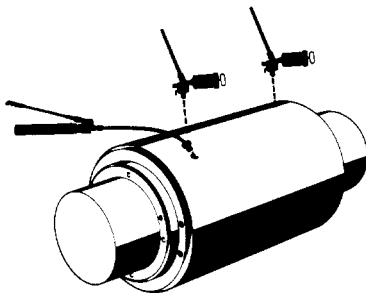
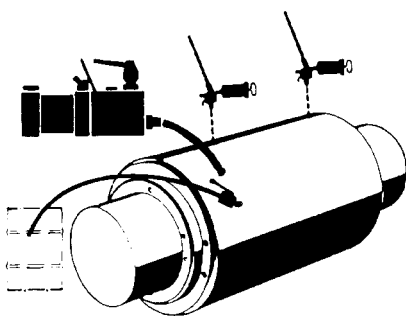
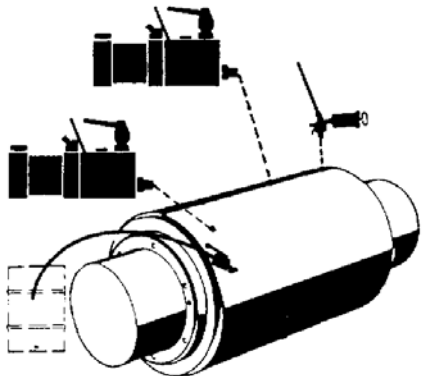
5.2 Handling the locking device

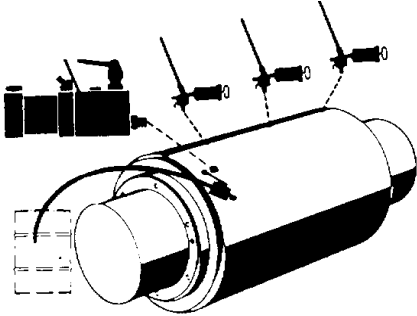
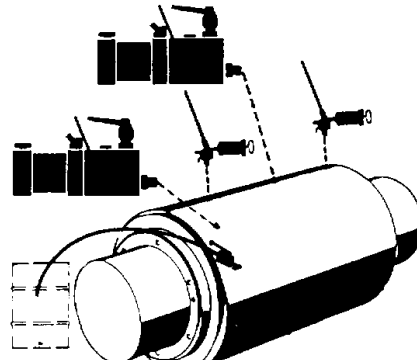
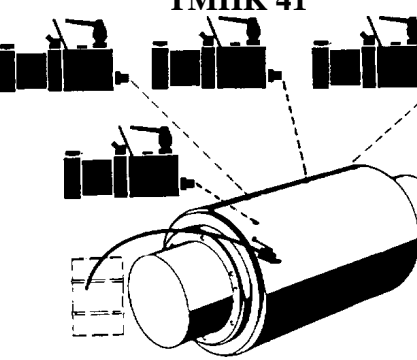
The locking devices should be released by unscrewing the screws 1/2 turn before starting the mounting procedure. When the coupling is finally mounted, the locking devices should be tightened once again. When tightening, tighten the screws crosswise (see table below for tightening torque). The gap between the nut and the hydraulic chamber can be inspected with a feeler gauge to make sure that the locking devices are activated.

Coupling size	Tightening torque
200-290	7 Nm
300-490	12 Nm
500-700	20 Nm

6 EQUIPMENT FOR MOUNTING AND DISMOUNTING

For mounting and dismantling of the coupling, a number of tool kits has been assembled. The kit to be used is selected with reference to the coupling size.

Coupling size	Description	SKF set no.
OKX / OKXA / OKXE 200- 500	1 Tool case 728245-3 2 Oil injector 226400 1 Hand operated pump TMJL 50 1 Pipe 227958A 1 Adapter block 226402 1 Set of hex keys 1 Spare parts for injector 226400 Mass: 28.1 kg. Set TMHK 38 can also be used for these coupling sizes. The set contains a hydraulic pump driven by compressed air which enables the coupling to be mounted more quickly.	TMHK 37 
OKX / OKXA / OKXE 200- 500	1 Air driven pump set: THAP 030/SET 1 Return hose 729147A 2 Oil injectors 226400 1 Set of hex keys 1 Spare parts for injector 226400 Mass: 32.1 kg	TMHK 38 
OKX / OKXA / OKXE 200- 500	1 Air driven pump set: THAP 030/SET 1 Return hose 729147A 1 Air-driven pump THAP 150 1 Oil injector 226400 1 Set of hex keys 1 Spare parts for injector 226400 Mass: 76.2 kg including weight of pallet	TMHK 38S 

<p>OKX / OKXA / OKXE 500 ></p>	<p>1 Air driven pump set: THAP 030/SET 1 Return hose 729147A 3 Oil injectors 226400 1 Set of hex keys 1 Spare parts for injector 226400 Mass: 35.1 kg. This set is intended for use on board ship where dismantling and mounting is only carried out infrequently. For shipyards and workshops TMHK 40 or TMHK 41 is recommended.</p>	<p>TMHK 39</p>  <p>The diagram shows a cylindrical coupling component with a flange on one end. Three oil injectors are shown with dashed lines indicating their connection points on the top of the cylinder. A return hose is connected to the side of the cylinder. The entire assembly is shown in a perspective view.</p>
<p>OKX / OKXA / OKXE 500 ></p> <p>OKX / OKXA / OKXE 500 ></p>	<p>1 Air driven pump set: THAP 030/SET 1 Return hose 729147A 1 Air-driven pump THAP 150 2 Oil injectors 226400 1 Set of hex keys 1 Spare parts for injector 226400 Mass: 78.2 kg including weight of pallet This set or also set TMHK 41 are recommended for shipyards and workshops. The air-driven high pressure pump simplifies works considerably.</p> <p>1 Air driven pump set: THAP 030/SET 1 Return hose 729147A 3 Air-driven pump THAP 150 1 Set of hex keys Mass 126.7 kg including weight of pallet. This set is recommended for shipyards and workshops.</p>	<p>TMHK 40</p>  <p>The diagram shows a cylindrical coupling component with a flange on one end. Two oil injectors are shown with dashed lines indicating their connection points on the top of the cylinder. A return hose is connected to the side of the cylinder. The entire assembly is shown in a perspective view.</p> <p>TMHK 41</p>  <p>The diagram shows a cylindrical coupling component with a flange on one end. Three air-driven pumps are shown with dashed lines indicating their connection points on the top of the cylinder. A return hose is connected to the side of the cylinder. The entire assembly is shown in a perspective view.</p>

7 MOUNTING INSTRUCTIONS

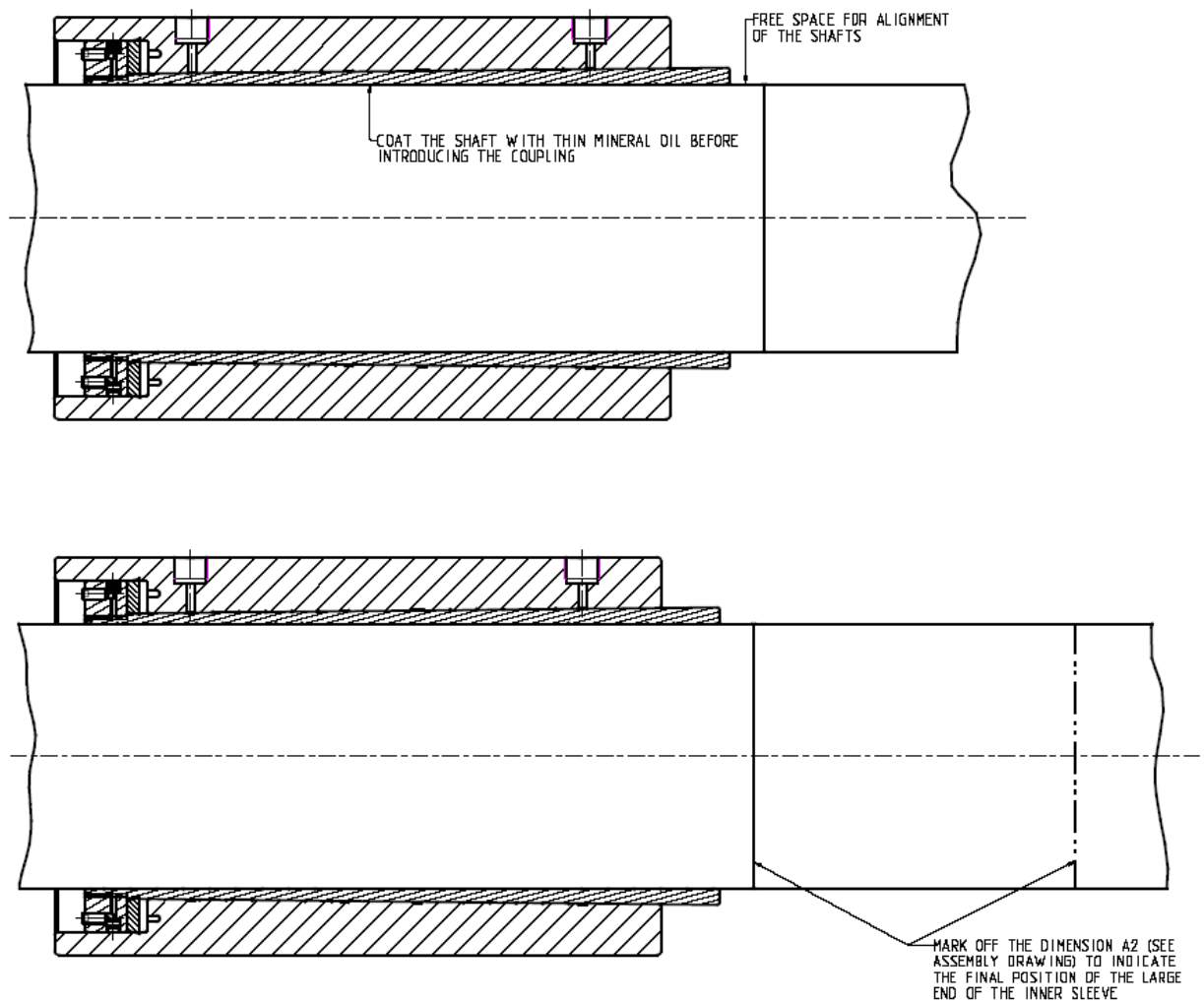
See enclosed assembly drawing for references.

Remove any burrs on the coupling seating on the shaft. **Clean and wash the inner sleeve bore and the coupling seating with white spirit, so that the anticorrosive agent is removed.**

7.1 Positioning of the Coupling on shaft.

Suspend the coupling opposite the shaft on which dimension A_2 has been marked off, ensuring that the large end of the inner sleeve faces this shaft and that the connection holes are at the top of the coupling. Coat the shaft with thin oil before introducing the coupling. Slide the coupling on, guiding it carefully to prevent it from damaging the shaft. Push the coupling on until so much of the seating emerges that the shafts can be aligned accurately.

NOTE The locking devices should be kept tightened while positioning the coupling on the shaft.

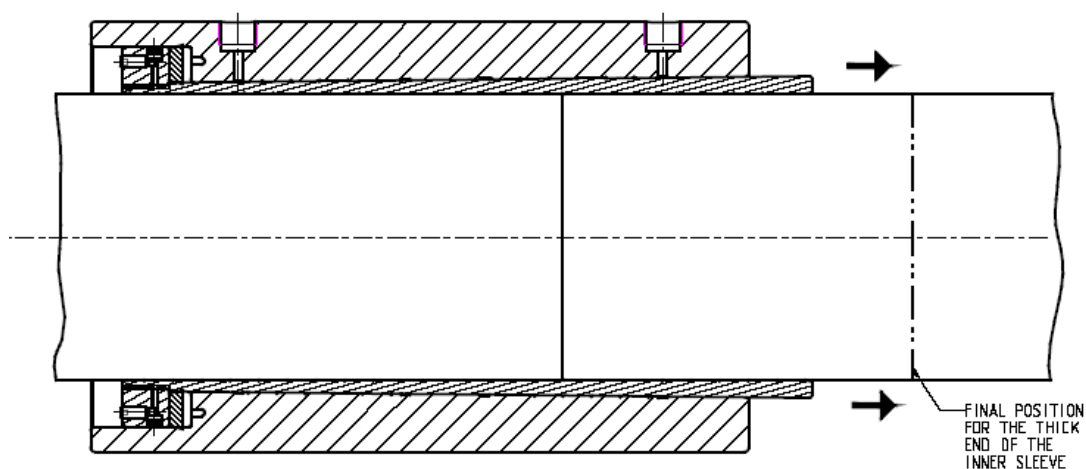


7.2

Align the shafts with precision, vertically and horizontally and ensure that the gap between the shaft ends is not more than 1% of the shaft diameter. Support the shafts and the coupling during the mounting process so that no misalignment appears. Coat the seating on the shaft with thin oil to prevent scraps on the shafts when sliding the coupling in position.

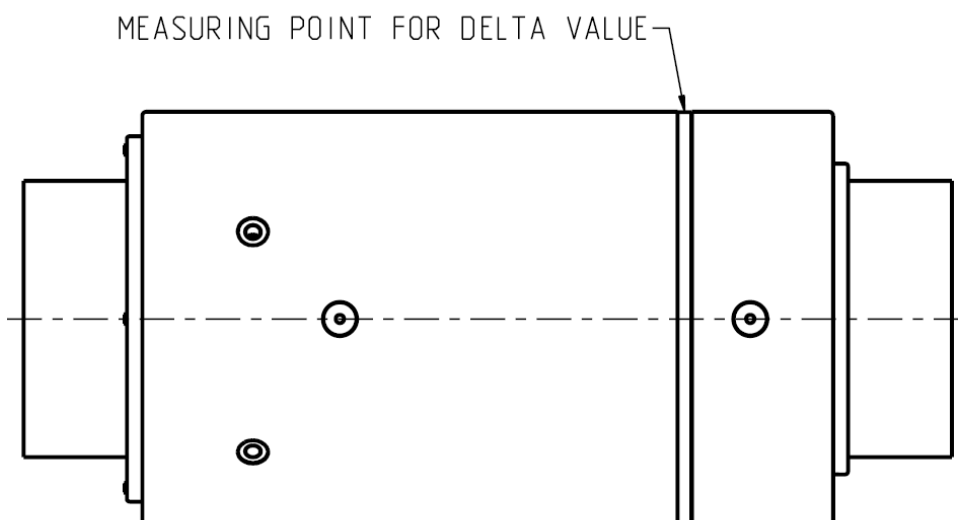
Slide the coupling back along the shafts until the large end face of the inner sleeve coincides with the A2 mark on the shaft.

NOTE The coupling must not weigh upon the shafts



7.3

When the coupling is in correct position and before mounting, measure the outside diameter of coupling and record it. The place for measuring is marked on the outside of the coupling with a shallow groove. (see assembly drawing for Δ value and position of the groove).



7.4 Drive up procedure

Position the coupling so that one of the two $\frac{1}{4}$ " plugs connected to the oil chamber is in top position (12⁰⁰ a clock). Couplings ≥ 700 has one $\frac{1}{2}$ " and one $\frac{1}{4}$ " hole and the $\frac{1}{2}$ " hole should be in top position. Unscrew the plugs and connect the low pressure pump to the lower $\frac{1}{4}$ " hole. Connect the high pressure injectors to the $\frac{3}{4}$ " holes on the coupling hub.

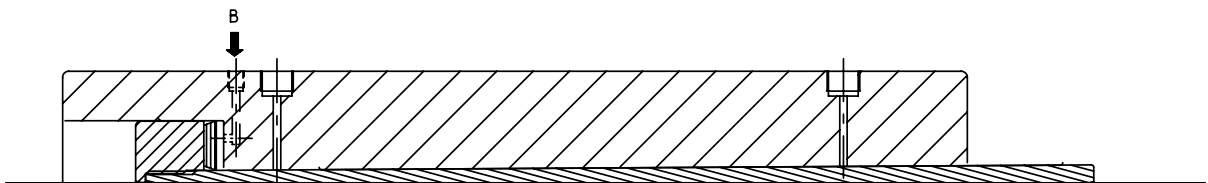
Calculate the final diameter of the coupling after drive up. Use the measured outside diameter + Δ value stamped on the coupling or see the assembly drawing for the Δ value.

Stainless steel coupling.

The stainless steel coupling is delivered with plastic plugs mounted and one steel plug is supplied for the venting hole ($\frac{1}{4}$ " or $\frac{1}{2}$ "). When the coupling is finally mounted the plastic plugs should be remounted.

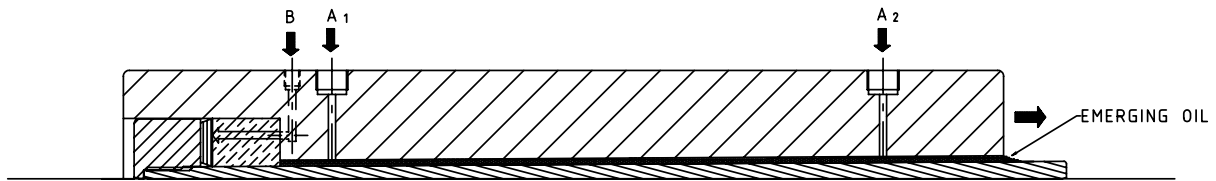
7.4.1 Couplings using 1 or 2 high pressure injectors (size 100 - 490)

Start pumping oil into the hydraulic chamber (B) until oil free from air bubbles escapes through the open $\frac{1}{4}$ " hole (or the $\frac{1}{2}$ " hole for larger couplings). Then close that hole with the plug.

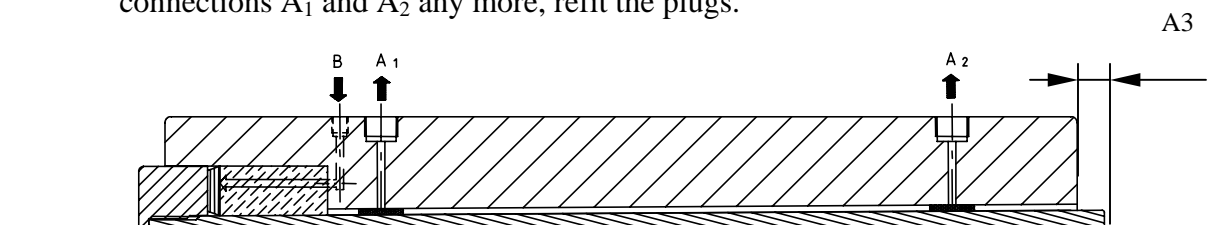


Begin working the high pressure injector connected to the $\frac{3}{4}$ " hole A₁ and then (if there is more than one injector) start working the high pressure injector connected to A₂. Work the high pressure pumps with even strokes until oil emerges around the periphery at the large end of the inner sleeve. Continue pumping for a couple of minutes.

Start the pump connected to the oil chamber (B) to begin the drive up of the outer sleeve. **It is important to continue working the high pressure injectors with even strokes during the entire drive up operation.** If it is necessary to refill the container of injector 226400 during the drive up procedure, always stop the pump connected to the oil chamber first. After refilling, work the injectors first until oil emerges again around the periphery at the large end of the inner sleeve. Continue the drive up procedure until the diameter of the outer sleeve has increased by the dimension Δ see 7.4. As the Δ value should be confirmed after the oil is drained out, the value measured before draining should be 5% higher.

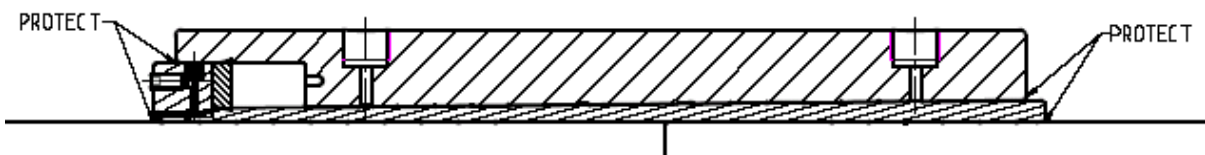


Stop the pump connected to the hydraulic chamber B, but keep the pressure. Open the return valves on the injectors A₁ and A₂. Keep the pressure (B) in the hydraulic chamber. After 10 minutes, measure the Δ value again, to confirm the correct diameter increase according to 7.4. Open the return valve on the pump connected to the oil chamber (B) slowly to release the pressure, make sure the outer sleeve not is moving. Remove the injectors connected to the $\frac{3}{4}$ " holes A₁ and A₂. Disconnect the pump connected to the oil chamber (B) and refit the plug. When oil is not draining out from connections A₁ and A₂ any more, refit the plugs.



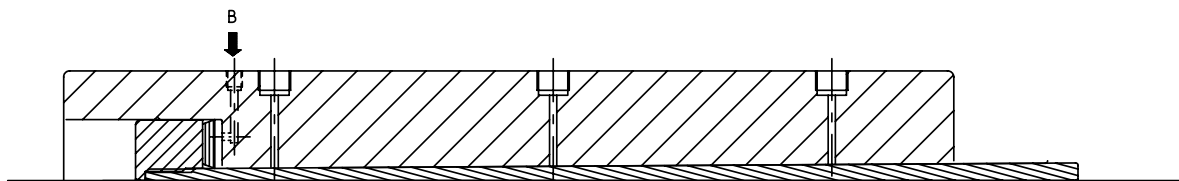
After this first mounting of the coupling the distance A3 (distance from the end of the inner sleeve to the end of the outer sleeve) should be measured and recorded, this can be used as a confirmation at the next mounting of the coupling instead of measuring the Δ value increase.

Protect the ends of the coupling at the shaft and the clearance between the nut and the outer sleeve using silicon or similar protective. This will prevent moisture from penetrating the coupling parts. Tighten the locking device as described in chapter 5.2.



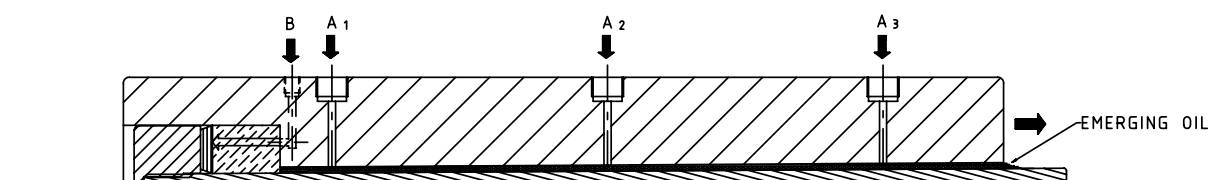
7.4.2 Couplings using 3 high pressure injectors (size >500).

Start pumping oil into the hydraulic chamber (B) until oil free from air bubbles escapes through the open $\frac{1}{4}$ " hole, or from the open $\frac{1}{2}$ " hole on coupling ≥ 700 . Then close that hole with the plug.



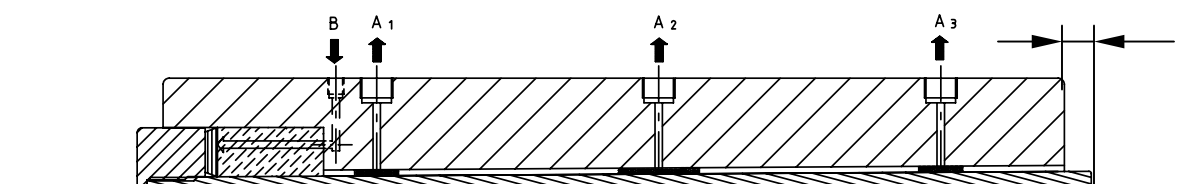
Begin working the high pressure injector connected to the $\frac{3}{4}$ " hole A_2 located in the middle of the coupling. When oil emerges around the periphery at the large end of the inner sleeve, start injection also with the other two injectors A_1 and A_3 . Work all injectors for a couple of minutes.

Start the pump connected to the oil chamber to begin the drive up of the outer sleeve. **It is important to continue working the high pressure injectors with even strokes during the entire drive up operation.** If it is necessary to refill the container of injector 226400 during the drive up procedure, always stop the pump connected to the oil chamber first. After refilling, work the injectors first until oil emerges again around the periphery at the large end of the inner sleeve. Continue the drive up procedure until the outer sleeve has increased by the dimension Δ see 7.4. As the Δ value should be confirmed after the oil is drained out, the value measured before draining should be 5% higher.



Stop the pump connected to the hydraulic chamber B, but keep the pressure. Open the return valves on the injectors A_1 , A_2 and A_3 . Keep the pressure (B) in the hydraulic chamber. After 10 minutes, measure the Δ value again, to confirm the correct diameter increase according to 7.4. Open the return valve on the pump connected to the oil chamber (B) slowly to release the pressure, make sure that the outersleeve not is moving. Remove the injectors connected to the $\frac{3}{4}$ " holes A_1 , A_2 and A_3 . Disconnect the pump connected to the oil chamber (B) and refit the plug. When oil is not draining out from connections A_1 , A_2 and A_3 any more, refit the plugs.

A3



After this first mounting of the coupling the distance A3 (distance from the end of the inner sleeve to the end of the outer sleeve) should be measured and recorded, this can be used as a confirmation at the next mounting of the coupling instead of measuring the Δ value increase.

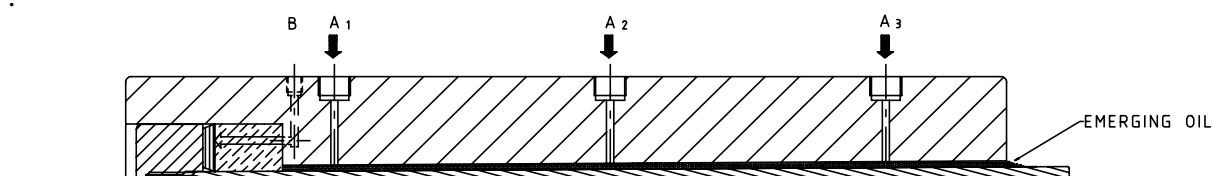
Protect the ends of the coupling at the shaft and the clearance between the nut and the outer sleeve using silicon or similar protective. This will prevent moisture from penetrating the coupling parts. Tighten the locking device as described in chapter 5.2.



8 DISMOUNTING INSTRUCTIONS

- 1 Support the shafts on both sides of the coupling. Release the locking devices on the coupling, see chapter 5.2.
- 2 Connect the pump and injectors as for mounting and fill up the oil chamber with oil as the procedure for mounting, see chapter 7.4. Connect also the extra return pipe to the 1/2" or the other 1/4" vent hole at the hydraulic chamber.
- 3 Pressurise the oil chamber to ~ 10 MPa and start the high pressure injectors following the procedure for mounting. See 7.4.
- 4 Continue to work the high pressure injectors until oil emerges around the periphery at the large end of the inner sleeve. If the outer sleeve moves relatively the inner sleeve taper while the pressure in the oil chamber increases also indicates that there is a satisfying oil film. Open the return valve on the pump connected to the hydraulic chamber and at the same time the valve on the extra return pipe, this while the injectors are working, and the outer sleeve will slide down on the inner sleeve. **Work the high pressure injectors until a fully dismantled position is obtained in order to maintain a good oil film between the sleeves**

NOTE Make sure that the A3 dimension is not decreasing while dismantling the coupling



9 REPLACING THE OIL CHAMBER SEALING

The OKXC coupling is a unit, which normally should not be disassembled. If it however is necessary because of a damaged sealing, the nut must be removed first.

9.1 Coupling removed from the shaft

Release the locking device in the nut as described in chapter 5.2.

Unscrew the nut and remove the sealing using a tool with rounded edges to avoid damaging the surfaces. Replace it with the new sealing and guide it carefully over the inner sleeve threads not to destroy the sealing edge. Push it against the bottom of the chamber. Correct mounted the sealing outer edge and inner edge will have good contact against the bottom and the face will have a convex form.

Remount the nut and tighten it properly. With a blast of compressed air in one ¼ " hole, the sealing will be forced in position. Tighten the locking device (see 5.2).

9.2 Coupling mounted on the shaft.

If there is a leakage from the oil chamber when preparing for dismounting procedure, it is necessary to replace the sealing.

Follow the above mentioned procedure for removing the coupling nut and removal of the sealing. Place the nut on the shaft to get good access to the chamber. The new sealing must be cut to get it around the shaft. Do this with a long knife so that it will be a straight and smooth cut. Place the sealing around the shaft with the smallest outer diameter facing the nut. The flat surface of the nut can be used as a template. Use a cyanoacrylat glue for rubber to glue the divided surfaces together. Place the sealing in the chamber guiding it carefully over the threads and 10mm up on the taper of the inner sleeve. Try to get the sealing as straight and flat as possible. Remount the nut and position the sealing with a blast of compressed air in one of the ¼ " hole.

WARNING! NEVER USE HIGH PRESSURE INJECTORS (A₁-A₃) IF THE NUT HAS BEEN REMOVED

10 ASSEMBLY DRAWING

Pos.	Benämning	Artikelnr.
1	Slangfäste	1817413
2	Snabbkoppling	1817464
3	Snabbkopplingsnippel	1817465
4	Ventil	1817077
5	Filterregulator inkl. manometer	EAW2000-F02-X64 K8-10-40
6	Nippel	02024-R4
7	PML Fettpump	9650
8	Nippel	02024-R4+0203-6-4
9	T-stycke	0143-4
10	Fettslang L 3 m.	GR2T1/4+03500404x2 +0002-4x2
11	Nippel	1700/04/04
12	Ventil	BKH R1/4
13	Slangfäste	3822-4-6
14	Slang L 1m.	OL10040 10 1m
15	Fett svivel 1/4"	1100-A
16	Gummistålbricka	GBR 1/4"

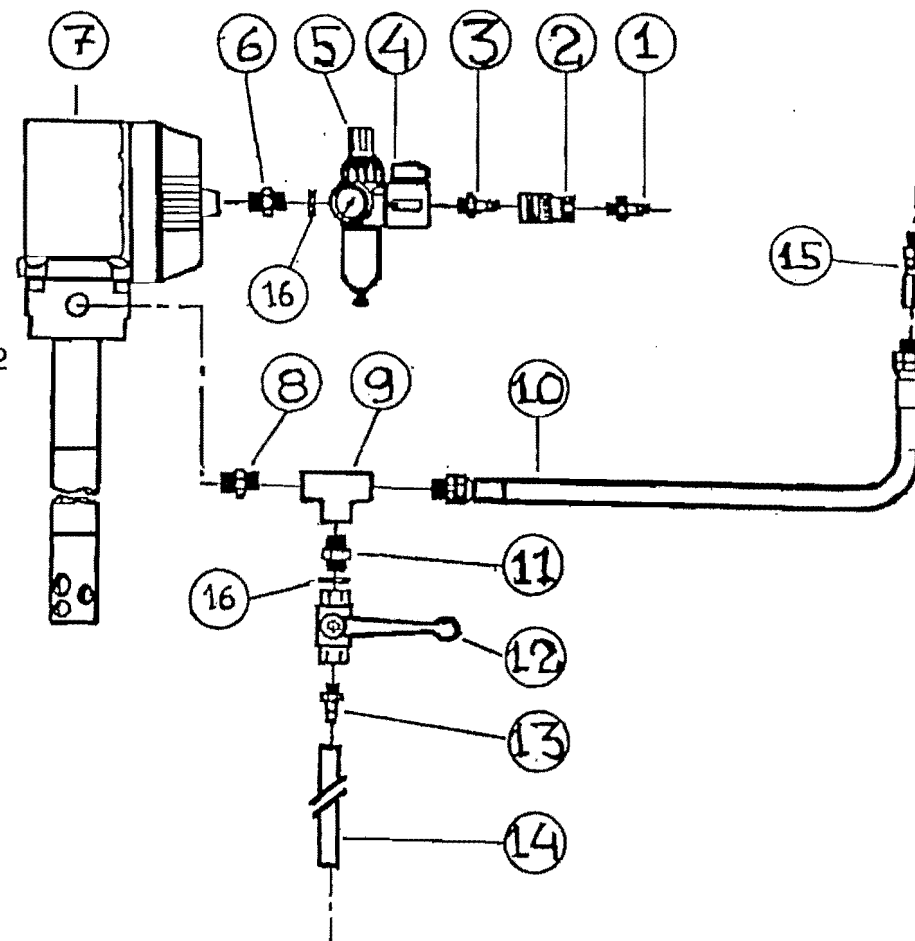
Leveransutförande:

Pos 1-6+16 monteras.

Pos 8-9+11-14+16 monteras i pump

Pos 10+15 monteras.

Delmonteringar packas i pumpkartong.



Kartong märkes med 071056 P17D-14

KaMeWa Högtryckspump

Eurolube AB
Box 55 132 22 Saltsjö-Boo



Service Guide

49036-E

9611
9650
338043-J1

High-Pressure Stripped Pump

Description

The major components of these stripped pump models consist of an air-operated motor and a pump tube. The air motor connects directly to the single-acting reciprocating pump tube.

These high-pressure stripped pumps (50:1 ratio) are designed to deliver a range of greases [up to NLGI # 3] and operate directly from their original drums or bulk containers.

Each pump model is designed with a pump tube length to accommodate different size containers. See Figure 1.

Specifications

Air Motor

Piston Diameter x Stroke		Air Inlet	Maximum Air Pressure	
Inches	Centimeters		psi	Bars
2-15/16 x 3	7.5 x 7.6	1/4" NPTF (F)	150	10.3
For details on the air motor, refer to Service Guide SER 338066-A1				

Pump Tube

Material Outlet	Max. Material Pressure		Delivery/Minute (Approximate)*		Displacement per Cycle	
	psi	Bars	Pounds	Kilograms	In ³	Cm ³
3/8" NPTF	7500	517	3	1.4	0.39	6.39
* For detailed information, refer to Figure 3						

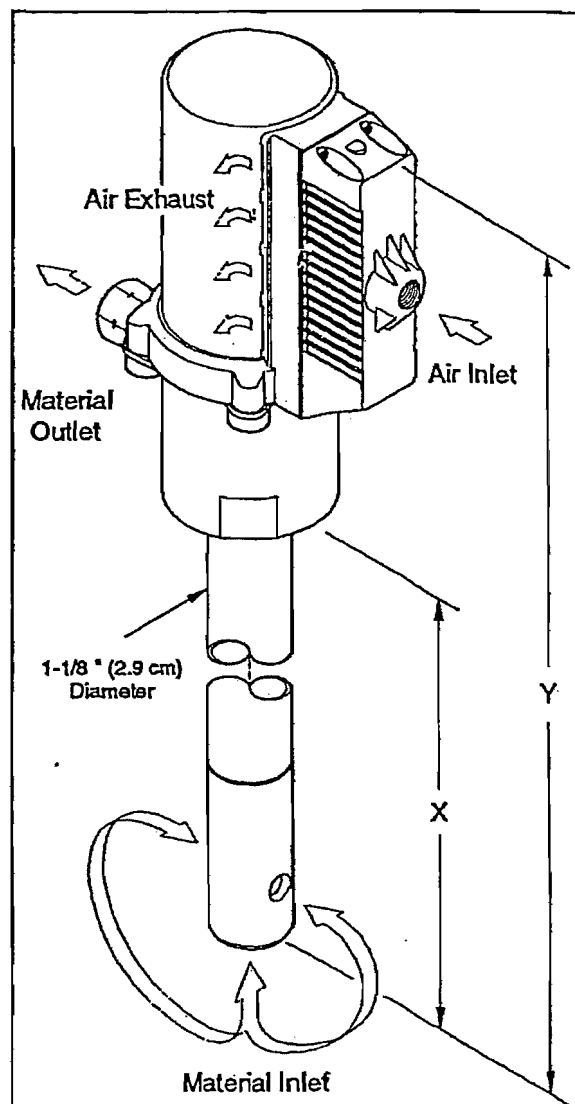
Table 1 High-Pressure Stripped Pump Specifications

Package Models

The usage for each model of stripped pump is indicated below.

Stripped Pump Model	Package Model
9611	9611-H, 9611-Z
9650	9650-A, 9651, 9651-S, 9651-T
338043-J1	9611-A, 9611-B

Table 2 High-Pressure Stripped Pump Usage



Stripped Pump Model	Container	X		Y	
		Inches	Cm	Inches	Cm
9611	35 pounds	13.75	34.9	22	55.9
9650	120 pounds	27.75	70.5	36	91.4
338043-J1	70 pounds	17.68	45	25.9	65.8

Figure 1 High-Pressure Stripped Pump Models 9611, 9650, and 338043-J1

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PO Box 473515, Charlotte, North Carolina 28247-3515

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SER 9611/9650
Revision (12-96)

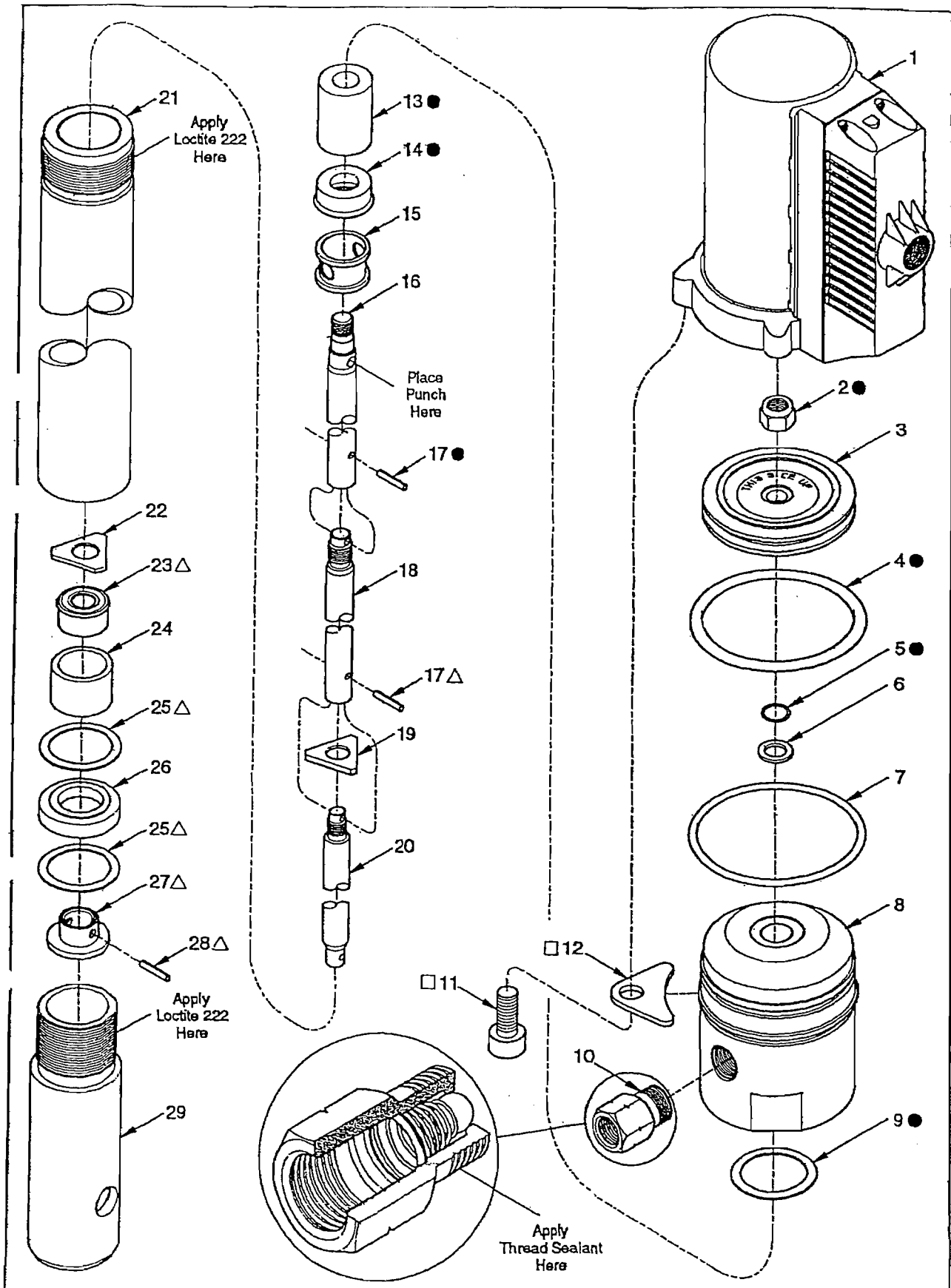


Figure 2 High-Pressure Stripped Pump Models 9611, 9650, and 338043-J1 - Exploded View

Item No.	Part No.	Description	Qty	Notes	Numeric Order Part # (Item #)
1		Motor Assembly, Air	1	See SER 338066-A1	51929 (2)
2	51929	Nut, Elastic Stop, 3/8 " -24	1	●	171000-7 (5)
3	338111	Piston, Air	1		171000-103 (4)
4		O-Ring, 2-5/8 " ID x 3 " OD	1	●	171003-10 (7)
5	171000-7	O-Ring, 3/8 " ID x 1/2 " OD	1	●	171031-5 (17)
6	338109	Washer, 3/8 "	1		171032-3 (28)
7	171003-10	O-Ring, 2-3/4 " ID x 3 " OD	1		171892 (11)
8	338515	Body	1		172190-10 (23)
9		Gasket, 0.90 " ID (Aluminum)	1	●	172190-26 (14)
10	338512-A	Valve Assembly, Check	1		338041 (12)
11		Bolt, 5/16 " -18 x 1/2 "	4	□	338056 (22)
12		Keeper	4	□	338066-A1 (1)
13		Bearing (Brass)	1	●	338071 (24)
14		Seal, 1/2 " ID x 7/8 " OD	1	●	338092-1 (21)
15	338094	Ring, Lantern	1		338092-2 (21)
16	338108	Rod, Upper	1		338092-7 (21)
17		Pin, Roll, 5/64 " Dia. x 1/2 " Long	2	●△	Qty of 1 in each kit 338093 (29)
18	338099-1	Extension, 6.66 " Long	1		Model 9611 338094 (15)
	338099-2	Extension, 20.66 " Long	1		Model 9650 338095 (13)
	338099-7	Extension, 10.59 " Long	1		Model 338043-J1 338096 (9)
19	338104	Guide	1		338098 (20)
20	338098	Rod, Primer	1		338099-1 (18)
21	338092-1	Tube, 11.54 " Long	1		Model 9611 338099-2 (18)
	338092-2	Tube, 25.54 " Long	1		Model 9650 338099-7 (18)
	338092-7	Tube, 15.47 " Long	1		Model 338043-J1 338100 (25)
22	338056	Stop	1		338101 (26)
23		Seal, 0.182 " ID x 0.532 " OD	1	△	338102 (27)
24	338071	Valve, Foot	1		338104 (19)
25		Gasket, 0.75 " ID (Aluminum)	2	△	338108 (16)
26	338101	Seat	1		338109 (6)
27	338102	Disc, Primer	1	△	338111 (3)
28		Pin, Roll, 3/32 " Dia. x 3/8 " Long	1	△	338512-A (10)
29	338093	Body, Primer	1		338515 (8)

Legend:
 Part numbers left blank (or in *italics*) are not available separately
 ●△□ designates a repair kit item

Repair Kits

Part No.	Kit Symbol	Description
393573-1	●	Kit, Repair (for Upper Pump Tube Assembly) [Includes tube of 393590 Teflon Grease]
393574	△	Kit, Repair (for Lower Pump Tube Assembly)
393641	□	Kit, Repair, Air Motor Keeper and Screw
393530-10		Kit, Seal [includes five (5) of item number 23]
393530-26		Kit, Seal [includes five (5) of item number 14]

Accessories

Part Number	Description
326750-F1	Bung Adapter, 2" NPTF (m)

Table 3 High-Pressure Stripped Pump Accessory Component

Preventive Maintenance

Refer to section entitled **Overhaul** for the procedures necessary to perform maintenance.

Daily	Weekly	Monthly	Yearly
Wipe Exterior with Clean Cloth	Inspect for Air and/or Material Leakage		

Table 4 High-Pressure Stripped Pump Preventive Maintenance Schedule

Performance Curves

A pump's ability to deliver material is based on the pressure (psi/Bars) and quantity (cfm/lpm) of air supplied to the motor and the amount of material discharge [back] pressure to be overcome within the system.

This chart contains curves based on three different air pressures. The curves relate delivery in pounds (kilograms) per minute (X axis) to air consumption in cubic feet (liters) per minute (right Y axis) and to material discharge pressure in psi/Bars (left Y axis).

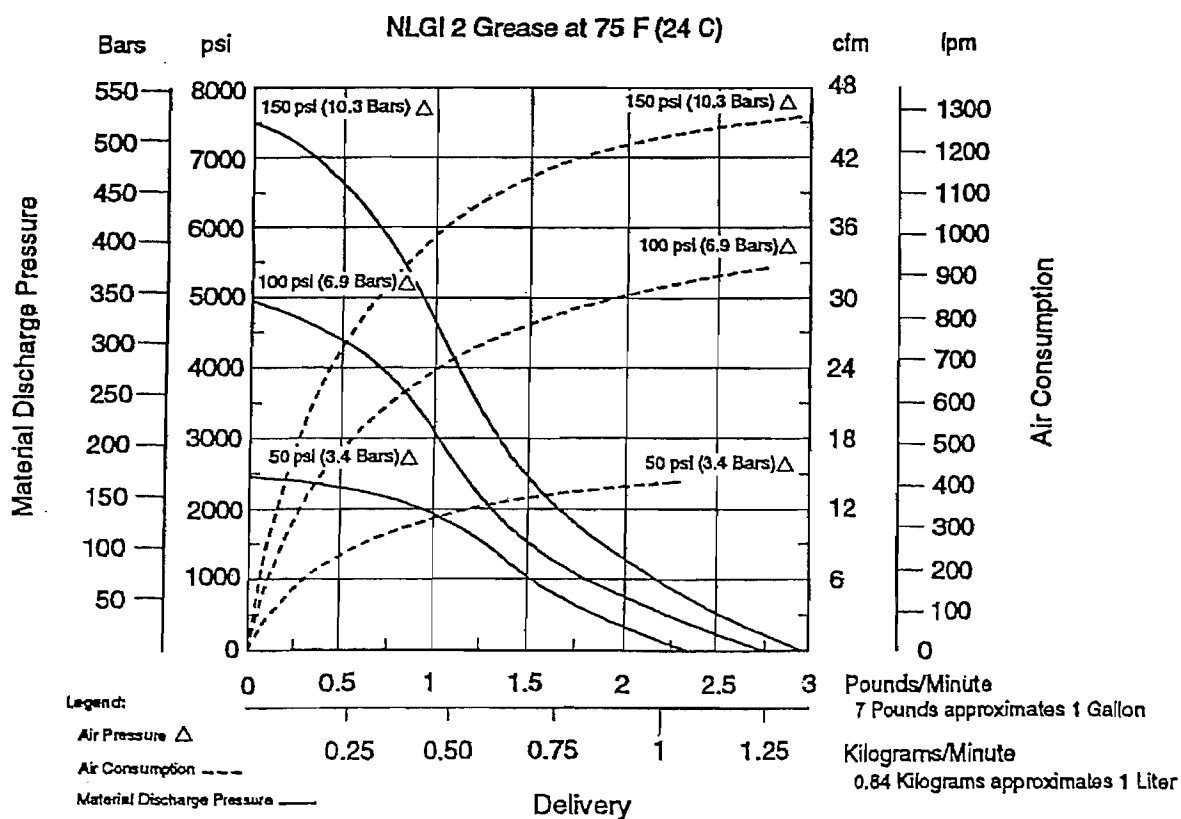
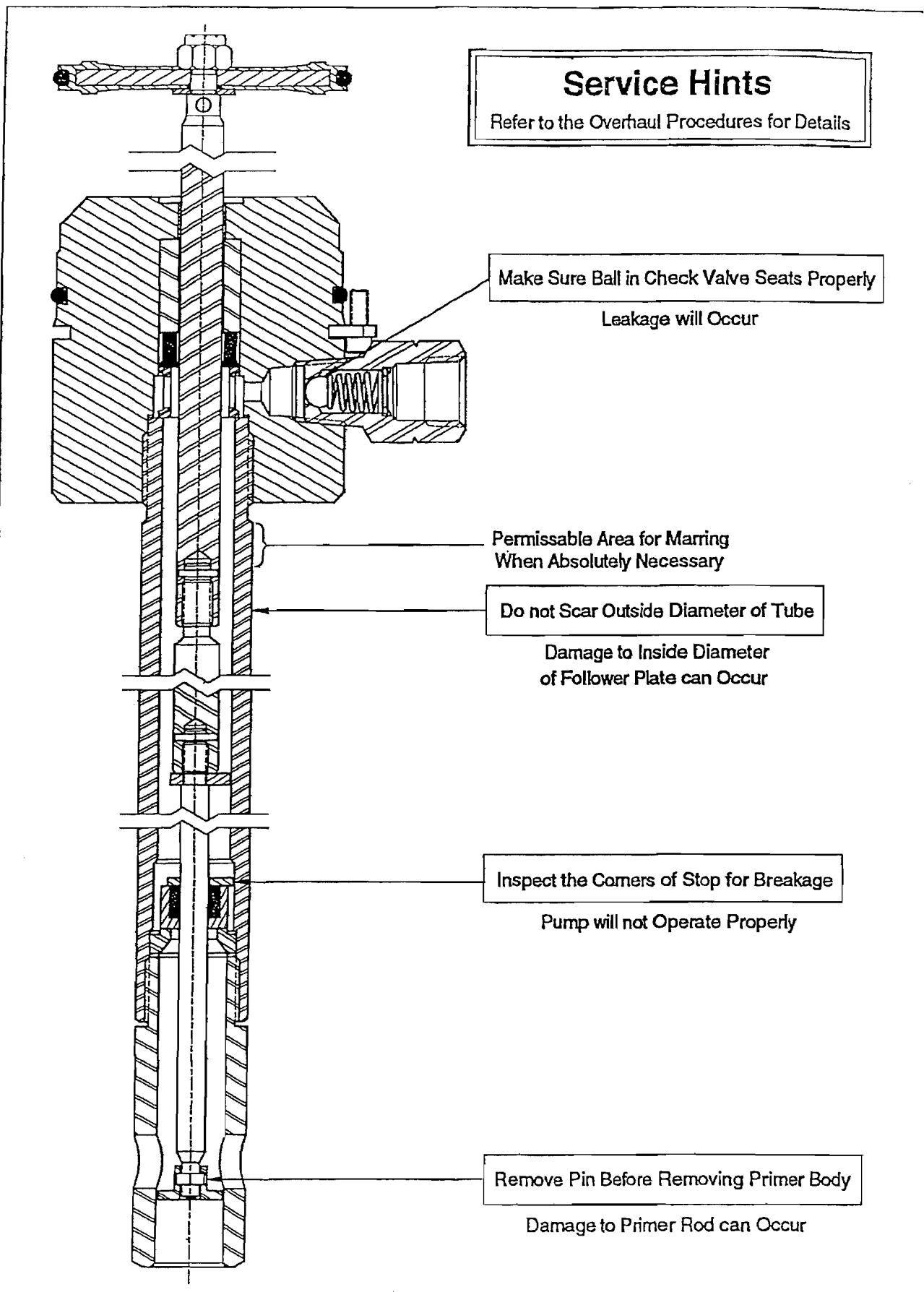


Figure 3 Delivery versus Discharge Pressure and Air Consumption



Overhaul

NOTE: Refer to Figure 2 for component identification on all overhaul procedures.

Prior to performing any maintenance procedure, the following safety precautions must be observed. Personal injury may occur.



WARNING

Do not use halogenated hydrocarbon solvents such as methylene chloride or 1,1,1-trichloroethane in this pump. An explosion can result within an enclosed device capable of containing pressure when aluminum and/or zinc-plated parts come in contact with halogenated hydrocarbon solvents.

Release all pressure within the system prior to performing any overhaul procedure.

- **Disconnect the air supply line from the pump motor.**
- **Into an appropriate container, operate the control valve to discharge remaining pressure within the system.**

Never point a control valve at any portion of your body or another person. Accidental discharge of pressure and/or material can result in injury. Read each step of the instructions carefully. Make sure a proper understanding is achieved before proceeding.

Removal

Remove the pump assembly from the package model.

- Refer to the applicable package model Service Guide for detailed information. See Table 2.

Disassembly

Separate Air Motor from Pump Tube

1. Clamp the pump assembly in a soft-jaw vise at Body (8).
2. Remove Bolts (11) that secure the Body to Air Motor Assembly (1).
 - Remove Keepers (12) from the Body.
3. With a side-to-side motion, pull the Air Motor assembly from the Body.
 - Lubricate O-Ring (7) with oil to ease separation.

Pump Tube

4. Remove Nut (2) that secures Air Piston (3) to Upper Rod (16).

- Remove the Air Piston from the Rod.

NOTE: Place an appropriate size punch or other suitable tool into the hole of the Upper Rod. See Figure 2.

5. Remove O-Ring (5) and Washer (6) from the Upper Rod.
6. Remove O-Ring (4) from the Air Piston.
7. Remove Roll Pin (28) that secures Primer Disc (27) to Primer Rod (20).
 - Use an appropriate size punch.

NOTE: Position the rod assembly as required to align the Roll Pin with the hole in Primer Body (29).

8. Remove the Primer Disc from the Primer Rod.
9. Break the connection of Tube (21) from the Body.
 - Place an appropriate size tool into the hole of the Primer Body. At the same time turn the Tube with a strap wrench.
10. Unscrew Primer Body (29) from the Tube.
 - Prevent the rotation of the Tube with the use of the strap wrench.
11. Pull the entire rod assembly from the bottom of the Tube.
12. Unscrew the Tube from the Body.

Rod Assembly

13. Remove Gasket (25), Seat (26), additional Gasket (25), Foot Valve (24) [with Seal (23)], and Stop (22) from the Primer Rod.
 - Remove the Seal from the Foot Valve.
14. Remove Roll Pin (17) that secures Extension (18) to the Primer Rod.
 - Use a punch and a small hammer.
15. Unscrew the Primer Rod from the Extension.
16. Remove Guide (19) from the Primer Rod.
17. Remove Roll Pin (17) that secures Upper Rod (16) to the Extension as required.
 - Use a punch and a small hammer.
18. Unscrew the Extension from the Upper Rod.

Body

19. Remove Gasket (9) from the Body.
20. Remove Lantern Ring (15), Seal (14), and Bearing (13) from the Body.
21. Remove O-Ring (7) from the Body.
22. Unscrew Check Valve Assembly (10) from the Body.

Clean and Inspect

NOTE: Use the appropriate repair kit for replacement parts. Make sure all the components are included in the kit before discarding used parts.

1. Clean all metal parts in cleaning solvent. The solvent should be environmentally safe.
2. Inspect all parts for wear and/or damage.
 - Replace as necessary.
3. Inspect Air Piston (3) for fatigue cracks.
 - Replace as necessary.
4. Inspect Upper Rod (16) and Primer Rod (20) closely. Use a magnifying glass to detect any score marks on the Rods.
 - Replace as necessary.
5. Closely inspect the mating surfaces of Foot Valve (24) and Seat (26) for any imperfections. Ensure a smooth and clean contact is obtained.
6. Fill Check Valve Assembly (10) with solvent. Make sure no leakage occurs.
7. Inspect the corners of Stop (22) for breakage. Place the Stop into the bottom of Tube (21). Make sure the Stop is secure within the Tube when pressure is applied.

Assembly

NOTE: Prior to assembly, certain components require lubrication. Refer to Table 5 for details.

Pump Tube

NOTE: Refer to Figure 4 for a section view of the pump tube assembly.

1. Install O-Ring (7) onto Body (8).
2. Install and seat Bearing (13) and Seal (14) [heel end first] into the Body.
3. Install Lantern Ring (15) into the Body.
4. Screw Extension (18) into Upper Rod (16).
 - Make sure the hole in the Extension aligns with the hole in the Upper Rod.
5. Install Roll Pin (17).
 - Use a small hammer.
6. Install Guide (19) onto the threaded end of Primer Rod (20).
7. Screw the Primer Rod assembly hand-tight into the Extension.

IMPORTANT: Do not back-off the Primer Rod more than 1/2 turn.

8. Unscrew the Primer Rod until the hole in the Primer Rod aligns with the hole in the Extension.
9. Install Roll Pin (17).
 - Use a small hammer.
10. Install the Rod assembly [chamfer end first] into the bottom of the Body.
 - Use care passing the Seal.

Item No. on Figure 2	Description	Item No. on Figure 2	Description
Clean Oil			
4	O-Ring, 2-5/8" ID x 3" OD	14	Seal, 1/2" ID x 7/8" OD
5	O-Ring, 3/8" ID x 1/2" OD	23	Seal, 0.182" ID x 0.532" OD
7	O-Ring, 2-3/4" ID x 3" OD		
Magnalube-G Teflon Grease *			
Coat the Inside Diameter of the Air Motor Assembly			
*.Part number 393590 is a 0.75 ounce (21.8 gm) tube of Magnalube-G Teflon grease			

Table 5 Lubricated Components

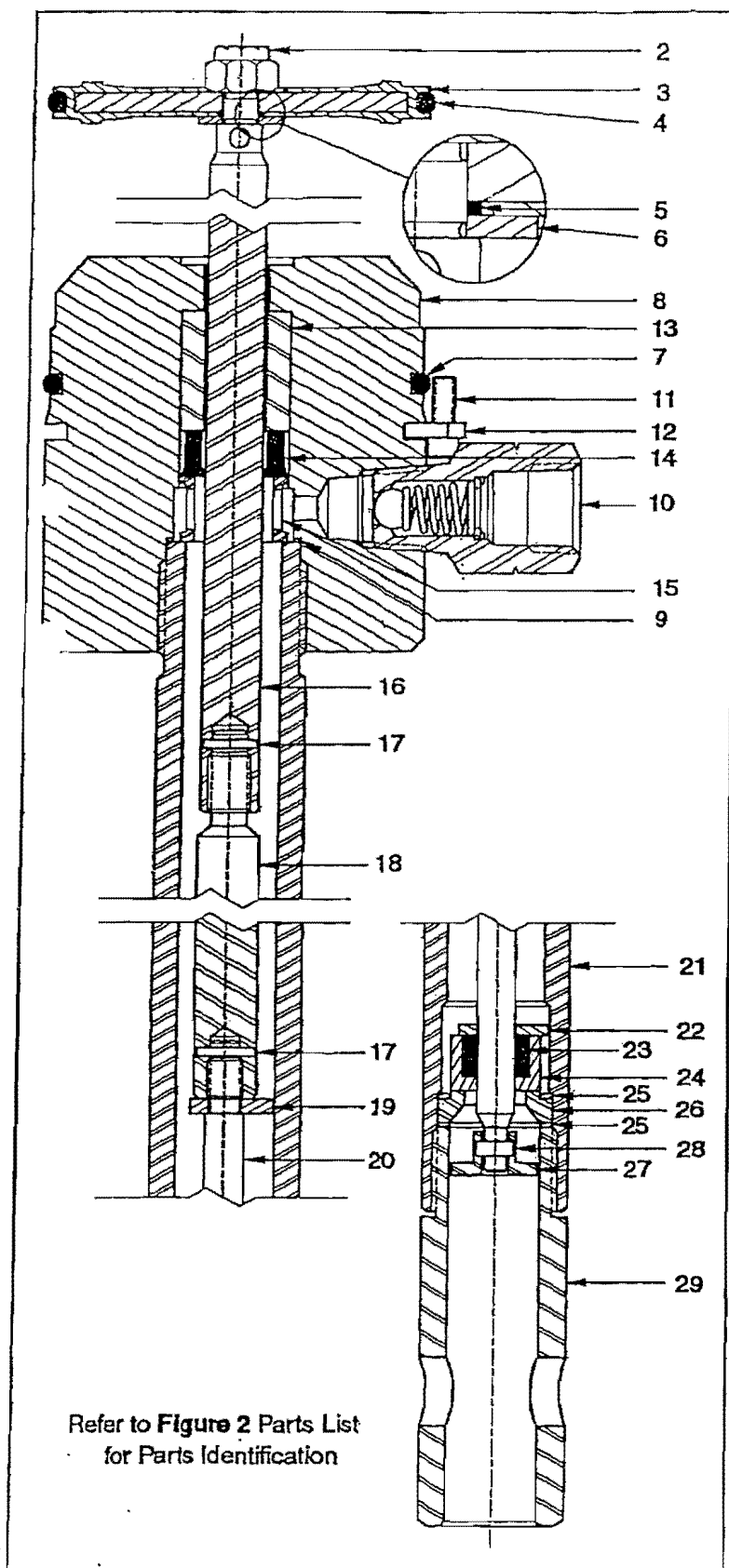


Figure 4 Pump Tube Assembly 338087-A1, B1, and H1
Section View

11. Install and seat Gasket (9) into the Body.

IMPORTANT: If a primer is used with Loctite 222, the curing time is greatly reduced.

12. Screw Tube (21) [with Loctite 222] into the Body. See Figure 2.

- Follow the thread sealant manufacturer's recommendations
- Do not tighten at this time.

13. Install Stop (22) onto the Primer Rod.

14. Install Seal (23) [heel end first] into Foot Valve (24).

15. Install the Foot Valve assembly (Seal first) onto the Primer Rod.

16. Install and seat Gasket (25) into the Tube.

17. Install Seat (26) [stepped end first] into the Tube:

18. Install additional Gasket (25) onto the Seat.

19. Screw Primer Body (29) [with Loctite 222] into the Tube. See Figure 2.

- Follow the thread sealant manufacturer's recommendations

20. Place an appropriate size tool into the hole of the Primer Body.

- Tighten the Primer Body into the Tube and at the same time the Tube into the Body.
- Make sure to properly crush all Gaskets.

21. Position the rod assembly as required so the hole in the Primer Rod is visible through the hole in the Primer Body.

22. Install Primer Disc (27) onto the Primer Rod.

- Make sure the hole in the Primer Disc aligns with the hole in the Primer Rod.

23. Install Roll Pin (28).

- Use a small hammer and a punch.

Air Piston

24. Install Washer (6) and O-Ring (5) onto the Upper Rod.

25. Install O-Ring (4) onto Air Piston (3).

26. Place the Air Piston (observe THIS SIDE UP) on top of the Upper Rod.
27. Install Nut (2) that secures the Air Piston to the Upper Rod.
 - Tighten the Nut securely.

NOTE: Place an appropriate size punch or other suitable tool into the hole of the Upper Rod. See Figure 2.

28. Screw Check Valve Assembly (10) [with thread sealant] into the Body.
 - Tighten the Check Valve securely.

Attach Air Motor to Pump Tube

29. Clamp the Body securely in a soft-jaw vise.
30. Install Air Motor Assembly (1) squarely onto the Body.
 - Use care passing the O-Ring.
 - Make sure the Check Valve Assembly orients properly with the inlet of the Air Motor.
31. Install Keepers (12) into the groove of the Body.
 - Make sure the holes align with the Air Motor Assembly.
32. Install Bolts (11) that secure the Body to the Air Motor Assembly.
 - Tighten the Bolts evenly and securely in a crisscross pattern.

Bench Test and Operation

1. Slowly supply air pressure [not to exceed 15 psi (1 Bar)] to the pump's motor.
 - The pump assembly should cycle.

If the pump assembly does not cycle, refer to the **Troubleshooting Chart** for details.

With air pressure at zero:

2. Connect a product hose to the pump's Check Valve Assembly.
 - Direct the hose into an appropriate collection container.
3. Place the pump in the product to be dispensed.
4. Slowly supply air pressure to the pump's motor.
5. Allow the pump to cycle slowly until the product is free of air.

If the pump assembly does not prime, refer to the **Troubleshooting Chart** for details.

WARNING



Should leakage occur anywhere within the system, disconnect air to the motor. Personal injury can occur.

With air pressure at zero:

6. Attach a control valve to the outlet hose of the pump.
 - Make sure the nozzle on the control valve is open.
7. Slowly supply air pressure to the pump's motor.
8. Allow the pump to cycle slowly until the product is once again free of air.
9. Set the air pressure to 100 psi (6.9 Bar).
10. Operate the control valve into a container.
11. Shut off the control valve.
 - Visually inspect the pump for external leaks.
 - The pump should not cycle more than once or twice in one hour.

If the pump does not stall, refer to the **Troubleshooting Chart** for details.

12. Check the motor for air leakage.

If the motor leaks, refer to the **Air Motor Service Guide** for details.

IMPORTANT: Make sure to reset the air pressure to the required operating pressure.

Installation

Additional items that should be incorporated into the air piping system are listed in Table 6.

Part Number	Description
5604-2	Moisture Separator
7604-B	Regulator and Gauge

Table 6 Air Line Components

Troubleshooting Chart

Pump Indications	Possible Problems	Solution
Pump does not cycle	1. Air motor not operating properly 2. Pump tube jammed and/or contains loose components 3. Insufficient air pressure	1. Inspect air motor and rebuild or replace as necessary. Refer to SER 338066-A1 2. Rebuild pump tube 3. Increase air pressure
Pump will not prime	1. Excessive cycling speed 2. Pump leaking internally	1. Reduce air pressure 2. See Internal Leaks
Pump cycles rapidly	Product source empty	Replenish product
Pump will not stall (cycles more than once or twice per hour)	1. Pump requires break-in period 2. Pump leaking internally 3. Pump leaking externally 4. Distribution system leaking	1. Operate the pump against moderate fluid pressure for up to one hour 2. See Internal Leaks 3. See External Leaks 4. Correct leak
External Leaks		
Product leakage visible at bottom of Body (8)	1. Tube (21) not sufficiently tight 2. Damaged Gasket (9)	1. Tighten Tube (21) into Body (8) 2. Separate Tube (21) from Body (8) and replace Gasket (9)
Product leakage visible between Tube (21) and Primer Body (29)	1. Primer Body (29) not sufficiently tight 2. Damaged Gasket (25)	1. Tighten Primer Body (29) into Tube (21) 2. Separate Primer Body (29) from Tube (21) and replace Gasket (25)
Internal Leaks		
Pump does not prime or cycles continuously, or slowly (once or twice/hour)	1. Foreign material between Foot Valve (24) and Seat (26) 2. Foreign material in Check Valve Assembly (10) 3. Worn or damaged Foot Valve (24) 4. Worn or damaged Seat (26) 5. Worn or damaged Check Valve Assembly (10) 6. Worn or damaged Seal (23) 7. Worn or damaged Primer Rod (20) 8. Primer Disc (27) missing	Locate and eliminate source of foreign material. Disassemble pump tube, clean, inspect, and replace worn or damaged components.
Product leakage visible at Air Motor Assembly (1) exhaust	1. Worn or damaged Seal (14) 2. Worn or damaged Upper Rod (16)	Separate Tube (21) from Body (8) and replace worn or damaged component(s).

Changes Since Last Printing

Initial Release



Service Guide

49037-E

338066-A1
338066-C1

Pneumatic Logic Air Motor

Description

The air motors in the model 338066 series power a variety of fluid and material reciprocating pumps.

The pump tube assembly is secured to the motor with bolts. The bolts retain keepers that hold the body of the pump tube to the mounting ring of the air motor. See Figure 3.

Models 338066-A1 and 338066-C1

The difference between these models is the standard of thread for the air inlet. Refer to Table 1.

CAUTION

To comply with the warranty, an air line lubricator must not be used with this air motor.* The motor is packed with Teflon lubricant (part number 393590) and requires no additional lubrication except during service.

A moisture separator/filter should be used to prevent contamination and the washout of lubricant.

Operation

The designation pneumatic motor logic (PML) is derived from the method of controlling movement of the components within the motor's valve assembly.

Pneumatically actuated pilot valves (one at each end of a spool valve) cause the spool valve to shift. The spool valve directs air pressure to one side of the motor's piston and exhausts air from the opposite side.

* For icing conditions, an air line lubricator is permissible. The lubricator must deliver an ethylene glycol based (non alcohol) anti-icing agent. Alemite Corporation recommends Kilfrost (tested and approved).

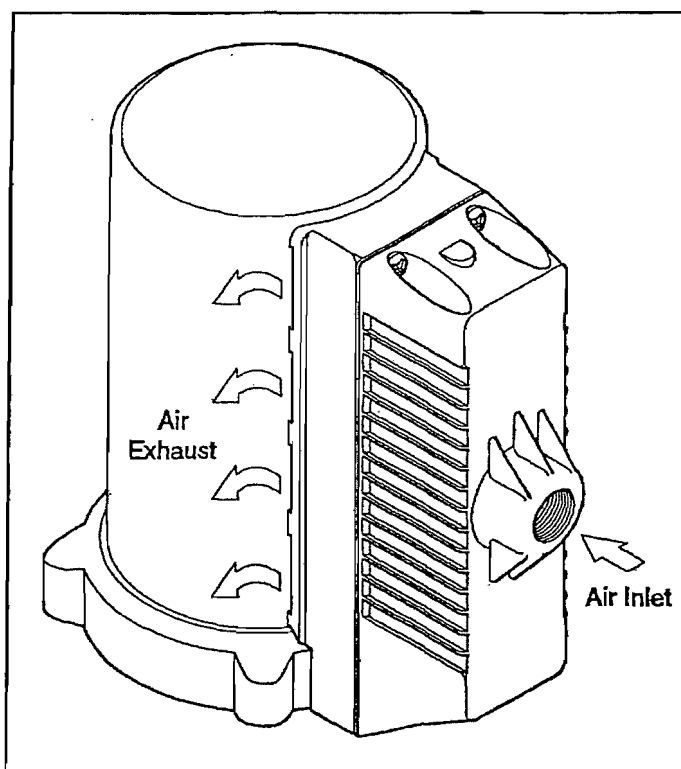


Figure 1 Air Motor Model 338066 Series

Pilot ports in the cylinder control the pilot valves as the ports are uncovered by the piston. The section view of the motor on Pages 6 and 10 illustrate the upstroke and downstroke respectively.

NOTE: These air motors are not available to be purchased separately.

Specifications

Air Motor Model	Piston Diameter x Stroke		Air Inlet	Maximum Air Pressure	
	Inches	Centimeters		psi	Bars
338066-A1	2-15/16 x 3	7.5 x 7.6	1/4" NPTF (F)	150	10.3
338066-C1			1/4" BSP (F)		

Table 1 Air Motor Model 338066 Series Specifications

Alemite Corporation
PO Box 473515, Charlotte, North Carolina 28247-3515

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SER 338066-A1
Revision (11-96)

Item No.	Part No.	Description	Qty	Notes	Numeric Order Part # (Item #)
1		Plug (Brass)	2	●	77903 (19)
2	171009-7	O-Ring, 13/16 " ID x 15/16 " OD	2	●	171000-3 (18)
3		O-Ring, 0.437 " ID x 0.562 " OD (Red Dot)	6	●	171000-7 (14)
4	338051	Piston, Pilot	2	●	171009-1 (8)
5		O-Ring, 0.750 " ID x 0.937 " OD (Red Dot)	2	●	171009-7 (2)
6		O-Ring, 1/8 " ID x 1/4 " OD	6	●	172353 (13)
7	338052	Bushing (Brass)	2	●	172398 (15)
8	171009-1	O-Ring, 7/16 " ID x 9/16 " OD	4	●	338040 (23)
9	338053	Valve, Pilot (Brass)	2	●	338042 (22)
10	338049	Valve, Directional Spool	1	●	338044 (21)
11	338046	Body	1	●	338046 (11)
12		Cover, w/ 1/4 " NPTF air inlet (Aluminum)	1	△	Model 338066-A1 338047 (17)
		Cover, w/ 1/4 " BSPT air inlet (Aluminum)	1	▲	Model 338066-C1 338048 (20)
13		Screw, 10-24 x 1-1/4 "	2		338049 (10)
14	171000-7	O-Ring, 3/8 " ID x 1/2 " OD	3	●△▲	Qty of 1 in △▲ Kits 338050 (1)
15		Screw, 10-24 x 5/8 "	2		338051 (4)
16		Screw, 8-32 x 1-1/4 "	4	●△▲	338052 (7)
17		Plug (Steel)	2	●	338053 (9)
18	171000-3	O-Ring, 3/16 " ID x 5/16 " OD	2	●	338384-1 (6)
19		Nut, 8-32	4	●	338384-2 (3)
20		Gasket	1	●	338384-3 (5)
21	338044	Manifold	1	●	338483-1 (12)
22	338042	Cylinder	1		338483-2 (12)
23	338040	Ring, Mounting	1		338484 (16)

Legend:
Part numbers left blank (or in italics) are not serviced separately
● △ ▲ designates a repair kit item

Repair Kits

Part No.	Kit Symbol	Description
393567-1	●	Kit, Air Valve (Assembled)
393596	△	Kit, Aluminum Cover (w/ 1/4 " NPTF air inlet) [Retrofit for plastic cover]
393596-A	▲	Kit, Aluminum Cover (w/ 1/4 " BSPT air inlet) [Retrofit for plastic cover]

Replacement Module (Air Valve and Aluminum Cover with 1/4 " NPTF Air Inlet)

Part No.	Description	Notes
393631	Module Assembly, Replacement (Assembled)	Consists of Repair Kits 393567-1 and 393596

NOTE: Additional repair kits are illustrated on the following page.

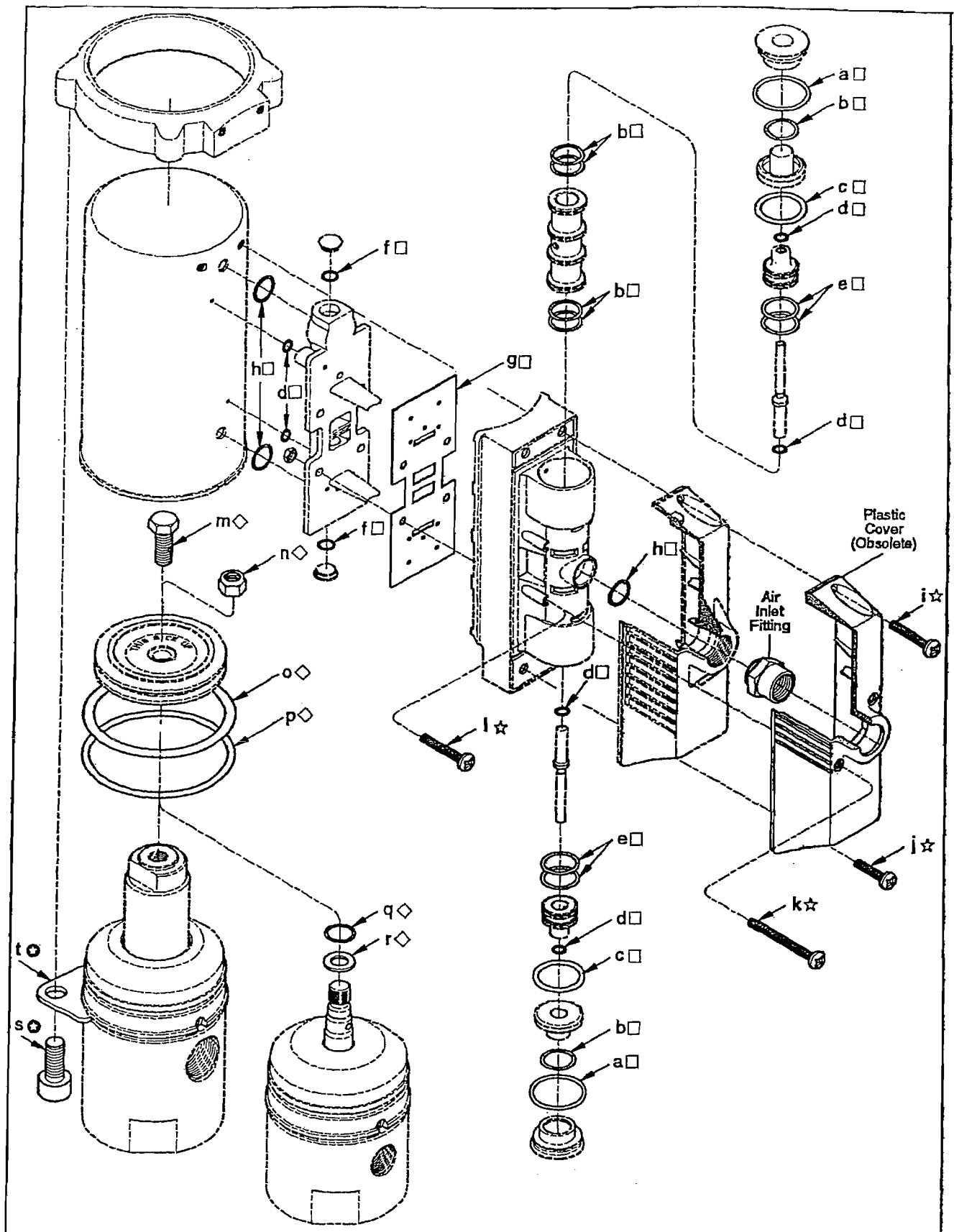


Figure 3 Additional Kits for Air Motor and Pump Tube Assembly

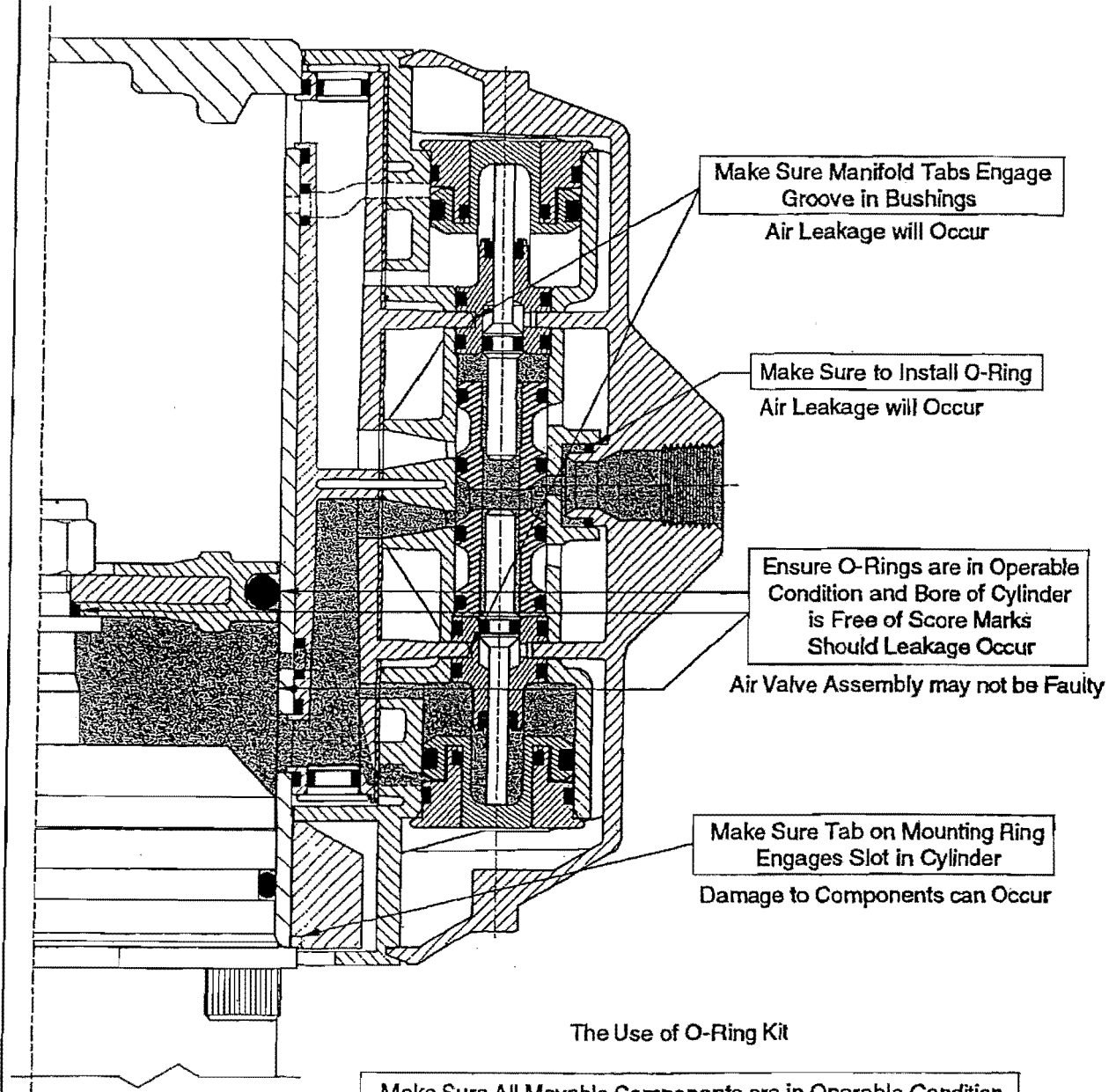
Item	Part No.	Description	Qty	Notes		Numeric Order Part # (Item #)	
a	171009-7	O-Ring, 13/16 " ID x 15/16 " OD	2	□		51929	(n)
b		O-Ring, 0.437 " ID x 0.562 " OD (Red Dot)	6	□		171000-103	(o)
c		O-Ring, 0.750 " ID x 0.937 " OD (Red Dot)	2	□		171003-10	(p)
d		O-Ring, 1/8 " ID x 1/4 " OD	6	□		171000-3	(f)
e	171009-1	O-Ring, 7/16 " ID x 9/16 " OD	4	□		171000-7	(h, q)
f	171000-3	O-Ring, 3/16 " ID x 5/16 " OD	2	□		171009-1	(e)
g		Gasket	1	□		171009-7	(a)
h	171000-7	O-Ring, 3/8 " ID x 1/2 " OD	3	□		171892	(s)
i		Screw, 10-24 x 1-1/4 "	2	☆		172353	(i)
j		Screw, 10-24 x 5/8 "	2	☆		172398	(j)
k		Screw, 8-32 x 1-3/4 "	4	☆	For plastic cover	172399	(k)
l		Screw, 8-32 x 1-1/4 "	4	☆	For aluminum cover	172409	(m)
Additional Kit Items Applicable to the Pump Tube Assembly						338041	(t)
m		Screw, (w/ Nyloc Insert) 3/8 " -24 x 3/4 "	1	◇		338048	(g)
n	51929	Nut, Elastic Stop, 3/8 " -24	1	◇		338109	(r)
o		O-Ring, 2-5/8 " ID x 3 " OD	1	◇		338384-1	(d)
p		O-Ring, 2-3/4 " ID x 3 " OD	1	◇		338384-2	(b)
q	171000-7	O-Ring, 3/8 " ID x 1/2 " OD	1	◇		338384-3	(c)
r	338109	Washer, 3/8 "	1	◇		338484	(l)
s		Bolt, 5/16 " -18 x 1/2 "	4	⊕			
t		Keeper	4	⊕			
Legend: Part numbers left blank (or in italics) are not serviced separately □ ◇ ☆ ⊕ designates a repair kit item							

Repair Kits

Part No.	Kit Symbol	Description
393568	□	Kit, Air Valve (Rubber Components) [Includes tube of 393590 Teflon lubricant]
393569	◇	Kit, Air Motor Cylinder and Piston Seal (Includes tube of 393590 Teflon lubricant)
393570-1	☆	Kit, Screw Assortment (For both plastic and aluminum covers)
393641	⊕	Kit, Keeper

Service Hints

Refer to the Overhaul Procedures for Details



Make Sure All Movable Components are in Operable Condition and Bore of Body is Free of Score Marks Prior to Kit Installation

O-Rings will Deteriorate Prematurely

Test Air Valve on Pump Known to be in Operable Condition After Kit Installation

Rebuilt Air Valve Assembly may not be Faulty

IMPORTANT: Prior to performing any maintenance procedure, the following safety precautions must be observed. Personal injury may occur.



WARNING

Do not use halogenated hydrocarbon solvents such as methylene chloride or 1,1,1 - trichloroethane in this motor. An explosion can result within an enclosed device capable of containing pressure when aluminum and/or zinc-plated parts come in contact with halogenated hydrocarbon solvents.

Release all pressure within the system prior to performing any overhaul procedure.

- Disconnect the air supply line from the motor.
- Into an appropriate container, operate the pump's control valve to discharge remaining pressure within the system.

Never point a control valve at any portion of your body or another person. Accidental discharge of pressure and/or material can result in injury.

Read each step of the instructions carefully. Make sure a proper understanding is achieved before proceeding.

Overhaul

NOTE: Refer to Figure 2 for component identification on all overhaul procedures.

Disassembly

Separate Air Motor from Pump Tube

1. Clamp the pump assembly in a soft-jaw vise at the body.
2. Remove the bolts that secure the body to Mounting Ring (23).
 - Remove the keepers from the body.
3. With a side-to-side motion, pull the air motor assembly from the body.
 - Lubricate the O-Ring with oil to ease separation.

Air Motor

4. Remove Screws (13) and (15) that secure Cover (12) to Cylinder (22).
 - Remove the air valve assembly from the Cylinder.

5. Remove O-Rings (14) and O-Rings (6) from the rear of Manifold (21).

6. Remove Mounting Ring (23) from the Cylinder.

NOTE: On earlier models, remove Screws (k) that secure the plastic cover to the Body and Manifold. See Figure 3.

7. Remove the Cover from Body (11).

8. Remove O-Ring (14) from the Cover.

NOTE: On earlier models, remove O-Ring (h) from the air inlet fitting. See Figure 3.

9. Remove Screws (16) that secure the Body to the Manifold.
 - Remove Nuts (19) from the rear of the Manifold.
10. Separate the Body from the Manifold.
11. Remove Gasket (20) from the Manifold.
12. Remove Plugs (17) from each end of the Manifold.
 - Remove O-Ring (18) from each Plug.

CAUTION

Should Pilot Piston (4) remain within the Body, use care during removal. Damage can occur.

13. Remove Plugs (1) [w/ Pilot Piston (4)] from each end of the Body.
 - Separate the Pilot Piston from each Plug.
14. Remove O-Rings (2) and (3) from both Plugs.
15. Remove O-Ring (5) from each Pilot Piston.
16. Remove Pilot Valve (9) [w/ Bushing (7)] from each end of the Body.
 - Separate the Bushing from each Pilot Valve.
17. Remove O-Ring (6) from both Pilot Valves.
18. Remove O-Rings (6) and (8) from each Bushing.

CAUTION

Remove Spool Valve (10) from the Body with care. Damage to either component can occur.

19. Remove Spool Valve (10) from the Body.
20. Remove O-Rings (3) from the Spool Valve.

Clean and Inspect

NOTE: Use the appropriate repair kit for replacement parts. Make sure all the components are included in the kit before discarding used parts.

1. Clean all metal parts in a cleaning solvent. The solvent should be environmentally safe.
2. Inspect all parts for wear and/or damage.
 - Replace as necessary.
3. Inspect the bores of Body (11) and Cylinder (22) closely for score marks.
 - Replace as necessary.

Assembly

NOTE: Prior to assembly, certain components require lubrication with Magnalube-G Teflon grease. Refer to Table 2 for details.

IMPORTANT: Always use Magnalube-G Teflon grease in this air motor.

Air Motor

NOTE: Refer to Figure 2 and Figure 5 for component identification on all assembly procedures.

Item No. on Figure 2	Description	Notes	Item No. on Figure 2	Description
9	Pilot Valve - O-Ring Groove and Long Stem.	See Figure 2	11	Body - All Bores
10	Spool Valve - O-Ring Grooves and Bore		22	Cylinder - Bore
All O-Rings illustrated in Figure 4				
NOTE: Part number 393590 is a 0.75 ounce (21.8 gm) tube of Magnalube-G Teflon grease				

Table 2 Components Lubricated with Magnalube-G Teflon Grease

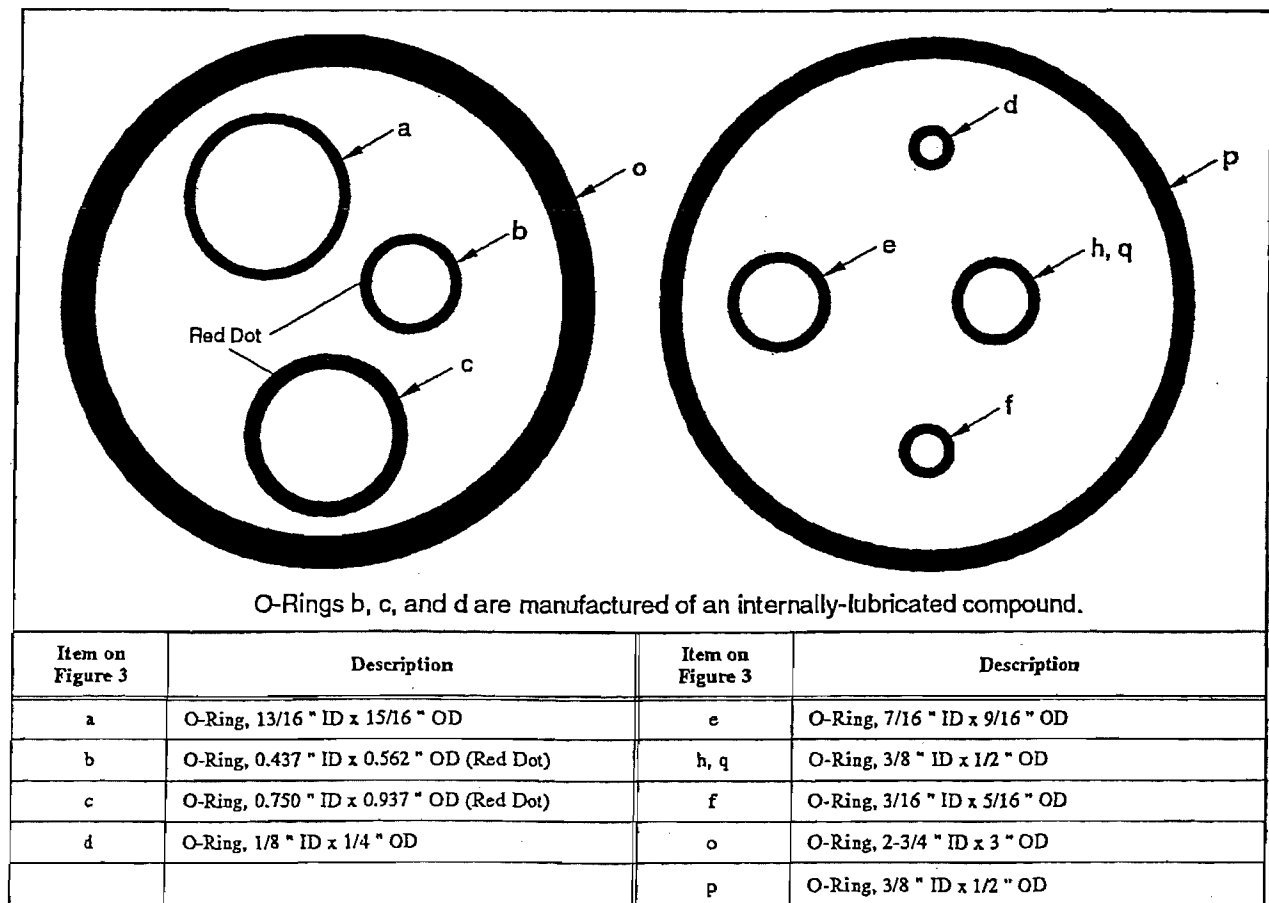


Figure 4 O-Ring Chart (Actual Size)

To ease the assembly process, identify all the O-Rings. Position each O-Ring on the chart. See Figure 4.

1. Install O-Rings (3) onto Spool Valve (10).
 2. Install O-Ring (6) into each Bushing (7).
 3. Install O-Rings (8) onto the outside diameter of each of the Bushings.
 4. Install O-Ring (6) onto both Pilot Valves (9).
 5. Install and seat the Pilot Valve (small diameter first) into the larger diameter of the Bushing.
 - Repeat the process for the additional Pilot Valve and Bushing.
 6. Install one of the Pilot Valve and Bushing assemblies (large diameter first) into the Body.
 - Make sure the Bushing seals properly in the bore.
 7. Position the Spool Valve partially into the bore of Body (11).
 - Use care not to unseat the Bushing.
 8. Install and seat the additional Pilot Valve and Bushing assembly (large diameter first) into the opposite end of the Body.
- IMPORTANT:** Push the Bushing assembly fully into the Body. This positions the Spool Valve properly. The valve assembly will fail to operate unless the Spool Valve is properly installed.
9. Install O-Ring (5) onto each Pilot Piston (4).
 10. Install O-Ring (3) into each Plug (1).
 11. Install O-Ring (2) onto the outside diameter of each of the Plugs.
 12. Install and seat the Pilot Piston (stem first) into the bottom of the Plug.
 - Repeat the process for the additional Plug.
 13. Install and seat each Plug assembly into the Body.
 14. Install O-Ring (18) onto each Plug (17).
 15. Install and seat the Plugs into each end of the Manifold.
 16. Install Gasket (20) onto the flat side of Manifold (21).
 17. Install and seat the Manifold (tabs first) into the back of the Body.

IMPORTANT: The tabs on the Manifold must engage the groove in each Bushing (7). When each Bushing is seated properly in the Body, the Manifold will seat properly.

18. Install Nuts (19) into the rear of the Manifold.

19. Install Screws (16) through the Body.
 - Tighten the Screws evenly and securely in a crisscross pattern. Do not overtighten.

NOTE: On earlier models (See Figure 3):

- Install O-Ring (h) onto the Air Inlet Fitting.
- Position the Inlet Fitting (threads first) into the Plastic Cover.
- Position the Cover onto the Body.
- Install the nuts into the rear of the Manifold.
- Install Screws (k) through the Cover and Body.
- Tighten the Screws in a crisscross pattern. Do not overtighten.

20. Install O-Ring (14) onto the bushing on the inside of Cover (12).

21. Install the Cover onto the Body.

IMPORTANT: Make sure the tab on Mounting Ring (23) engages with the slot in Cylinder (22). Damage to components can occur.

22. Install Mounting Ring (23) onto Cylinder (22).

23. Install O-Rings (6) into the smaller ports on the Manifold.

24. Install O-Rings (14) into the larger ports on the Manifold.

IMPORTANT: Make sure the O-Rings remain in position. Spot the O-Rings with Teflon grease as necessary.

25. Align the valve assembly with the holes in the Cylinder and Mounting Ring.

26. Install Screws (13) into the top of the Cover and into the Cylinder.

27. Install Screws (15) into the bottom of the Cover and into the Mounting Ring.

28. Tighten all the screws evenly and securely in a crisscross pattern. Do not overtighten.

For details on pump tube components, refer to the Pump SER Service Guide for details.

Attach Air Motor to Pump Tube

29. Clamp the body securely in a soft-jaw vise.

30. Install the air motor assembly squarely onto the body.
 - Use care passing the O-Ring.
 - Make sure the material outlet on the body orients properly with the inlet of the air motor.

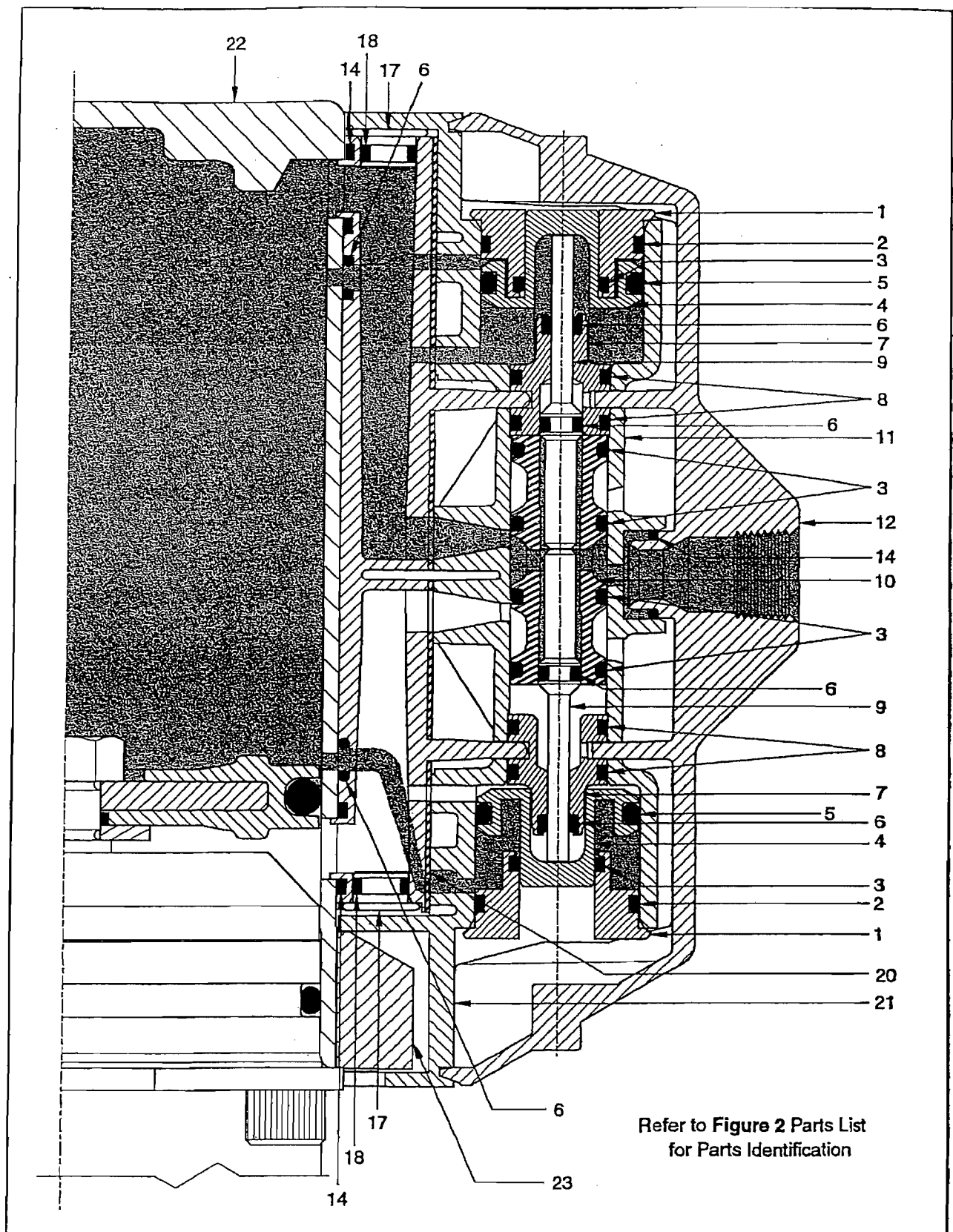


Figure 5 Air Motor Model 338066 Series- Section View

31. Install the keepers into the groove of the body.
32. Install the bolts that secure the body to the air motor assembly.
 - Tighten the bolts evenly and securely in a crisscross pattern.

Bench Test and Operation

1. Slowly supply air pressure [not to exceed 50 psi (3.4 Bar)] to the pump's motor.
 - The pump assembly should cycle.

If the pump assembly does not cycle, refer to the Pump **SER Service Guide** for details.

With air pressure at zero:

2. Connect a product hose to the pump's material outlet.
 - Direct the hose into an appropriate collection container.
3. Place the pump in the product to be dispensed.
4. Slowly supply air pressure to the pump's motor.
5. Allow the pump to cycle slowly until the product is free of air.

If the pump assembly does not prime, refer to the Pump **SER Service Guide** for details.

WARNING



Should leakage occur anywhere within the system, disconnect air to the motor. Personal injury can occur.

With air pressure at zero:

6. Attach a control valve to the outlet hose of the pump.
 - Make sure the nozzle on the control valve is open.
7. Slowly supply air pressure to the pump's motor.
8. Allow the pump to cycle slowly until the product is once again free of air.
9. Set the air pressure to 60 psi (4.1 Bar).
10. Operate the control valve into a container.
11. Shut off the control valve.
 - Visually inspect the pump for external leaks.
 - The pump should not cycle more than once or twice in one hour.

If the pump cycles more than once or twice an hour, refer to the Pump **SER Service Guide** for details.

12. Check the motor for air leakage.

If the motor leaks, refer to the **Troubleshooting Chart** for details.

Installation

Additional items that should be incorporated into the air piping system are listed in **Table 3**.

Part Number	Description
338860	Regulator, Gauge, Separator Combination (w/ Auto Dump)
7604-B	Regulator and Gauge (Included with 338860)
5604-2	Moisture Separator (Included with 338860)

Table 3- Air Line Components

Troubleshooting Chart

Indications	Possible Problems	Solution
Air Motor does not cycle	1. Insufficient air pressure 2. Jammed air valve assembly 3. Pump tube jammed and/or contains loose components	1. Increase air pressure 2. Rebuild or replace air valve assembly 3. Rebuild pump tube
Air motor does not cycle and air blowing at exhaust	Spool Valve (10) hung-up on center position *	Reposition Spool Valve (10) Disassemble air motor, clean, inspect, and replace worn or damaged components and lubricate with Magnalube-G Teflon grease.
Air motor cycles and air blowing at exhaust	Missing O-Ring(s)	Disassemble air motor, clean, inspect, and install O-Ring(s). Lubricate with Magnalube-G Teflon grease.
Air motor cycles and slight air leakage at exhaust	1. Worn or damaged O-Ring(s) 2. Initial tightening of Screws (13) and/or Screws (15) not sufficient	1. Disassemble air motor, clean, inspect, and replace worn or damaged O-Ring(s) Lubricate with Magnalube-G Teflon grease. 2. Tighten Screws (13) and/or (15)
* Spool Valve (10) can hang on the center position due to icing, lack of lubrication, and/or contaminants. Use an anti-icing agent as required.		

Changes Since Last Printing

New Format



S I M P L A N

INSTALLATION OF THE SEAL

- A) When the seals are unpacked from the packaging, disassemble the rotating boot assembly from the seal stationary flange #7.
- B) Remove stationary ring #24 from stationary flange #7. This is achieved by first finding the anti-rotation pins #22. Place a feeler gauge or thin knife blade under the ring and locate the position of the pins. To remove the ring, place your hands over the pin locations and pull the ring out. Care must be taken to pull the ring evenly. *Lifting one side more than the other could cause the ring to break.* Silicon Carbide is a very hard material but it should be handled with care, as the material is very brittle. Check the two o-rings #21/#23 for damage.

WARNING! It is extremely important that the very sensitive sealing faces on rings #9 and #24 are not damaged in any way, however slight, and that they do not come into contact with oil or grease at any time.

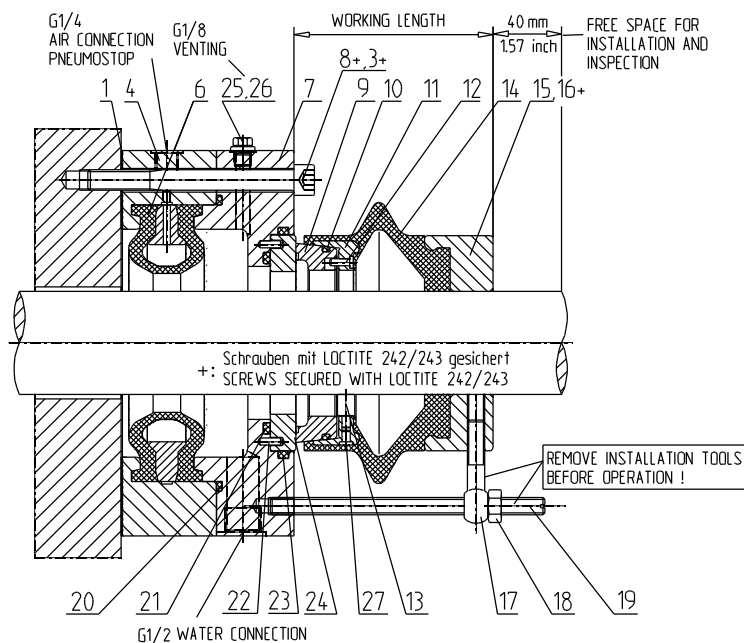
- C) The stationary flanges #7/#4 should be mounted on the sterntube flange and secured.
- D) The propeller shaft should now be installed in the vessel.
- E) When the propeller shaft has been pulled up to position to re-install the muff coupling, coat the shaft with "green soap", in order to grease it. Fit the boot assembly on the shaft. At this time you have to adjust the 4 nylon pins #13 in the boot #14. This is achieved by hand filing the pins by equal amounts. The arrangement of the pins is to stop any movement of the boot when the shaft is operated. Set a small clearance between the pins and shaft (approx. 1/16"). Take care to remove all filings from the insides of the boot #14.
- F) After completing the adjustment of the pins #13, remove the boot from the shaft.
a) Fit the o-rings #21/#23 in the stationary housing ring #7.
b) Place the stationary ring #24 on the shaft. Wrap the ring with rags etc. to avoid any damage to the ring.
c) Place the boot #14 back on the shaft. Leave the sealing ring #9 in the boot assembly. Wrap again with rags to avoid damage.
- G) Jump the muff coupling back on the prop shaft and pull the shaft up to the gearbox coupling. Place a couple of bolts in the coupling.
- H) Assemble stationary ring #24 in the flange assembly.
1. Mark the location of pins #22 on flange #7.
2. Mark the location of the holes in the ring (with chalk).
3. Coat the o-rings #21/#23 with the white paste (Klüber 46 MR 401) supplied with the seal unit.

4. Line up the marks.
5. Press stationary ring #24 into the locating pins #22, place your hands over the pin locations when pressing in.

- I) Push the boot assembly along the shaft to meet the stationary flange #7. Install the tension gear (4 rods #19 & 4 eyebolts #17). Locate loosely the split brass clamp (locking) ring #15 over boot #14. Tighten nuts #18 on the tension bars #19 taking care to move the nuts approximately the same distance by crosswise tightening.

Note: On the drawings the distance given between the flange face and back of the split ring is the compressed seal length. I.e. model 120 shows 116 mm or 4.56". As a word of caution, a little "less" tension is better than a little more. When the compression of the seal is achieved, tighten cap screws #16 on split clamp (locking) ring #15. Remove the tension gear from the seal.

Seal Size	Working Length	
	mm	inch
60	96	3,78
70	96	3,78
80	96	3,78
90	116	4,57
105	116	4,57
120	116	4,57
135	116	4,57
150	116	4,57
165	116	4,57
180	116	4,57
195	128	5,04
210	128	5,04
225	128	5,04



- J) Remove the plastic cap from the water connection at the bottom of the flange (1/2" pipe thread).
- a) Connect the water supply pipe if necessary.
 - b) If cooling is coming from a scoop on the sterntube, place a plug in the flange.
- K) a) Connect a quick-release air connection on the pneumostop outlet (1/8" pipe thread). This is the most aft connection.
- b) Connect an open vent pipe without a vent valve to a suitable height above the water level, or, if not possible, a vent valve on the flange (1/4" pipe thread).
- L) When the vessel goes back into the water open the vent valve, if installed, on top of the seal to completely fill the seal with water, removing all air.
- M) At full revolutions the seal temperature will be approx. 15 to 20 degrees F (8 to 12 °C) above sea temperature.

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1 General about SIMPLAN – Seal

Type: **SIMPLAN – (SiC-P)**, with standstill seal (Pneumostop).

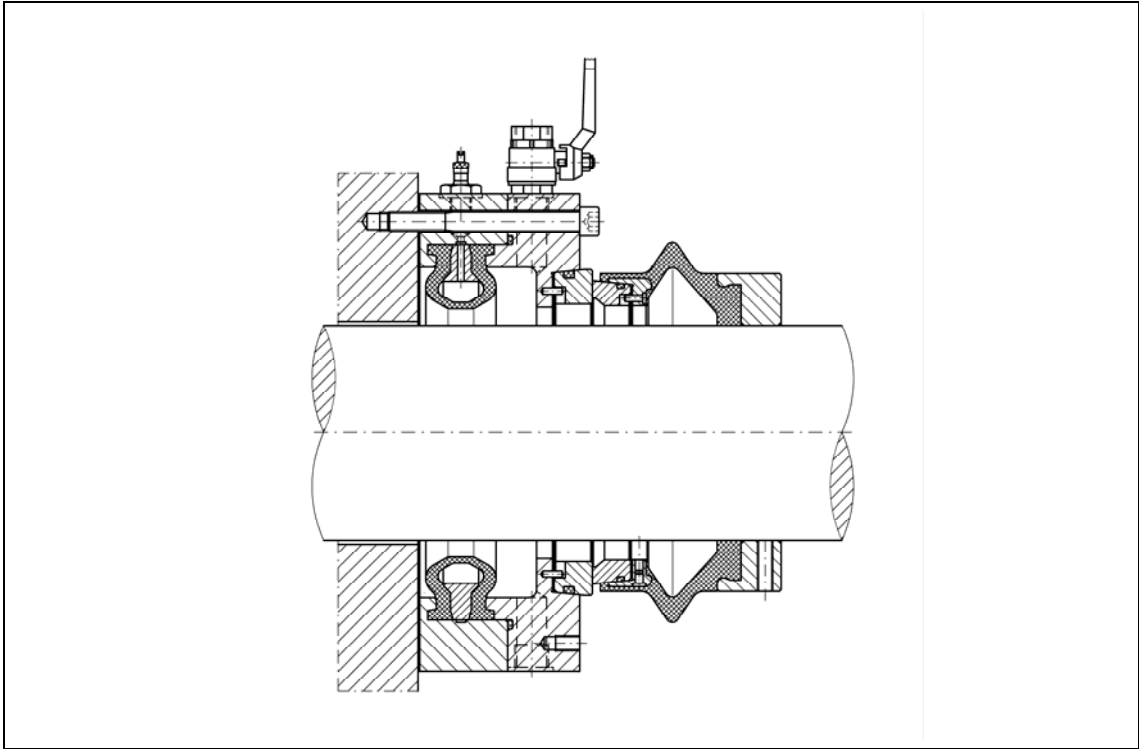


Fig. 1: Cross sectional view SIMPLAN Standard

1.1 General description about sterntube seals

The SIMPLAN seal is a mechanical face seal for water lubricated sterntubes. It is equipped with a standstill seal. Type SiC-P is fitted with silicon carbide sealing rings. These sealing rings are wear-resistant.

The standstill seal included in the seal unit consists of housing rings (4 and 7) and an inflatable tube ring (6) which is clamped between rings (4, 7) and insert ring (5).

Counter ring (24) is fixed in the housing ring (7) by o-ring (23). Relative motion of sealing ring (24) to housing ring (7) is stopped by two dowel pins (22). The stationary sealing ring (24) forms, together with the rotating ring (9), the axial seal. Both sealing rings (9 and 24) are made of silicon carbide.

The rotating sealing ring (9) is pressed into a metal insert ring (11) vulcanised to a rubber seal body called boot or bellows (14). Tightness between sealing ring (9) and insert ring (11) is guaranteed by an o-ring (10).

The boot/bellows (14) is held fixed on the shaft by means of clamp ring (15). This ring (15) ensures that the necessary contact pressure is provided between counter ring (24) and

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sealing ring (9). Pins (12, 13) fitted radially and axially in insert ring (11) ensure reliable torque transmission to sealing ring (9) and optimal centricity of the rubber seal body (14) to the shaft.

The seal is supplied ready to install.

The water connection necessary for flushing the seal is located at the bottom side of the housing ring (7). The venting line is connected to the top.

Prior to operating the seal unit its housing must be vented.

Further data on the individual components and materials from which the SIMPLAN seal is made is given in the enclosed parts list. *

* See Part 3, drawing „ Aft SIMPLAN seal with parts list “.

1.2 Application and specified usage

Our seals are intended only for the stipulated application (e.g. for sealing rotating ship's shafting against water).

Any other or additional usage shall be considered not as specified.

The specified use includes also following the operating instructions and adhering to the inspection and maintenance conditions.

Usage not in accordance with specifications shall lead to the loss of all warranty rights.

1.3 Explanation of symbols and notes



This symbol will be found next to **danger notes** which indicate direct or indirect hazards to life and limb.

Grave or critical injuries may result if these notes are not followed. The seal and/or surrounding items may also be damaged or destroyed.



This symbol will be found next to **safety notes** containing instructions or rules.

Faults and malfunctions of the seal may result if these notes are not followed. Damage to the seal and/or surrounding items may also occur.



This symbol will be found next to a **note** that contains special information on key functions, or special tips for use that help you to make optimum use of the seal.



Rights under the warranty will be lost if the danger and safety notes are not followed.

- The numbers in parentheses () are the reference numbers on the corresponding drawings.
- Data in square brackets are nominal dimensions for a specific project; the actual values may vary from these.

1.4 Copyright

These operating instructions are intended for the fitters, the operator, and the operating personnel.

The manufacturer, **B+V Industrietechnik**, retains the copyright in these operating instructions.

These operating instructions may only be reproduced in the context of their incorporation into wider documentation, just as the seal is incorporated into a wider installation to be documented.

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2 SHIP DESIGN CRITERIA IN REGARD TO THE SIMPLAN SEAL

During the vessel design stage, the following data must be taken into account:

- Maximum allowed water pressure. *
- The rpm limits of the seal.
- Axial and radial movement of the shaft. *
- Maximum air pressure for the emergency standstill seal. *
- Type of air supply, venting of air supply line.

and:

- The front face of the sterntube must be rectangular to the shaft.
- The flange connection (PCD) at the sterntube must be checked *
- Seal must be ordered for the final shaft diameter.

Also important:

- Minimum quantity of flushing water required.
- Venting line from seal to be well above water level.
- The flushing water arrangement (forced lubricated system) *:
 - Main flow into the sterntube.
 - Auxiliary flow into the seal.
 - Pipe always below water line.
 - Bottom connection on seal to be used.
 - We recommend to install a flushing water pump.
 - We recommend to install a water cooler with thermostatic valve.
 - We recommend to install a flow indicator.

* See Part 3, drawing SGC:3-201-0015-000. „Cooling Water Diagram“.



The engine room must be heated in order to avoid freezing of the flushing water within the SIMPLAN seal during the winter time.



Any additives to the sterntube flushing water must be approved by B+V Industrietechnik for compatibility with materials of the seal.

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3 FITTING THE SIMPLAN SEAL

3.1 Before installation of the seals

The SIMPLAN seal will be supplied machined to the final shaft diameter and ready to fit.



The seal may only be removed from the box in which it was supplied immediately prior to fitting.

- The entire sterntube system must be checked to ensure absolute cleanness.
- Prior to fitting the seal, the true running and rectangularity of the sterntube front face in respect to the shaft must be checked when shaft is coupled. *
- The various surfaces and the shaft surface within the seal area must be cleaned and inspected for damage.
- Check recess and PCD at sterntube and SIMPLAN housing for correct dimensions.
- Remove the seal from the box, remove fitting device (17, 18, 19).
- Check the seal for transport damage and cleanliness.



The finely machined sealing surfaces of the sealing ring (9) and counter ring (24) are extremely sensitive and must under no circumstances be damaged.

3.2 Fitting the seal from inboard, with the propeller shaft being fitted from aft/outboard

The shaft is already inserted into the sterntube from the aft/outboard into a position such that the aft and forward SIMPLAN seal can be fitted.

- Remove the rotating boot / bellow assembly (14) (with clamp ring 15) from the stationary flange ring (7).
- Fit gasket (1) on the shaft.
- Fit pre-assembled, stationary part of the seal (4, 5, 6, 7) (with counter ring (24) installed) on the shaft and slide it to the sterntube together with the gasket (1).



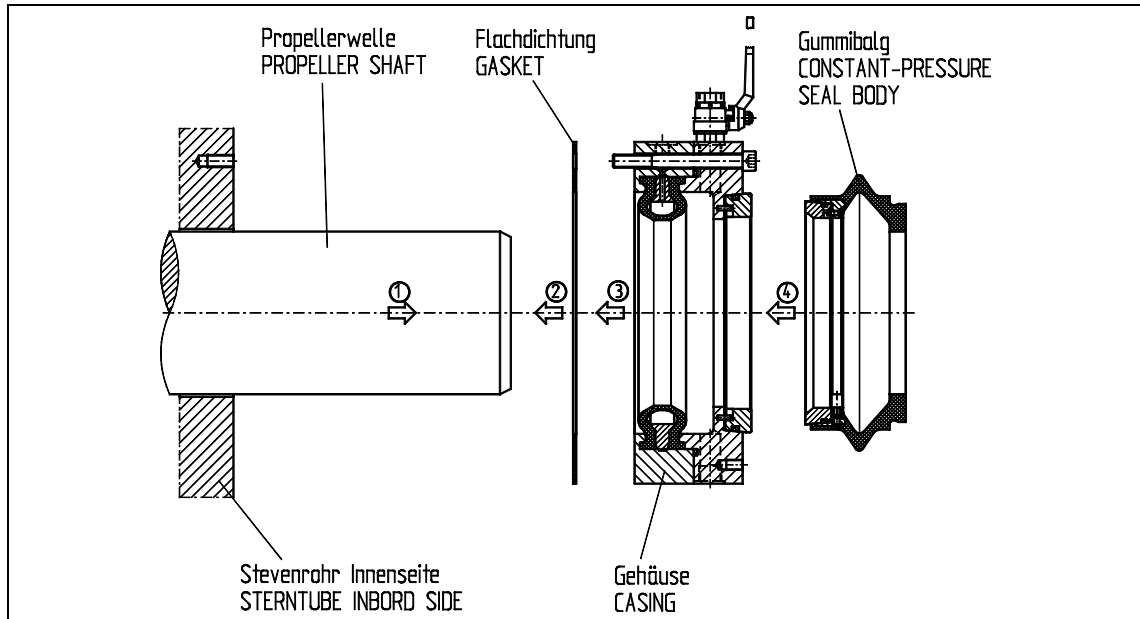


Fig. 2: Fitting the Simplan

Shaft fitted from aft/outboard



It must be ensured that the sealing faces of the counter rings (24) and sealing rings (9) are not damaged.

- Fasten the pre-assembled part of the seal (4, 5, 6, 7 and 24) together with the gasket (1) to the stern tube with bolts (8), secured with Loctite.
- If not installed, fit the, for the special shaft diameter ready machined, centering pins (13) into the inner area of the boot (14).
- Check the distance between two opposite centering pins (13). It must be bigger than the shaft outer diameter: **0,5 to 0,8 mm** (0.002 and 0.032 inch) for Size 180 and below; or **0,8 to 1,2 mm** (0.032 and 0.047 inch) for Size 195 and above.
- Coat the rubber seal body (boot/bellows) (14) neck collar on its shaft contact surface with "Klüberpaste 46 MR 401".



Ensure, that the white "Klüber" paste contacts neither the silicon carbide sealing ring faces nor the area between clamp ring and shaft. These contact surfaces must be clean and dry.

- Fit the boot (14) with inserted sealing ring (9) and centering pins (13), but without clamp ring (15) on the shaft and slide it against the counter ring (24).

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Do not fix boot / bellow assembly (14) to the shaft by clamp ring (15) until the shaft is coupled.

- Bring the shaft into its final position.



Slide the boot/bellows (14) with the inserted sealing ring (9) and centering pins (13) in direction of the counter ring (24) while moving the shaft.

- Couple up the shaft.



Do not allow temperatures above **95°C** (200 °F) for more than one hour to heat the boot/bellows (14) via the shaft and clamp ring (15), while fitting or removing the coupling muff.
If required, cool the shaft in the area of the boot/bellows (14).
Too much heat will destroy or harden the boot/bellows (14).

- Check shaft displacement 'W' relative to the seal housing. *
- Slide the boot (14) with inserted sealing ring (9) carefully against the counter ring (24).

* See Part 3, drawing SGC:3-201-0012-000. „Installation dimensions with tolerances “.

For further instructions go ahead with chapter **“Fitting the aft seal”**.”

3.3 Fitting the seal with the propeller shaft being fitted from inboard the vessel

The shaft is in a temporary position in front of the sterntube, so that the inner seal can be moved over the shaft.

- Remove the boot/bellows (with clamp ring 15) from the stationary flange (7).
- If not installed, fit the, for the special shaft diameter ready machined, centering pins (13) into the inner area of the boot (14).
- Check the distance between two opposite centering pins (13). It must be bigger than the shaft outer diameter: **0,5 to 0,8 mm** (0.002 and 0.032 inch) for Size 180 and below; or **0,8 to 1,2 mm** (0.032 and 0.047 inch) for Size 195 and above.
- Coat the boot/bellows (14) neck collar on its shaft contact surface with "Klüberpaste 46 MR 401".





Ensure that the white “Klüber” paste contacts neither the silicon carbide sealing ring faces nor the area between clamp ring and shaft. These contact surfaces must be clean and dry.

- Fit the boot/bellows (14) with inserted sealing ring (9) and centering pins (13) on the shaft and slide it towards the coupling flange.



Do not fix boot / bellow assembly (14) to the shaft by clamp ring (15) until the shaft is coupled.

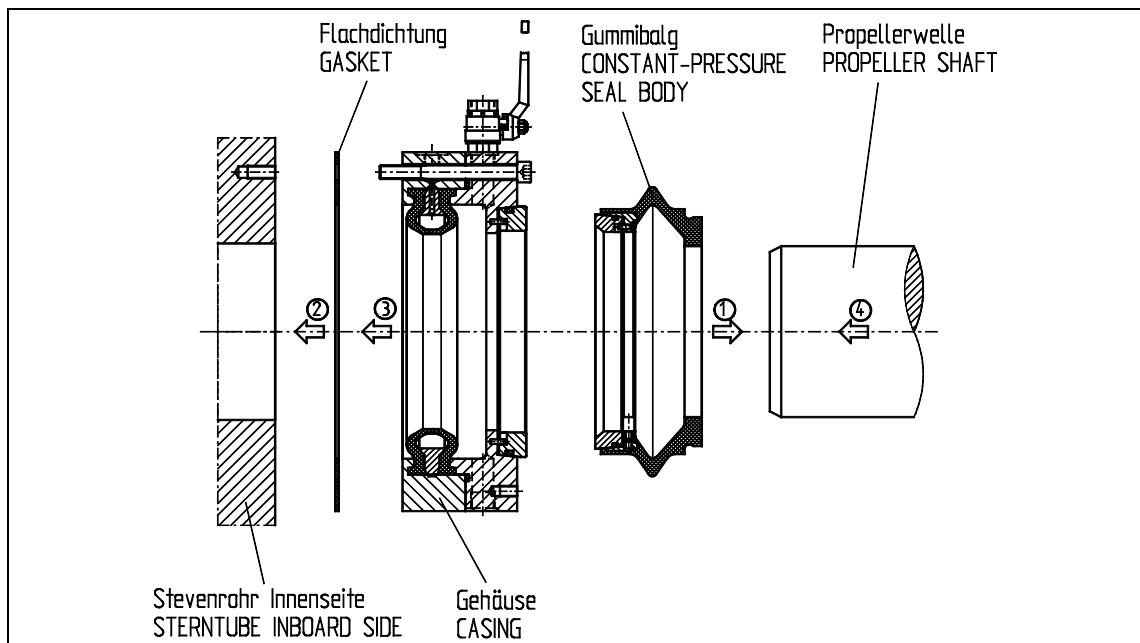


Fig. 3: Fitting the Simplan

Shaft fitted from inboard



It must be ensured that the sealing faces of the and sealing rings (9) are not damaged.

- Fit pre-assembled, stationary part of the seal (4, 5, 6, 7), with counter rings (24) installed and with the gasket (1), at the sterntube by bolts (8), secured with Loctite
- Draw in the shaft into the sterntube.
- Bring the shaft into its final position.



Slide the boot/bellows (14) with the inserted sealing ring (9) and centering pins (13) in direction of the coupling flange while moving the shaft.

- Couple up the shaft.



Do not allow temperatures above **95°C** (200 °F) for more than one hour to heat the boot/bellows (14) via the shaft and clamp ring (15), while fitting or removing the coupling muff.
If required, cool the shaft in the area of the boot/bellows (14).
Too much heat will destroy or harden the boot/bellows (14).

- Check shaft displacement 'W' relative to the seal housing. *
 - Slide the boot (14) with inserted sealing ring (9) carefully against the counter ring (24).
- * See Part 3, drawing SGC:3-201-0012-000. „Installation dimensions with tolerances “.

For further instructions go ahead with chapter “**Fitting the aft seal**”.

3.4 Final Assembly and aligning the seal



Keep in mind that the shaft must be in its final position and coupled when fastening and aligning the seal.

3.4.1 Final Assembly

- Coat the contact face of boot/bellows (14) in way of the clamp ring halves (15) with "Klüberpaste 46 MR 401".
- Place the clamp ring halves (15) around the boot/bellows (14) and the shaft, insert screws (16) and only tighten to the extent that clamp ring (15) can still be moved by means of the tensioning device (18,19) for pre-tensioning the boot/bellows (14) on the shaft.
- Attach the device (17, 18, 19). Therefor proceed as follows:
 - Screw the eye bolts (17) into the clamp ring (15) and turn it back until the eyes are in direction of the shaft.
 - Screw the threaded bolts (19) through the eye bolts (17) into the housing ring (7).
 - Screw the nuts (18) onto the threaded bolts (19) against the eye bolts (17) by hand.
- For the initial position, turn nuts (18) manually against the eyebolts (17) **until the faces of the counter ring (24) and sealing ring (9) make contact**.

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In the initial position, the distance deviation between the rear edge of clamp ring (15) and front edge of housing (7) ring should not be more than $\pm 0,3 \text{ mm}$ in the area of eyebolts (17).

- Tighten each nut (18) clockwise halve turn **until the preload specified in the drawing is reached.**

* See Part 3, drawing SGC:3-201-0012-000. „Installation dimensions with tolerances “.

1.1.1 Alignment check

- Check the alignment of the clamp ring. The distance deviation between the rear edge of the clamp ring (15) and front edge of the housing ring (7) should not be more than $\pm 0,2 \text{ mm}$ in the area of the eye bolts, otherwise realign it (as described in section below).
- Check the gap between sealing ring with 0,05 mm feeler gauge, minimum at top and bottom. Then turn the shaft 180° and check again. If the feeler gauge can be inserted into the gap, realign the clamp ring (15) (as described in chapter “Realigning the seal (ship is in the water), and cleaning the surfaces”).

3.4.2 Fastening the Clamp ring

- Tighten the clamp ring (15) with the screws (16), using Loctite.



The final distance deviation between the rear edge of clamp ring (15) and front edge of housing ring (7) should not be more than $\pm 0,2 \text{ mm}$ in the area of eyebolts (17). *

- Remove tensioning screws and eyebolts (17, 18, 19) and store on board.

* See Part 3, drawing SGC:3-201-0012-000. „Installation dimensions with tolerances “.

1.2 Pipework for the seal

A flushing-water system for the seal must be provided (i.e. circulating water pump, scoop or a connection to the engine cooling water system)

The pipe lines should always be below the water level to ensure that no air can enter the system.

We recommend a flushing system with a main flow to the sterntube for cooling the sterntube and an auxiliary flow using smaller diameter pipe for cooling the seal.

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After installation of the SIMPLAN seal, the pipe work is carried out (use cleaned pipes only)

- Install piping for flushing the sterntube.
- Install piping for flushing the seal.
- Install piping for the standstill seal (Pneumostop) and connect this to the air supply. Remove the valve insert of valve (32), install vent valve in supply line.
- Install piping for venting the seal.

* See Part 3, drawing SGC:3-201-0012-000. „Installation dimensions with tolerances “.

1.3 Final check of the seal (ship is out of the water)



Ensure that the white “Klüber” paste will contact neither the silicon carbide sealing ring surfaces nor the area between clamp ring and shaft. These contact surfaces must be clean and dry.

- Check the Pneumostop (at standstill) for tightness (ship is out of the water) by inflating to 2,5 bar air pressure. Then vent the Pneumostop completely.
- Be prepared to inflate the Pneumostop if leakage occurs during floating of the vessel.
- Be prepared to shut off the water connection to the seal.
- Float the vessel.



While floating the vessel, check the seals visually for tightness. If there is leakage, inflate the Pneumostop to 2,5 bar above water pressure, and shut off the water connection to the seal.



4 MEASURES PRIOR TO THE OPERATION OF THE SEAL

1.4 Final installation check of the seal (ship is in the water)

- Check the underside of the seal for moisture (dampness is acceptable). Water drops are unacceptable. If there is water the seal surfaces must be cleaned or the clamp ring realigned (see chapter "Realigning the seal (ship is in the water) and cleaning the surfaces).
- Open the vent line.
- Open the valves in flushing-water line.

1.4.1 Checking the Pneumostop for correct functioning

- Inflate the Pneumostop (6) to 2,5 bar above water pressure.



Do not turn the shaft when the Pneumostop is inflated.

If the Pneumostop is not vented, it will be destroyed when the shaft starts turning.

If the Pneumostop is damaged, the drain must be closed and the ship dry-docked for repair!

- Close the valves in the flushing water line.
- Keep vent line open.
- Disconnect or drain the flushing water line to drain the seal.
- Check the seal for leakage at the flushing water line connection or drain.



If water runs out of the drain continuously, the Pneumostop is not inflated, or is damaged, or unable to seal as dirt is between the Pneumostop and the shaft surface.

- Connect flushing water line / close drain valve.
- Vent the Pneumostop (6) by opening or removing valve (32) insert and release the air pressure completely.
- Open the valves in the flushing water line.

1.4.2 Alignment check

- Check the alignment of the clamp ring. The distance deviation between the rear edge of the clamp ring (15) and front edge of the housing ring (7) should not be more than ± 0,2 mm in the area of the eye bolts, otherwise realign it (as described in section below).

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- Check the gap between sealing ring with 0,05 mm feeler gauge, minimum at top and bottom. Then turn the shaft 180° and check again. If the feeler gauge can be inserted into the gap, realign the clamp ring (15) (as described in section below).

1.4.3 Realigning the seal (ship is in the water), and cleaning the surfaces



Always secure the clamp ring (15) by fitting the tensioning device (threaded bolt, eye bolt and hexagon nuts 17, 18, 19).

- Inflate the Pneumostop (6) as described in chapter “Checking the Pneumostop for correct functioning”.
- Loosen the clamp ring (15) and relieve the tension on the boot/bellows. If the seal surfaces stick together, pull the boot/bellows back, away from the seal housing.



To avoid damage, never use metal tools such as screwdrivers to separate the silicon carbide rings.

- Clean the carbide ring surfaces carefully (only if necessary)
- Realign clamp ring (15) and fix it as described in chapter “Aligning the seal”.

1.5 Start up

- The seal must be vented by means of the vent valve (ball cock 25) when the ship is in the water.



Operating the sealing rings dry will result in the destruction and failure of their sealing faces.

It is absolutely necessary, therefore, to vent the seal housing after every docking, refilling of sterntube lubricant and periodically during the vessel's operation.

This can be done by fitting a short pipe to the vent valve (ball cock 25) whereby the vent valve has to be opened regularly, or, to have a permanent venting by means of an open pipe line with the end as far as possible above the water line, while ball cock (25) must be open all the time.

- Check whether the standstill seal (Pneumostop) is pressureless.
- Open the flushing water connection to the seal.
- Check whether the flushing water pump is operating and there is a flow in the line.

1.6 Checking the seal during HAT or engine trials

During the following manoeuvres, check the seals as described in chapter “Final installation check of the seal (ship is in the water)”.

- With the Pneumostop (6) not inflated, run the shaft ahead (ship is tied up at the quay).
- With the Pneumostop (6) not inflated, run the shaft astern (ship is tied up at the quay).
- After HAT (Harbour Acceptance Test) check visually for leakage at the seal. If there is leakage, check the seal, clean the sealing ring surfaces or realign if necessary (see chapter “Realigning the seal (ship is in the water), and cleaning the surfaces”).



Remember that the ball cock (25) in the vent line at the seal must be open when the vent line ends above water line, otherwise vent manually at regular intervals.



5 MAINTENANCE

1.7 Maintenance of the seal during OPERATION

The SIMPLAN seal is classified by Germanic Lloyd in accordance with the rules laid down by the so-called ZKR (Central Commission for International Rhine River Shipping). Accordingly, the seal is maintenance-free for a minimum period of five years.

- It is recommended to check the seal water system with the pump in operation prior to each sailing. If scoops are used, the check should be carried out when the vessel starts moving.

1.8 Maintenance of the seal during LAYUPS

In order to prevent standstill corrosion in the seal:

- The flushing water pump must be switched on minimum once a week for about 5 minutes and the seal flushed through.
- If scoops are used (no pump system), the shaft must be turned by whatever means for at least 5 minutes per week.

5.1 Long Term Maintenance

Every 5 years when the ship is due for docking, renew the following parts:

- The Pneumostop (6).
- Constant-Pressure seal Body (14) with Sealing Ring (9) and O-Ring.(10)
- The O-rings (20) and (23).

To be checked and to be renewed or replaced if necessary:

- The Counter Ring (24).
- The Packing (1) at the Casing Ring surfaces.



6 TROUBLE SHOOTING



When working on the seal while the ship is floating, always:

- Prevent the shaft from turning.
- Inflate the "Pneumostop" emergency seal.
- Block the flushing line and drain the seal
- Secure the clamp ring (15) by fitting the installation tools (17, 18, 19) before slackening the screws (8).



If there is leakage, the seal unit in general, and the sealing ring faces in particular must be checked as soon as possible.

No.	Problem	Cause	Remedy
1	Seal is leaking during operation	Dirt between sealing rings	Clean surfaces of sealing rings (9 and 24) after inflating the Pneumostop when shaft is at standstill.
		Misalignment	Realign clamp ring (15) after inflating the Pneumostop when shaft is at standstill. See „Alignment check“.



No.	Problem	Cause	Remedy
2	Seal is leaking during operation	Compression set	<p>Pre-tension the boot/bellows (14) as follows:</p> <ul style="list-style-type: none"> Inflate the “Pneumostop” emergency standstill seal. Fit the tensioning screws and tighten the nuts (18) until the boot/bellows is held in place. Loosen the clamp ring (15) and release the tension on the boot/bellows until the two silicon carbide rings are making contact with each other without pressure. Then increase the tension on the boot/bellows until the tension value on the respective drawing is reached, plus a maximum of 3 mm more beyond the previous position of the clamp ring on the shaft. <p>If the boot/bellows has a compression set such that the drawing dimensions cannot be achieved, the boot/bellows must be replaced.</p>
3	Pneumostop does not deflate	Valve (32) insert keeps air in the Pneumostop.	Remove the air valve (32) insert to remove all air from the Pneumostop.
		Air supply line pressurised.	Vent the air supply line.
4	Water flows out of the drain continuously (during repair)	Flushing water line is not closed.	Close flushing water line.
		Pneumostop is not inflated, is damaged, or unable to seal as dirt is between the Pneumostop and the shaft surface.	Activate Pneumostop, replace if damaged or clean area between Pneumostop and shaft surface.
5	Seal runs hot	Valve(s) in vent line is closed	Vent line valve(s) must be open.
		No flushing water flow	Water must flow through flushing line into the seal.

Tab. 1: Trouble shooting SIMPLAN

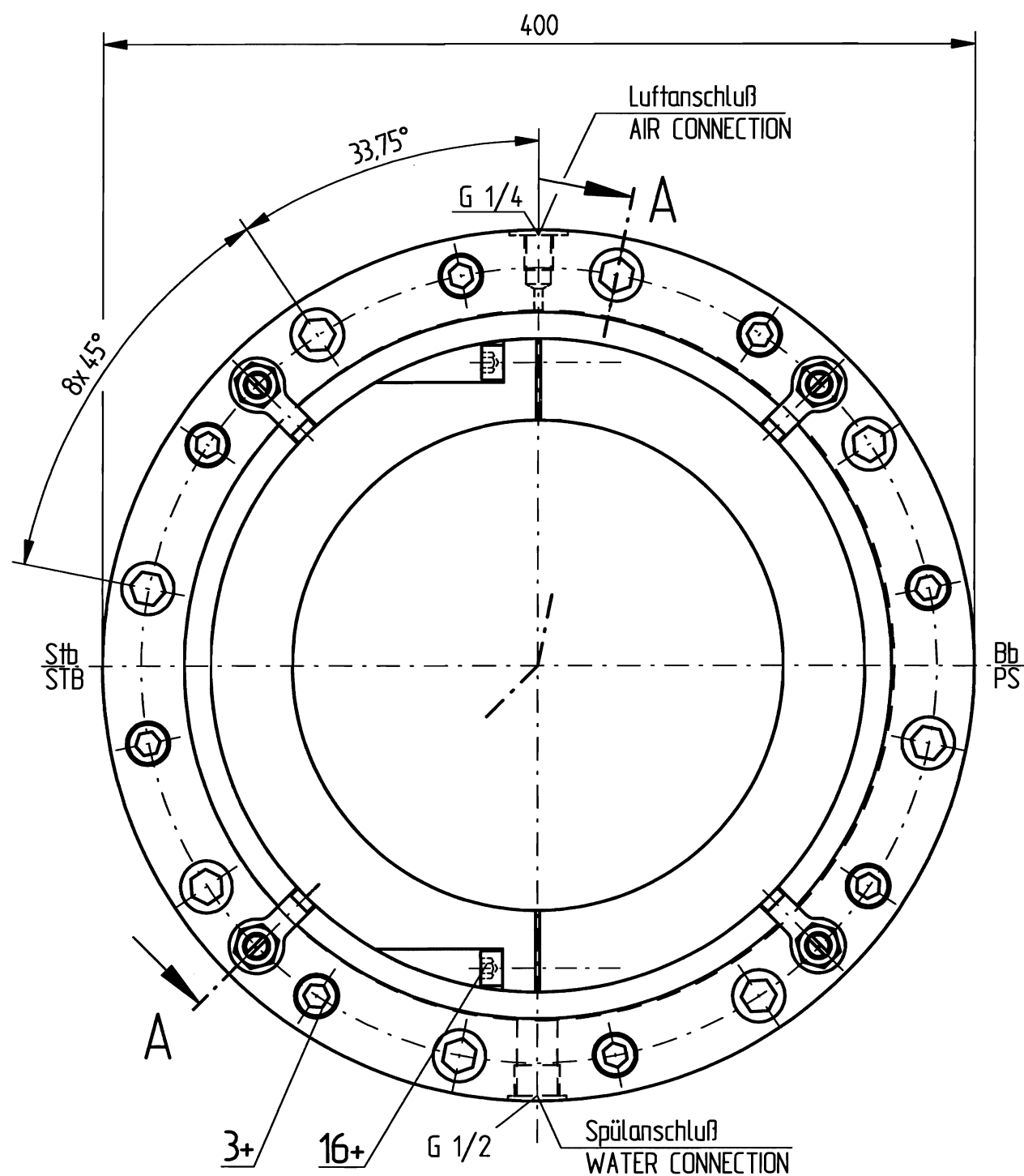
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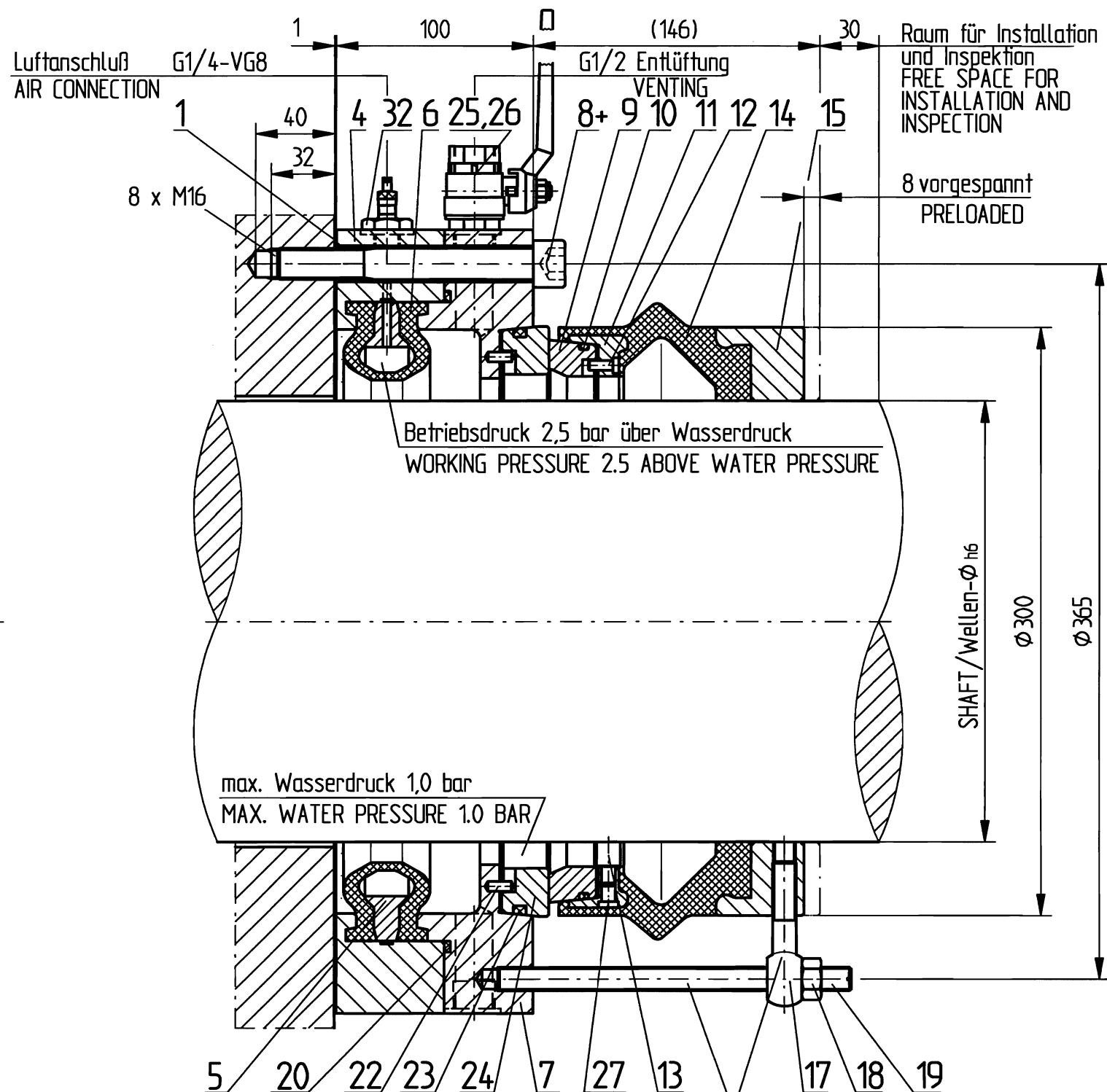
erforderliche Wassermenge für die Abdichtung
im Normalbetrieb 1l/h pro 1mm Wellendurchmesser
WATER QUANTITY REQUIRED FOR SEAL AT STANDARD
OPERATION 1L/h PER 1mm SHAFT DIAMETER

Zulässige Wellenbewegung im Betrieb
ALLOWABLE SHAFT DEFLECTION DURING OPERATION
radial $\pm 3\text{mm}$
axial $\pm 3\text{mm}$

+ : Schrauben mit LOCTITE 243/245 gesichert
SCREWS SECURED WITH LOCTITE 243/245

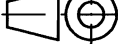


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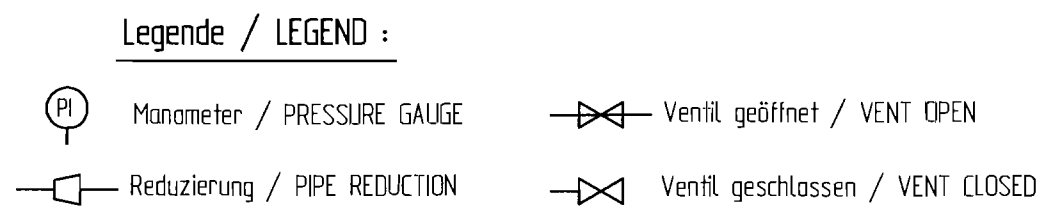
Vor Inbetriebnahme Spannwerkzeug entfernen !
REMOVE INSTALLATION TOOLS BEFORE OPERATION !


Anzugsmoment fuer / TIGHTENING TORQUE FOR		
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16	M 10	30
3	M 12	50
8	M 16	120

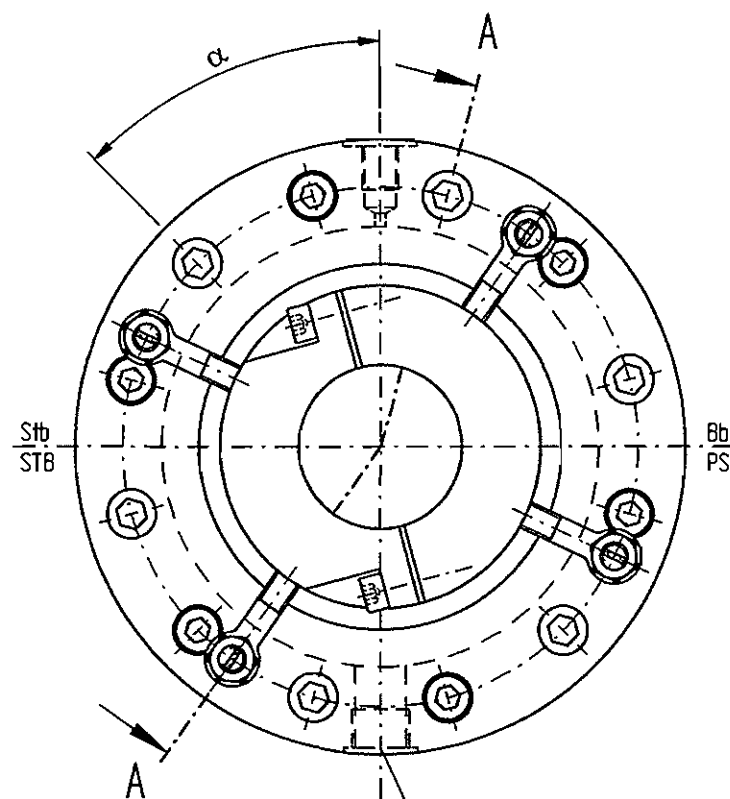
SHAFT-/Wellen-Ø 225 - 240				Projektion: 		Maßstab %		WEIGHT: 66,5 kg	
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				Bearb.	Datum 03.02.2003	Vordere Abdichtung, Gr.225 FWD SEAL, SIZE 225			
				Gepr.	26.02.08				
				Norm					
				CAD:	G:8EE9440D.SZA				
						Blohm + Voss Industries GmbH		SGC : 3-218-0008-000.1 ·	
1	Anzugsmomente neu	22.02.2008	Old			Ers. f.:		Ers. d.:	
Zust.	Änderung	Datum	Name	Urspr.					

Einzelteilliste / PARTS LIST				Thyssen B+V Industrietechnik
SIMPLAN Abdichtung / SIMPLAN SEAL vorn / FORWARD		Zeichnungs-Nr. / DRAWING-No.		Seite/ PAGE
Größe / SIZE: 225 SiC-P		SGC:3-218-0008-000.1 -		1 von / of 2
Pos. POS.	Anzahl No.	Benennung NAME	Zeichnungs-Nr. DRAWING-No.	Werkstoff MATERIAL
1	1	Flachdichtung GASKET	SGC:4-218-0001-001.	AFM 34
3	8	Zylinderschraube M12 x 50 HEXAGON SOCKET HEAD CAP SCREW	DIN 912	A4 - 70 STAINLESS STEEL
4	1	Gehäusering CASING RING	SGC:3-218-0005-004.	Bronze BRONZE
5	1	Einlegering NECK RING	SGC:4-218-0003-005.	Bronze BRONZE
6	1	Pneumostop PNEUMOSTOP	SGC:4-218-0003-006.	Neopren NEOPRENE
7	1	Gehäusering CASING RING	SGC:3-218-0006-007.	Bronze BRONZE
8	8	Zylinderschraube M16 x 130 HEXAGON SOCKET HEAD CAP SCREW	DIN 912	A4 - 70 STAINLESS STEEL
9	1	Gleitring SEALING RING	SGC:4-218-0006-009.	SiC-3
10	1	O-Ring ø 270 x 3,5 O-RING	DIN 3771	Viton VITON
11	1	Einlegering NECK RING	SGC:3-218-0001-011.	Bronze BRONZE
12	2	Stopfen PLUG	SGC:4-216-0001-012.	Bronze BRONZE
13	8	Zentrierstift CENTERING PIN	SGC:4-216-0002-013.	Bronze BRONZE
14	1	Gummibalg CONSTANT-PRESSURE SEAL BODY	SGC:2-218-0001-014.	Neopren NEOPRENE
15	1	Klemmring, geteilt CLAMP RING, SPLIT	SGC:3-218-0001-015.	Bronze BRONZE
16	2	Zylinderschraube M10 x 35 HEXAGON SOCKET HEAD CAP SCREW	DIN 912	A4 - 70 STAINLESS STEEL
17	4	Augenschraube M12 x 60 EYE BOLT		St STEEL
18	4	Sechskantmutter M12 HEXAGON NUT	DIN 555	St STEEL
19	4	Gewindebolzen M12 x 180 THREADED BOLT	SGC:4-216-0001-019.	St STEEL
20	1	O-Ring ø 330 x 4 O-RING	DIN 3771	Perbunan PERBUNAN

Einzelteilliste / PARTS LIST				Thyssen B+V Industrietechnik
SIMPLAN Abdichtung / SIMPLAN SEAL vorn / FORWARD		Zeichnungs-Nr. / DRAWING-No.		Seite/ PAGE
Größe / SIZE: 225 SiC-P		SGC:3-218-0008-000.1 ✓		2 von / of 2
Pos. POS.	Anzahl No.	Benennung NAME	Zeichnungs-Nr. DRAWING-No.	Werkstoff MATERIAL
22	2	Paßkerbstift 5 x 12 GROOVED PINS	DIN 1472	Chromstahl STAINLESS STEEL
23	1	O-Ring ø 285 x 5 O-RING	DIN 3771	Viton VITON
24	1	Gegenring COUNTER RING	SGC:4-218-0003-024.	SiC-2
25	1	Kugelhahn G 1/2 i/a BALL COCK	03-117 201/12	MS/Ni
26	1	Dichtband SEALING TAPE		PTFE
27	8	Stopfen PLUG	SGC:4-216-0001-027.	Bronze BRONZE
32	1	Pneumostop Ventil G 1/4 – VG8 PNEUMOSTOP VALVE	18-080-041.1	Ms BRASS

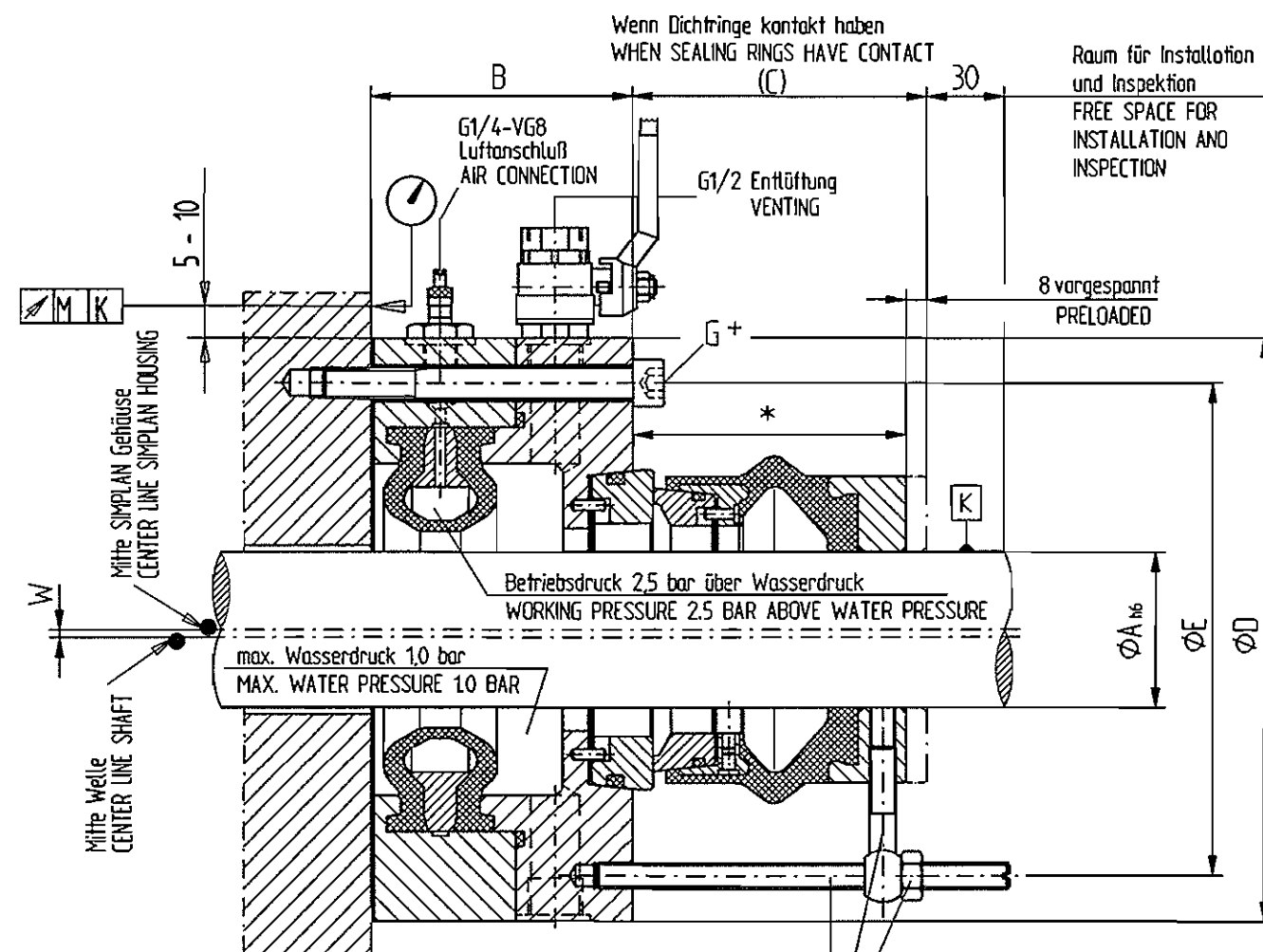


SIMPLAN						Maßstab %				
						Empfehlung / RECOMMENDATION				
				Beacht.	Datum 25.09.2002	Ordach	Kühlwasserdigramm COOLING WATER DIAGRAM			
				Gepr.	25.10.02	<i>SG</i>				
				Norm						
				CAD:	G00002726.SZN	MS22				
				 B+V Industrietechnik GmbH			SGC : 3-201-0011-000 .0			Blatt
Zust.	Änderung	Datum	Name	Urspr.	Ers. f.:	Ers. d.:				B



Zulässige Wellenbewegung im Betrieb
ALLOWABLE SHAFT DEFLECTION DURING OPERATION
radial ± 3 mm
axial ± 3 mm

G1/2 Spülanschluss
Erforderliche Wassermenge für die Abdichtung
im Normalbetrieb 1 l/h pro 1 mm Wellendurchmesser
G1/2 WATER CONNECTION
WATER QUANTITY REQUIRED FOR SEAL DURING NORMAL
OPERATION: 1 l/h PER 1 mm SHAFT DIAMETER



Vor Inbetriebnahme Spannwerkzeug entfernen!
REMOVE INSTALLATION TOOLS BEFORE OPERATION!

Größe SIZE	Wellendurchmesser SHAFT DIAMETER ØA h6	B	(C)	ØD	ØE	α	G	M max.	W *** max.
60	60 - 69	101	114	225	190	45°	6 x M12	1,6	± 2
70	70 - 79	101	114	235	200	45°	6 x M12		
80	80 - 89	101	114	245	210	45°	6 x M12		
90	90 - 104	101	134	255	220	33,75°	8 x M12	1,8	
105	105 - 119	101	134	270	235	33,75°	8 x M12		
120	120 - 134	101	134	285	250	33,75°	8 x M12		
135	135 - 149	101	134	300	265	33,75°	8 x M12	1,6	
150	150 - 164	101	134	315	280	33,75°	8 x M12		
165	165 - 179	101	134	330	295	33,75°	8 x M12		
180	180 - 194	101	134	345	310	33,75°	8 x M12		
195	195 - 209	101	146	370	335	33,75°	8 x M16	2,2	
210	210 - 224	101	146	385	350	33,75°	8 x M16		
225	225 - 240	101	146	400	365	33,75°	8 x M16		

* * Bei Verdopplung des max. zulässigen Wertes
ist eine Neuausrichtung des Gehäuses notwendig
IF THIS MAX. ALLOWABLE VALUE HAS DOUBLED,
SIMPLAN HOUSING HAS TO BE READJUSTED

* max. zulässige Abstands-Abweichung
im Bereich der vier Augenschrauben:
MAX. ALLOWED DISTANCE DEVIATION $\pm 0,3$ mm
AT THE FOUR EYE BOLTS:

+ Schrauben mit LOCTITE 242/243 gesichert
SCREWS SECURED WITH LOCTITE 242/243

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ThyssenKrupp B+V Industrietechnik GmbH

				Maßstab 1:1	
				SIMPLAN SEAL TYP: SIC-P	
				FWD SEAL DIMENSIONS WITH TOLERANCES	
				SGC: 3-201-0012-000.0	
				B+V Industrietechnik GmbH	
				Ers. 1: 2	
				Ers. d: 1	

SIMPLEX COMPACT

SPARE PARTS ORDERING

SPARE PARTS ORDERING



All parts / replacements shall be ordered from Blohm + Voss Industries GmbH by furnishing the following information:

- The information marked by * on the cover page
- Designation of the parts required **
- Pos.-No. of the parts required **
- Quantity of the parts required **

** See enclosed drawings in accordance with cover page

Please use the following contacts:

Blohm + Voss Industries GmbH

Ship components spares / service

Department MS 30

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20457 Hamburg, Germany

Or one of our worldwide service stations:

(see enclosed leaflet)

Phone: +49 40 3011 - extension

Fax: +49 40 3011 -1987 (seals and separators)

Fax: +49 40 3196189 (stabilizers, also dept. head)

Company web address: www.bv-industrie.de

Extention	Activities
-1195	Quotations for seal spare parts
-2120	
-2395	Commercial handling of orders for seal spare parts, and Huhn-seals
-2964	Delegating technicians for seals and TURBULO separators
-1684	Commercial and technical handling of orders for seal spare parts
-1283	Commercial handling of orders for seal spare parts
-2967	Commercial and technical handling of spare parts orders and quotations for TURBULO separators
-2308	Guarantee handling and service for stabilizers and steering gears
-1689	Spare parts order processing, delegating technicians for stabilizers and steering gears
-1676	Guarantee handling and service for stabilizers and steering gears
-1276	Guarantee handling and service, technical consulting and support for seals, TURBULO separators and bearings
-1673	
-2963	Commercial and technical handling of orders for SIMPLAN seal spare parts

Sales Agents for SIMPLEX and TURBULO PRODUCTS and **Service Stations** for SIMPLEX Seals Worldwide



A company
of ThyssenKrupp
Marine Systems

Blohm + Voss Industries

Blohm+Voss

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Malaysia Navy

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SIMPLAN Seal

Split Ring Assembly

Model SIC-P

Instructions:

Removing the unsplit and installing the split sealing rings (9) and (24)

1. Removal

- Prerequisites:
- Ship in dock **or**
 - Pneumostop inflated to 2,5 bars above water pressure and checked for leaks
 - Flushing-water supply de-activated
 - Water drained from the Simplan seal
 - Split rings (9, 24), new O rings (10, 23), A+B adhesive and heater for O-rings on hand
-
- Clean the surface of the shaft around 150 mm behind the clamp ring (15) thoroughly

Clamp ring:

- Release the tension of the constant-pressure seal body (14) by loosening the screws (16). Do not unscrew the screws (16) entirely, or remove the halves of the clamp ring (15) from the constant-pressure seal body



Due to the initial tension, the clamp ring (15) may jump backwards a bit when the screws (16) are loosened.

- Retract the clamp ring (15) with the constant-pressure seal body (14) and rings (11) and (9) from the casing far enough that both ring (9) and ring (24) can be extracted freely (see also attached sketch).

Sealing ring:

- Remove ring (9) from ring (11), for example by levering it out with two tools applied at opposite sides.
- Destroy ring (9), for example by hitting its outer diameter with a hammer.



SAFETY NOTE: Because of the fragments that may fly around, the technician should wear appropriate safety clothing and safety goggles!



SIMPLAN Seal

Split Ring Assembly



To prevent splinters getting into the seal, the ring (9) should be wrapped with rags.

Counter ring:

- Remove ring (24) from ring (7), for example by levering it out with two tools applied at opposite sides.
- Destroy ring (24) (see notes for ring (9)).
- Cut up the O rings, and dispose of them together with the fragments of the ring.
- Remove all fouling, splinters, etc. carefully from along the shaft between the casing (4, 5, 6, 7) and the clamp ring (15) with constant-pressure seal body (14) and ring (11), and clean the surface of the shaft thoroughly.

2. Installation

General safety hints:

- Do not remove the new rings (9, 24) from their packaging until immediately before installing them.



The super-finished sealing surfaces of the sealing ring (9) and the counter-ring (24) are very delicate, and must not be damaged under any circumstances!



Make absolutely sure that no oil or grease gets onto the bearing surfaces of the silicon-carbide rings (9, 24). These surfaces must be clean and dry!



Make sure that no foreign bodies get between the fracture surfaces of the ring halves!



SIMPLAN Seal

Split Ring Assembly

Counter ring

- Cut through the O-ring (23) supplied, place it around the shaft in the section between the casing ring (7) and constant-pressure seal body (14), and glue it together again with A+B adhesive, with the aid of a heater.
- First unpack ring (24), taking special care not to damage either the sealing surface or the fracture surface of the ring.
- Place the halves of the ring around the shaft, paying attention to the direction of taper (the smaller diameter must face towards the casing ring (7)), and carefully join them so that the fracture surfaces match precisely.
- Grease the O-ring (23) lightly, and insert it into the O-ring groove in ring (24).
- Slide the complete ring (24) into the taper of the casing ring (7), paying particular attention to the position of the keyways with respect to the grooved pins (22); see also attached sketch, steps 1 to 3.

Sealing ring

- Cut through the O-ring (23) supplied, place it around the shaft in the section between the casing ring (7) and constant-pressure seal body (14), and glue it together again with A+B adhesive, with the aid of a heater.
- Unpack ring (9), taking special care not to damage either the sealing surface or the fracture surface of the ring.
- Place the halves of the ring around the shaft, paying attention to the direction of taper (the smaller diameter must face towards the neck ring (11)), and carefully join them so that the fracture surfaces match precisely.
- Grease the O-ring (10) lightly, and insert it into the O-ring groove in ring (9).
- Slide the complete ring (9) into the taper of the neck ring (11), paying particular attention to the position of the keyways with respect to the plugs (12); see also attached sketch, steps 4 to 6.



SIMPLAN Seal

Split Ring Assembly

Clamp ring

- Slide the clamp ring (15) together with the constant-pressure seal body (14) and rings (11) and (9) up against the counter-ring (24).
- Position the installation device (17, 18, 19).
- For the initial position, turn the nuts (18) with your fingers against the eyebolts (17) until the bearing surfaces of the counter-ring (24) and sealing ring (9) are in contact.



In the initial position, the deviation in the distance between the rear edge of the clamp ring (15) and the front edge of the casing ring (7) in the vicinity of the eyebolts (17) should not exceed $\pm 0,3 \text{ mm}$.

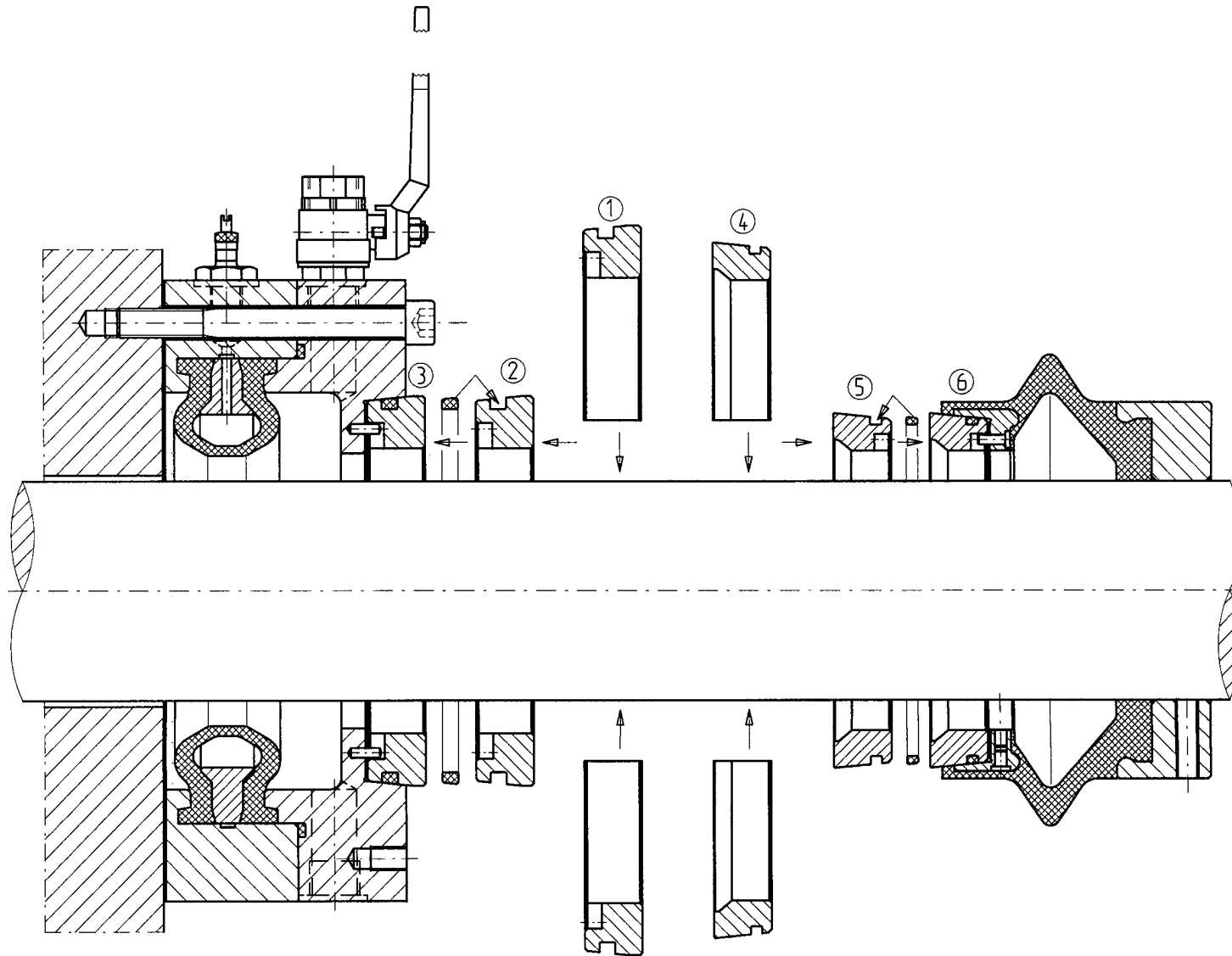
- Tighten the nuts (18) clockwise half a turn with a wrench, until the pre-loading given in the drawing has been reached.
- Fasten the clamp ring (15) with the screws (16) finally.



The final deviation in the distance between the rear edge of the clamp ring (15) and the front edge of the casing ring (7) in the vicinity of the eyebolts (17) should not exceed $\pm 0,2 \text{ mm}$.

Final steps:

- Dismantle the installation device (17, 18, 19), and store it on board.
- Vent the Pneumostop completely.
- Put the flushing-water supply into operation.
- Vent the Simplan seal



Ref. RD/JS 2007-03

COMPAC PROPELLER SHAFT BEARINGS SPECIFICATION

The information in this specification has been prepared based upon Thordon Bearings / Duwel Tecno experience and best practices developed over many years in designing and installing propeller shaft bearings.

More detailed information can be found in:

The Thordon Engineering Manual, the Thordon Water Lubricated Propeller Shaft Bearing Design Manual and Thordon's Bearing Sizing Calculation Program which supplement the information provided here.

If there are any questions regarding this specification, please contact Duwel Tecno.

Design

1. General

The bearing wear surface is Thordon COMPAC, a non-metallic, elastomeric polymer alloy. To reduce start-up friction and eliminate stick-slip, COMPAC's formulation includes special lubricants to provide a low coefficient of friction. To promote early formation of hydrodynamic film between the shaft and bearing, the lower (loaded) portion of the bearing is smooth, while the upper half of the bearing incorporates grooves for flow of the water lubricant/coolant.

The stern tube bearings shall be of water lubricated construction using forced water flow for cooling and lubrication. For strut type bearings, forward or astern movement of the vessel provides the cooling water flow.

The L/D ratio of the bearing shall be determined by taking into account the design pressure and the minimum shaft operating speed. As a general rule, the aft bearing L/D ratio can be 2:1 and the forward bearing 1:1, in accordance with the applicable classification society rules. In cases where the design involves only a stern tube bearing, this arrangement is acceptable as long as the bearing pressures are within classification society limits.

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2. Arrangement

Interference fitting is the recommended method for fitting the propeller shaft bearings. To achieve this, the bearing shall have a minimum wall thickness to permit interference fitting as specified by Thordon Bearing Sizing Calculation Program.

The bearing may be a solid tube or non-split and may comprise of single or multiple bearing segments. If the bearing is in multiple segments, an annular groove must exist between the segments to allow water flow in case of accidental angular misalignment.

3. Axial retention

All bearings must be fitted with mechanical means for limiting axial movement. Most commonly, this will be a step in the bore at one end and a circular, bolted retaining ring at the other.

4. Shaft liner

The shaft in way of the bearing should be fit with a circular, smooth continuous surface that may either be welded or a shrunk on liner. If a shaft liner is to be used, the liner shall be made from a good quality centrifugally cast bronze alloy or equivalent material with minimum thickness in accordance with classification society requirements.

Nickel aluminum bronze is not recommended as a shaft liner material. Please contact Duwel Tecno for other options.

5. Corrosion protection

If the shafting is made from a ferrous material, then the sections of the shaft exposed to seawater shall be suitably protected from corrosion. The shaft coating shall be applied in accordance with the manufacturers recommendations with care to be taken to ensure the integrity of the coating where it meets the shaft liners.

6. Cooling water

Cooling/lubrication water shall be supplied at the forward end of the stern tube so that it flows over the full length of the forward bearing through the stern tube, then over the full length of the aft bearing before exiting outboard.

The recommended method of supplying water to the stern tube is with a dedicated pump, however other methods are acceptable provided that the minimum water flow requirements are met at all shaft speeds. The water should be as cool as possible and water above 40°C (104°F) should be avoided.

The minimum water flow rate for COMPAC bearings is 0.15 liters per minute per millimeter (1 U.S. gal. per minute per inch) of shaft diameter.

For strut bearings, water flow is normally provided by the forward motion of the vessel. To ensure that the water supply is sufficient, there needs to be sufficient opening area at the forward and aft ends of the strut.

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The water supply piping arrangement shall include an electrical flow switch indicating low flow that is connected to an alarm in the control room or bridge. The low flow alarm should be set to alarm at a flow rate of 80% of the recommended flow rate.

If required by the customer, an additional flow meter providing a quantitative reading of water flow can be installed and situated in such location to be easily monitored by the ship's engineer.

7. Filters

Typically, the removal of abrasives between two operating surfaces will prolong the wear life in most mechanical systems. In blue water operation, the removal of abrasives is not normally required. However, if the vessel is to operate in waters containing sand or other abrasives, it is recommended to remove such abrasives to minimize bearing wear.

The removal of abrasives can be accomplished by many methods. The method chosen should remove abrasive particles down to a size of between 100 to 200 microns.

9. Seals

A face or lip seal is recommended, however other water lubricated seal options can be used.

Installation

The recommended method for fitting COMPAC bearings is to install using an interference fit. To ensure that the force generated to hold the bearings is sufficient, the dimensions of the machined bearing should be verified against the design dimensions for the installation.

The bearings can be installed with either dry ice or liquid nitrogen. During installation, it is recommended to leave gaps between the bearing segments and the retaining rings. The lower (loaded) part of the bearing I.D. is smooth and the upper half of the bearing has grooves. With multiple bearing segments, the grooves in the bearings should be aligned. Further information can be found in the Thordon Water Lubricated Propeller Shaft Bearing Design Manual.

Important: Please refer to our Marine Bearing Installation Manual regarding precautions when using a chocking compound.

Bearing Care – Installation to Delivery

Once the COMPAC bearing has been installed in the ship, it should be protected while in dry dock from:

1. Debris – the bearing should be protected against debris entering the bearing such as sandblasting material, paint, weld slag, etc.
2. Heat – the bearing should be protected from temperatures in excess of 50°C (122°F), especially from the heat of welding.
3. Chemical Attack – the bearing should be protected from any chemicals entering it.
4. Corrosion – adjacent metal parts should be protected from corrosion as the corrosion particles could enter the bearing and cause premature wear.

While the ship is afloat, the bearing should be protected from:

1. Debris – the bearing should be protected against waterborne debris such as sandblasting material or heavy sediment entering the bearing. The ship's propulsion system should not be tested at dockside or in dry dock basin where large amounts of debris can be stirred, allowing entry into the bearing.
2. Heat – the bearing should be protected from temperatures in excess of 50°C (122°F).
3. Chemical Attack – the bearing should be protected from any chemicals entering it.
4. Corrosion – adjacent metal parts should be protected from corrosion as the corrosion particles could enter the bearing and cause premature wear.
5. Marine Growth – The shaft should be turned two complete revolutions, every second day, to prevent marine growth.

Storage and Maintenance

Prior to Installation

Testing and experience indicate that Thordon COMPAC bearings can be stored for 5 years in the packaging provided and possibly in excess of 10 years.

The following steps will extend the life of the bearing in storage:

- 1. Store out of direct sunlight protected from weather, preferably in warehouse or similar.**
- 2. If possible, wrap the bearing in plastic wrapping or similar**
- 3. Store at ambient temperature – avoid excessive humidity and temperatures above 40°C (104°F).**
- 4. Avoid contact with solvents**
- 5. Store tubular material on end to minimize product deformation**

Long-term exposure to sun (ultraviolet radiation) may cause the surface of the material to undergo a colour change. However, once the surface layer is removed, the underlying material will be original colour and still maintain its physical properties.

Maintenance in Service

The wear of stern tube bearings is generally caused by either abrasive wear or overheating caused by excessive loading, high vibrations or reduction in cooling water to the bearings.

In Harbour

When the ship is in harbour for extended periods of time, marine growth may adhere to the shaft liner and lead to an increase in abrasive wear of the bearing. To try and prevent marine growth on the shaft, we recommend that the shaft be rotated 2.5 revolutions every three days.

At Sea

The filters should be monitored to ensure that they do not become clogged reducing water flow to the bearings.

Water Supply

The water supply to the stern tube should be fit with a flow-measuring device to alarm if the flow should go below .12liters/minute/mm shaft diameter. The flow meter should be checked on a quarterly basis to ensure that the setting is correct.

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Bearing Wear

The bearing will provide many years of service provided that it is operated and maintained properly. To provide information for future renewal due to wear the bearing clearance should be measured on an annual basis.

Divers should check the clearance every six months by fitting a feeler gauge into the space between the bearing and shaft at the aft end at top dead center. See figure 1 below.

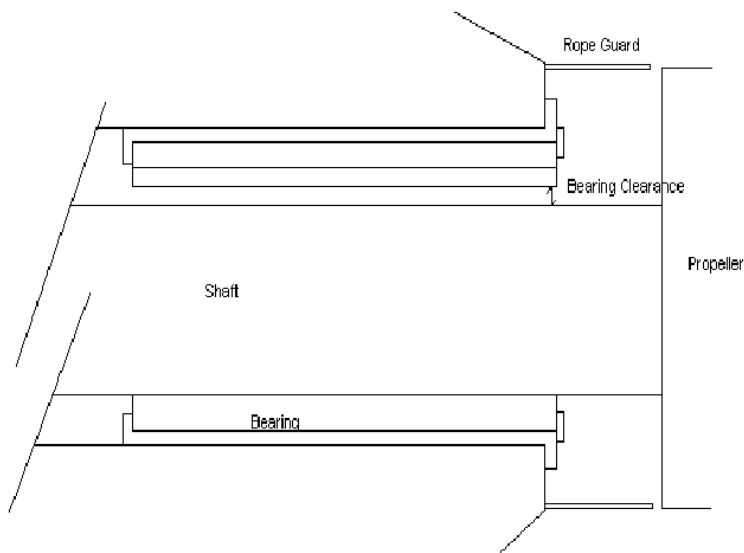


Figure 1

The readings should be recorded and maintained in the ships log.

In Drydock

When the ship is in Drydock, the clearance between the shaft and bearing at the aft end of the aft bearing at top dead center should be recorded. If the shaft is to be withdrawn, the shaft diameter and bearing bores should be measured at a minimum of three locations along the length and at top dead center and 60 and 120 degrees off of the vertical measurement.

Maximum Clearance

Water lubricated bearings, when properly designed, installed and maintained, will provide many years of satisfactory service. In service, however, the bearings will wear either as a result of abrasive or adhesive conditions.

As the bearing wears, the clearance in the bearing will increase and as clearance is normally easier to measure than wear, it is usual to state a maximum clearance limit for a bearing. The maximum clearance that can be accommodated is dependent upon both the bearing design and the shafting arrangement.

The maximum clearance recommended for water-lubricated bearings is then dependent upon the bearing design and the shafting arrangement. Bearing design includes bearing wall thickness, bearing configuration (grooved or ungrooved), loading, and shaft size while shafting arrangement dictates the positional relationship between the bearing and the propulsion machinery.

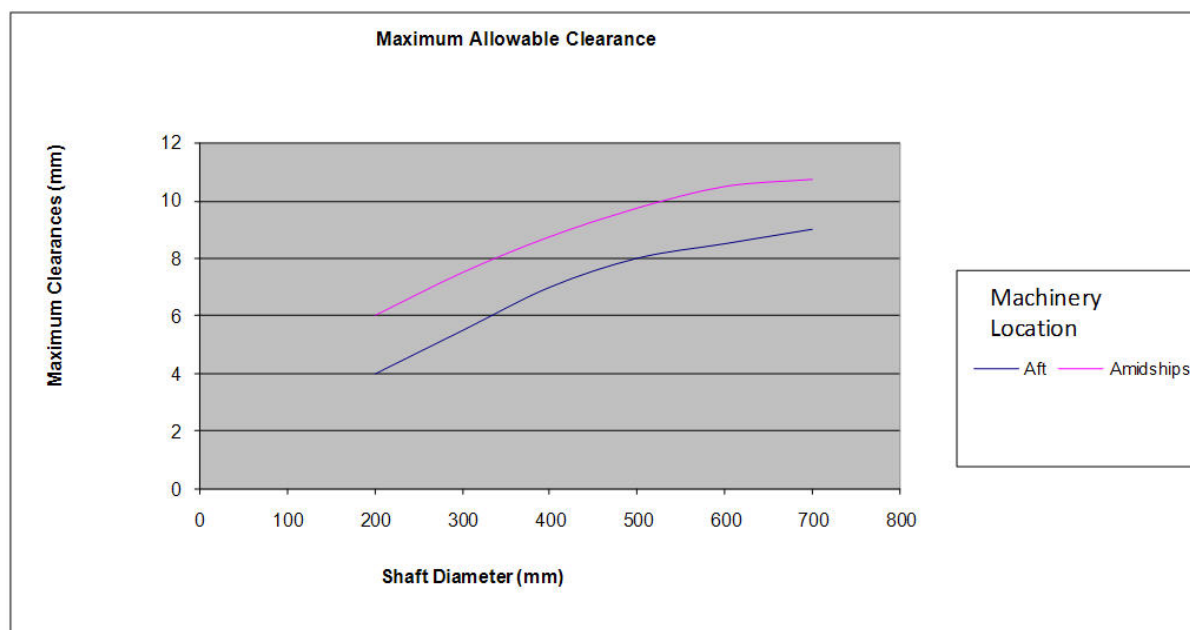
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The maximum bearing clearance is normally governed by the bending stresses in the shafting and the load transference to bearings located internally within the ship. The graph below provides a maximum recommended clearance for arrangements where the propelling machinery is either located amidships or is located aft.

The shafting arrangement needs to be reviewed to determine whether the machinery is considered aft or amidships. The machinery is considered amidships if there are 2 or more line shaft bearings forward of the stern tube. This ensures that if there is wear in the strut or stern tube bearings that load transference associated with the wear down does not affect the gearbox or propelling equipment. The machinery is considered aft if there is a single or no line shaft bearing forward of the stern tube.

Secondary considerations that need to be accounted are that there is sufficient bearing wall thickness above the edge of the retaining ring. In most normal applications, the wall thickness of the bearing is greater than the wear allowable to reach the maximum clearance. This ensures that when the bearing has worn to its maximum clearance, that the shaft has not contacted the bearing retaining ring and caused mechanical damage.

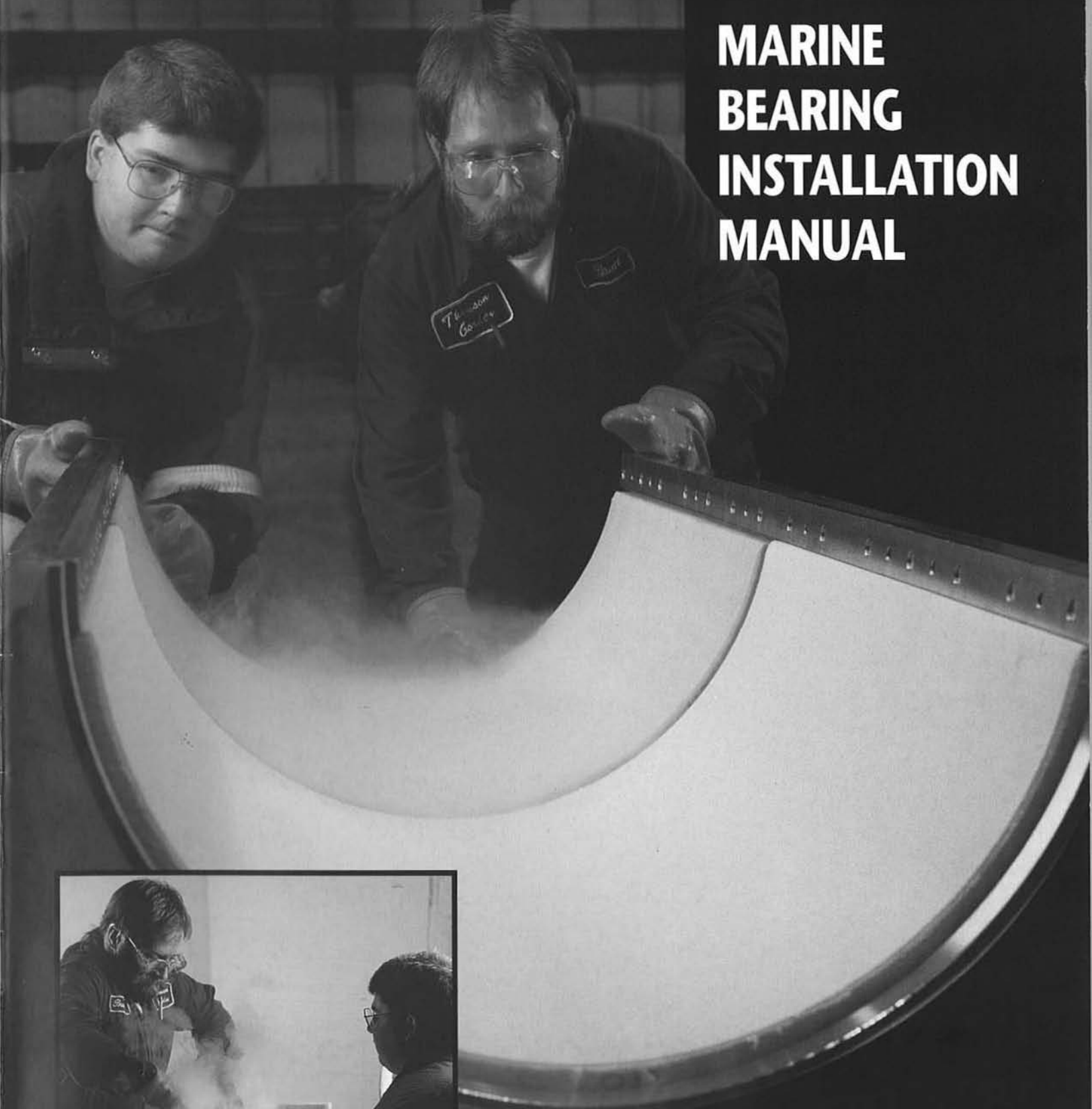
Maximum Allowable Clearance for Stern Tube and Strut Bearings



We trust that the above provides general guidelines in the determination of maximum clearances and wear.

If there are issues related to a specific installation, we recommend that you contact us at Duwel Tecno direct for more detailed information.

MARINE BEARING INSTALLATION MANUAL



VERSION 2.0

THORDON

BEARINGS INC. A member of the Thomson-Gordon Group

THORDON

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INTRODUCTION

Thordon is a unique polymer alloy developed by Thordon Bearings Inc. for use as a high performance bearing material, particularly in marine applications. Thordon bearings provide long life and offer a unique combination of low friction, high elasticity and good mechanical properties (abrasion and shock resistance). Thordon is homogeneous and has a relatively high coefficient of thermal expansion that facilitates freeze fitting. It is also resilient and shock resistant. Thordon marine bearings are much easier to handle and install than other traditional marine bearings. The important thing to remember is that Thordon is different from metallic bearing materials and therefore requires slightly different handling. Anyone accustomed to working with bronze or other metallic bearing materials will find that the recommended amounts of interference and running clearance for Thordon are greater than for metals. The securing methods common for bronze or bronze-shelled bearings must also be re-considered when fitting Thordon. For example, flanged fitting, set screwing along the O.D. and welding near the bearing are not acceptable with Thordon. Alternate methods of axially securing the bearing such as bolted end rings must be used. Thordon is a very easy material to machine. It is non toxic and machines dust free and therefore there are no health hazards involved.

Thordon is available in four grades for marine bearing system installations. These are XL, SXL, Compac and Composite. XL is the standard grade used in general marine applications. SXL is accepted as the preferred rudder material, especially for highly loaded rudder applications, because of its lower coefficient of friction and ability to run dry. SXL in TRAXL or Thor-Tape form is also used in deck gear applications. A separate instruction booklet is available. Compac is similar to SXL in composition and is specified for propeller shaft applications where low friction and long life are required. Composite is specially designed to provide long life in extremely abrasive conditions such as river boats, or suction cutter head dredges. All the Thordon grades are similar in their basic chemical composition, and the same approach can be taken to installing any of them. Where differences do exist, they will be pointed out in the text of this manual.

This manual is designed to provide all the information necessary to install Thordon marine bearings of any size. If you have any questions or concerns please contact your local Thordon Distributor, or Thordon Bearings Inc., for further information or design assistance. For easy reference we have divided the manual into chapters as follows:

- 1) Propeller Shaft Bearings***
- 2) Rudder Bearings***
- 3) Dimensioning***
- 4) Machining and Measuring Thordon***
- 5) Mating Surfaces and Housings***
- 6) Installation Methods***



CHAPTER 1

PROPELLER SHAFT BEARINGS

1.1.1 General

Thordon propeller shaft bearings are available to fit any size of shaft from 3/4" (20mm.) to 40" (1000mm.), and larger if required. They are available in a variety of forms that are described in the following sections of this chapter. Thordon propeller shaft bearings are normally fitted using an interference fit to hold them in place. In some applications anti-rotation or split tapered keys may be used. Thordon bearings are also bonded in place in certain circumstances. Axial retention rings are recommended for all Thordon bearing installations. Water lubrication is most commonly used with Thordon propeller shaft bearings but comments on oil lubrication are provided in section 1.4.2.

1.1.2 Bearing Length

Conventional propeller shaft bearings are normally supplied with a length/diameter ratio of 4:1 for the bearing next to the propeller. (Shorter lengths are used for inboard bearings.) This specification was based on the limited load bearing capability of other water lubricated propeller shaft bearings. Because of its significantly higher load bearing capability, Thordon is approved by most marine classification societies for use with a length/diameter ratio of 2:1. This means that Thordon bearings can be half the length of conventional marine bearings. Comments that relate specifically to the shorter length option will be provided where appropriate in this manual.

1.2 CYLINDRICAL BEARINGS

1.2.1 Fully Finished

Any Thordon bearing can be provided in fully finished form, ready to install. Such bearings may be machined by Thordon Bearings Inc, by the yard, or by your local distributor. Fully finished bearings can be supplied to meet any inch or metric housing and shaft combination. For standard sizes each bearing is given a reference code. Please refer to the Thordon Marine Bearing Standard Size List, for code names and nominal dimensions.

Fits and Clearances

Thordon fully finished bearings are normally designed for a press or shrink (interference) fit into the strut or stern tube. Sufficient oversize is allowed on the outside diameter of the bearing to prevent bearing movement, if the housing has not been pitted, corroded or rebored beyond its nominal diameter. Set screws are not recommended for securing the bearing in place. Fully finished bearings are not suitable for bonding into place unless they have been machined specifically for a bond fit. Final dimensions for machining Thordon bearings can be easily determined by using Thordon Bearing's computer sizing calculation program.

SXL, XL, Compac, or Composite

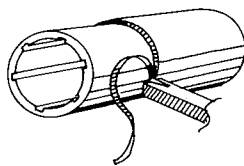
XL is the standard material for propeller shaft bearings. Compac is the special Thordon design incorporating the 2:1 length/diameter ratio, elimination of water grooves on the bottom of the bearing (to promote hydrodynamic lubrication), and the SXL grade of Thordon. Composite bearings are designed for extremely dirty water conditions where traditional bearing materials, and even the other grades of Thordon exhibit accelerated wear. For standard fully finished sizes of all styles, refer to the Thordon Marine Bearing Size List.

1:2:2 Semi Finished

Semi finished marine bearings are also available for shaft sizes from 2" (50mm.) up. A standard size range is produced for shafts up to 12" (300mm.). These bearings have similar dimensions to the fully finished bearings mentioned in section 1:2:1, but they have an oversize allowance on the outside, and undersize allowance on the inside. This extra material (approximately 1/16" (1.5mm.) up to 6" (150mm.) shaft size and 1/8" (3mm.) over 6" shaft) is added to give flexibility in machining to fit non-standard housings, shafts and liners. All standard semi finished bearings have the water grooves moulded in them. The O.D. and I.D. must be machined before installation. Refer to chapters 3 and 4 of this manual for dimensioning and machining instructions. Thordon Marine Bearing Size List provides nominal dimensions for Thordon semi finished marine bearings. They are available in XL, Compac or Composite as indicated.

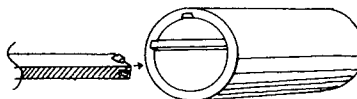
The "oversize" dimensions of semi finished bearings are based on calculated recommended dimensions for cold water installations, not on nominal shaft and housing sizes. Thus the I.D. of a semi finished bearing will be approximately 1.5mm (0.06") smaller than the calculated recommended I.D., not than the nominal I.D. (shaft size).

When semi finished bearings are supplied in two or more segments ("Grey" or larger) they come with an annular groove machined or moulded in one end of each segment. This is to facilitate water flow if there is misalignment of the water grooves. The annular grooves should be at the ends where the Thordon bearing segments meet.



1:2:3 Machined from Stock Tube

Thordon bearing material is available from most stocking distributors in standard tube form. These tubes are 13" (330mm.) long, and come in a variety of inside and outside diameters to suit almost any application. The only problem that arises in using stock tube for propeller shaft bearings is that this material does not have water grooves. Therefore it is necessary to machine these grooves before installation. TG drawing TG10520 on page 48 provides all the detailed information required for designing the appropriate groove configuration. Groove machining is normally done by using the boring bar on the lathe as a "shaper". Thordon Bearings Inc. has developed some special pneumatic router type cutters because of the number of water grooves that our machine shop cuts. Details are available on request.



Since Thordon stock tube comes in standard lengths of 13" (330mm.), it will often be necessary to use several pieces to make one marine bearing. The multiple piece concept is common with Thordon bearings. The only precaution that must be observed on installation is that the water grooves must be aligned. In view of the risk of misalignment on installation, we recommend an annular groove (approximately the width and depth of the longitudinal grooves) be machined on one end of each piece where it will meet another piece. The annular groove allows water to flow from one spool to the next even if the grooves are not perfectly aligned.

Inside and outside diameters of the Thordon bearings machined from stock tube can be determined by following the detailed calculation instructions in chapters 3 and 4.

Stave Construction

1:3:1 STAXL Semi Finished Staves

Thordon STAXL staves are preformed profile sections, each designed to cover a range of housing and shaft diameters with a minimum of machining. All STAXL staves are 1000mm. (39.4") long. The profile of STAXL staves is designed so that, in most cases, the only machining required is the boring of the inside diameter after the staves have been installed in the housing, carrier, or machine shop rig; or fly cutting of the ID surface of each stave to the appropriate radius before fitting. In the fitting process it is often necessary to cut the edge of one or two staves to achieve the required circumference.

STAXL staves are available in seven different sizes in cross sections coded A to G. Dimensions of each stave cross section are shown on drawing TG11069 on page 46. For each cross section, a range of shaft and housing sizes is shown. This information should be used as a guide to the suitability of a specific STAXL stave segment for a particular combination of shaft and housing. In addition, the thickness of the stave should be checked to ensure that there is sufficient material to machine to the required dimensions. It should be noted that, in all cases, the inside diameter of the STAXL staves must be machined to the appropriate radius. Some rubber staves are designed for tangential contact between stave and liner. This is not possible with Thordon.

If a standard STAXL stave segment is not suitable for a given installation "as is", it is normally possible to adapt one by machining the side angles and outside diameter radius. Stave thickness should be checked to ensure that there is sufficient material for the I.D. machining. If a very thin stave is required, it may be necessary to machine the O.D. of the stave, or deepen the water groove as machining of the I.D. only might eliminate the water grooves.



The number of staves required for an installation will vary with the actual size of the housing and the l/d ratio of the bearing. It also will vary with the number and size of keepers used (if any). The number of staves required to make a complete circle for a specific installation can be determined by using the following formula:

$$\frac{C-K}{W}$$

where *C*=Circumference of housing

K=Total width of all keepers

W=Chordal width of stave to be used

Note 1) The number of staves is rounded up to the next whole number when one keeper strip is used, or to the next even number when two keeper strips are used.

Note 2) The above number, to make a complete circle, must be increased appropriately for bearing lengths greater than one metre (39.37"). Avoid multiple small pieces to make up the stave lengths. The following table gives the chordal width of each STAXL stave cross section:

STAVE SEGMENT CHORDAL WIDTH

A	84 mm. (3.307")
B	78 mm. (3.071")
C	78 mm. (3.071")
D	75 mm. (2.953")
E	66 mm. (2.598")
F	58 mm. (2.283")
G	50 mm. (1.969")

The calculated number of staves required should be taken to the next highest number, or, in situations where two keeper strips are used, to the next highest even number.

1:3:2 Custom Moulded Staves

Thordon staves are also available in a fully moulded form. In this case full details of the housing and shaft including drawings where possible must be provided to Thordon Bearings Inc. in advance. Fully moulded bearings are designed to be fitted directly into the housing. No O.D. or I.D. machining

is required. It may, however, be necessary to machine the side of the last stave during fitting. The staves would normally be fitted using the freezing method. If we are advised in advance that freezing will not be used, then we can provide staves suitable for a drive fit. In this case keeper strips will be required to prevent rotation of the staves in the housing. When installing fully moulded staves we recommend that the inside diameter of the bearing be checked after assembly of the staves to ensure that it is consistent with the calculated inside diameter as indicated in chapter 3.

The "housing" referred to in this section can be either the stern tube or strut itself, or a bronze carrier. In either case the housing must be in good condition, and the dimensions must be as indicated in the drawings provided to Thomson-Gordon, or the fully moulded staves will not fit correctly. In view of this requirement, and the fact that production time for fully moulded staves may be 6-8 weeks, this type of stave is more suited to new construction than to repair.

Fully moulded staves are available in XL, SXL or Composite grades.

1:3:3 No-Groove Staves

Most conventional propeller shaft bearings have a length/diameter (L/D) ratio of 4:1, but Thordon can be used with half of the normal length (L/D ratio 2:1). This concept is accepted by the majority of the Marine Classification Societies. Some Societies require that the bottom half of a 2:1 L/D ratio bearing have no water grooves. This concept (developed by Thordon Bearings Inc.) facilitates the formation of hydrodynamic film and therefore lower friction. To meet this requirement, XL and SXL staves designed with no water grooves are available.

1:3:4 Dovetail Staves

Thordon staves are also available in dovetail form for installation in slotted housings. Ten standard sizes are available for different dovetail groove and housing dimensions. All staves are supplied with a flat top to be machined or bored after assembly and a standard 10° side angle. (15° side angle staves are available on special order). See the following table for stave dimension details.

NAME	SIZE NO.	(A) CHORD WIDTH		(B) THICKNESS	
		mm	inches	mm	inches
Boyne	1	43.00	1.693	0.875	7/8
Dnestr	2	46.18	1.818	0.875	7/8
Larch	3	49.61	1.953	0.938	15/16
Nethe	4	52.53	2.068	0.938	15/16
Rufiji	5	55.70	2.193	0.938	15/16
Eagle	6	58.88	2.318	0.936	15/16
Halil	7	70.00	2.756	1.063	1-1/16
Pelly	8	74.75	2.943	1.063	1-1/16
Nemunas	9	77.93	3.068	1.189	1-3/16
Tejo	10	81.10	3.193	1.189	1-3/16

Thordon dovetail staves are designed to be freeze fitted into the dovetail housing or carrier. After installing all the staves they must be line bored to the correct inside diameter. Many rubber type staves are designed with flat interior surfaces. This approach cannot be used with Thordon. A contoured inside surface is essential in all cases where Thordon is used. One acceptable alternative to line boring is fly cutting of each stave prior to installation.

1:4 LUBRICATION

1:4:1 Water

Water is the most common lubricant used with Thordon propeller shaft bearings. A positive flow of cooling water from a pump source is recommended. The flow rate should be 1 U.S. gallon per minute per inch of shaft diameter (0.15 litres/minute/mm.).

An increased water supply during the initial break in period is recommended if possible. Two water supply pipes are preferable to one large one. The cooling water should be as close as possible to the temperature of the water in which the vessel is operating. Water which has already been used to cool the main engine or other machinery before it reaches the bearings may not be suitable. Water over 60 deg C (140° F) can not be used as it will have a detrimental effect on the Thordon bearing.

Water should be injected ahead of the inboard bearing in a stern tube. Thordon bearings can run without water for a very limited time, but any sign of heating should be investigated immediately. For larger installations, temperature sensors and water flow alarms are recommended to ensure that an adequate flow of cool water is being maintained. If a vessel equipped with Thordon XL or SXL bearings spends a significant amount of time manoeuvring in very shallow or dirty water, consideration should be given to providing a source of clean water for bearing lubrication. A strainer or cyclone separator system can be used or even a temporary source of clean water (either sea ballast or fresh). The life of the bearings will be extended if clean lubricating water is supplied to the bearings under these conditions.

1:4:2 Oil

Thordon XL can be used in an oil filled stern tube if precautions are taken to ensure that the bearings are properly cooled. Due to the high viscosity and lower specific heat of oil (compared to water), and the low thermal conductivity of Thordon, there will be more heat buildup at the bearing surface than with traditional white metal bearings. This heat build up can be overcome by using an oil circulation pump and by ensuring that the stern tube is cooled by exposure to sea water in a flooded afterpeak, or by using a heat exchanger. Standard Thordon running clearances should be used in an oil lubricated system (not those for white metal). Provision should be made for thermal expansion. For oil lubricated stern tube installations we recommend that you consult your local Thordon distributor/technical representative, or Thordon Bearings Inc.

1:4:3 Grease

Grease lubrication of Thordon propeller shaft bearings is not recommended because grease cannot facilitate heat dissipation readily.

1:4:4 Thor-Lube

In the mid 1980's Thordon Bearings Inc. developed a unique pollution free stern tube system as an alternative to the conventional oil/white metal system. The system uses Thordon XL bearings and our special Thor-Lube lubricant. Thor-Lube is a completely water soluble lubricant which therefore eliminates pollution problems related to seal failure. The combination of Thor-Lube and Thordon XL bearings provides lower start up friction than a conventional oil/white metal system. Thor-Lube systems are available for new construction projects as well as for conversion of existing ships from other oil lubricated tailshaft systems. Detailed information on the Thor-Lube system is available from your Thordon distributor or from Thordon Bearings Inc.

CHAPTER 2

RUDDER BEARINGS

2:1 GENERAL

Thordon rudder bearings have become very popular for large and small vessels because of their long life and their ability to withstand impact and abrasion. Supplied in either tube or stave form, Thordon rudder bearings can operate with any type of lubrication - water, grease, oil, or, in the case of SXL, they can operate with no external lubrication at all. Water lubrication, or no lubrication are preferred because this eliminates the need for lubrication lines and pollution associated with grease lubrication. Where Thordon rudder bearings are expected to run dry, Thordon SXL grade should be used rather than XL because SXL has a lower dry coefficient of friction. SXL is also recommended for highly loaded submerged rudder bearings because its lower coefficient of friction provides better performance when high pressure reduces the lubricating properties of water.

Thordon bearings can be specified in all rudder bearing locations including stock, pintle and carrier bearings as well as bearings for tiller arm steering machines. On some spade rudder designs for military vessels Thordon SXL TRAXL bearings are recommended due to the high pressures generated by extreme manoeuvres at high speeds. In some older rudder configurations Thordon is not recommended for use in the bottom pintle position.

Thordon rudder bearings are now approved by some classification societies for pressures to 12 N/mm². This allows the designer to more closely match bearing pressure limits to the bending and torsion requirements for the rudder stock. Significant weight and cost savings can be achieved as well as a more slender rudder profile.

CYLINDRICAL BEARINGS

2:2:1 Complete tube

The most common type of Thordon rudder bearing is XL or SXL in tubular form. Because rudders move very slowly over a limited range, there is no need for a forced cooling water system, and therefore no need for the water grooves normally found in propeller shaft bearings. A full range of Thordon SXL rudder bearings in nominal diameters from 300 mm. (12"0) to 950 mm. (37") and an L/D ratio of 1.5:1 is available. Larger sizes can be supplied. Rudder bearings can also be made from standard stock Thordon tubes, although several tubes (normally 330 mm. (13") long) may be required to make a complete bearing.

Thordon rudder bearings are normally supplied in semi finished form for machining to the final dimensions required. (See chapters 3 and 4 for dimensioning and machining instructions.) Your local Thordon distributor also can supply fully finished bearings machined to the required dimensions and ready to install, if he is given the correct housing, shaft and operating environment information.

2:2:2 Split bearings

It is sometimes preferable to use split tubular bearings rather than complete tubes. Split bearings facilitate installation without removing the complete rudder, or completely dismantling the steering gear. Any Thordon tubular bearing can be split to facilitate installation. A standard milling machine is normally used for this purpose, although Thordon Bearings Inc. has developed technology for splitting rudder bearings without a saw cut, thus leaving no gap. If the splitting is accomplished by milling, then shims are normally used to fill the gap left by the cut. Assuming that the shims are the same width as the cut, then the bearings can be fully machined before cutting. Alternatively, they can be cut (split) in their semi finished form, and then bonded back together with **TG-75** for machining. This approach avoids the requirement for shims. Split bearings can be fitted with the same interference fit as tubular bearings. The inside diameter of the split bearings should be relieved along the edges of the split.

2:3 Stave Construction

Stave type bearings are sometimes used for large rudder installations, particularly for retrofit when it is desirable to avoid unshipping the rudder assembly or steering gear. Thordon XL or SXL can be supplied in stave form. Working with staves usually requires more time and labour than working with tubes, so the use of tubes is recommended when feasible. If Thordon is replacing laminated phenolic for example, just because the phenolic bearings was made in stave form is no reason to make the replacement Thordon bearing from staves.

2:3:1 Semi Finished Staves

A complete range of semi finished Thordon rudder bearing staves has not been produced because of the general preference for tube type bearings. Some sizes are available, however, for particularly large diameters and details are available from Thordon Bearings. Other sizes can be produced on request. Semi finished rudder staves are moulded to suit the required O.D., but must be machined on the I.D. to suit the specific stock dimensions and clearance requirements. The difference between rudder staves and STAXL propeller shaft staves is that the former do not have water grooves.

2:3:2 Fully Moulded Staves

When time permits, fully moulded rudder staves, ready to install, can be produced. To do this, Thordon Bearings Inc. must have full details of the housing, shaft and operating environment at least 6 weeks lead time before the staves are required.

2:4 LUBRICATION

2:4:1 Water

Pintle bearings are immersed under most loading conditions. Stock bearings may operate wet or dry. Since SXL is designed to run dry it is generally the best choice, allowing standardization. SXL is also recommended for highly loaded rudder bearings. The maximum recommended operating pressure for a water lubricated XL bearing is 5.5 N/mm² (750psi). For SXL, water lubricated or dry, this limit can be raised to 12 N/mm² (1680 psi). Thordon Bearings has no evidence that a water lubricated rudder stock or pintle bearing will last any longer than one operating dry.



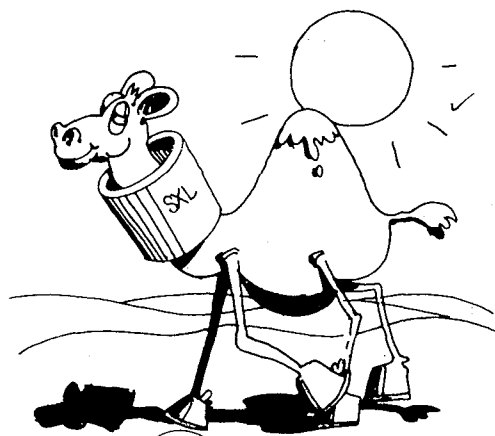
2:4:2 Grease

Grease lubrication can be used with any type of Thordon rudder bearing if the assembly is designed for grease lubrication. However, since one of the advantages of Thordon SXL is its ability to run dry, removal of an existing greasing system tends to make the Thordon installation more cost effective and eliminates a potential source of pollution.



2:4:3 Dry Running

If a rudder bearing is expected to run dry, Thordon SXL should be used. An initial application of grease will facilitate assembly and initial bedding in of the bearing.

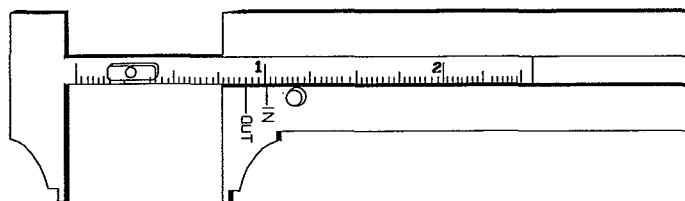


CHAPTER 3

DIMENSIONING

3:1 GENERAL

Dimensioning procedures for Thordon bearings are different from traditional bearing materials. Thordon bearings cannot be made to the same dimensions as the bronze, rubber, wood or other bearing materials they may be replacing. This chapter will provide the information necessary to dimension Thordon bearings. The process should be followed in the sequence indicated.



3:2 INFORMATION REQUIRED

The following information is required for dimensioning a Thordon bearing:

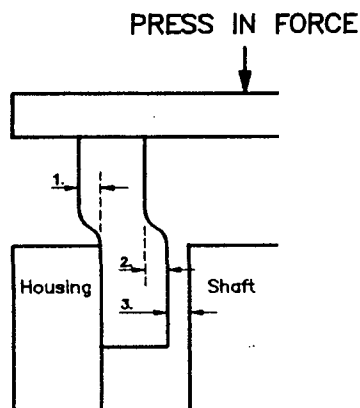
Housing:	<i>Maximum diameter</i> <i>Minimum diameter</i> <i>Roundness</i>
Shaft:	<i>Maximum diameter</i>
Temperature:	<i>Minimum expected operating temperature</i> <i>Maximum expected operating temperature</i> <i>Ambient temperature in the machine shop</i>
Lubrication:	<i>Water, Thor-lube, oil, grease, or none</i>
Application:	<i>Propeller shaft, rudder, or other</i>

It is important to check that the housing is round and has not been worn or pounded into an oval shape. Thordon, being a flexible elastomer, will adapt to the shape of the housing. See Chapter 6 for installation instructions if dealing with an out-of-round housing.

Prior to calculating bearing dimensions, the housing should be checked for alignment. If reboring is necessary, the bearing O.D. can then be sized to the new housing dimensions. If reboring is not appropriate see Chapter 6 for alternative installation procedures.

3:3 BEARING OUTSIDE DIAMETER TUBE TYPE BEARINGS

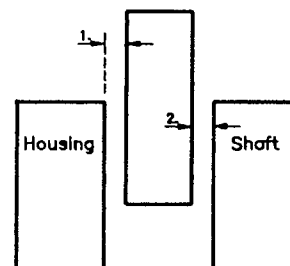
INTERFERENCE FIT PARAMETERS



Where: 1. Is Interference.
2. Is Bore Closure.
3. Is Installed Running Clearance.

Note: Minimum Installed Clearance =
Running Clearance
+ Thermal Expansion Allowance (if applicable)
+ Water Swell Allowance (if applicable)

BOND FIT PARAMETERS



Where: 1. Is Bond Thickness
2. Is Installed Running Clearance.

Note: Minimum Installed Clearance =
Running Clearance
+ Thermal Expansion Allowance (if applicable)
+ Water Swell Allowance (if applicable)

3:3:1 Interference

Thordon bearings are normally installed with an interference fit. The amount of interference will vary with the size of the bearing and with the minimum temperature at which it will operate. Additional interference is required for cold operation. Pages 39-42 provide graphs showing recommended interference at different variances from machine shop ambient. In all cases you should use the lowest temperature to which the bearing could possibly be exposed. Additional interference causes no harm, but insufficient interference for cold operations could cause the bearing to come loose in the housing. The amount of interference required should be added to the maximum housing diameter to give the minimum bearing outside diameter.

3:3:2 Machining Tolerance

The appropriate machining tolerance should be added to the minimum bearing O.D. figure calculated in 3:3:1 to give the maximum bearing O.D. Refer to page 24.

3:3:3 Summary

Maximum Housing O.D. + Interference = Minimum Bearing O.D.

Maximum Housing O.D. + Interference + Machining Tolerance = Maximum Bearing O.D.

3:4 BEARING INSIDE DIAMETER TUBE TYPE

3:4:1 Bore closure

Bore closure is the diametral reduction of the bearing I.D. that occurs when it is installed in a housing using an interference fit to hold it in place. The interference oversize is transferred to the bearing I.D. Page 43-44 gives the percentage of bore closure. This percentage should be applied to the average interference (calculated interference plus 50% of housing tolerance and 50% of machining tolerance on the bearing O.D.). The resultant figure will be the amount of expected bore closure. Actual bore closure may vary +/-15% from the calculated amount. Since the volume of a Thordon bearing at any given temperature remains constant, constraining the O.D. results in a reduced I.D. and a slight increase in length.

3:4:2 Running clearance

The recommended running clearance for Thordon bearings is given on Pages 37-38.

3:4:3: Dimensional changes due to water absorption

When immersed in water, Thordon only increases in volume 1.3% under normal conditions. Some of this expansion simply increases the amount of interference, but there is also an effect on the inside diameter of the bearing and length of the bearing. The normal water swell "Cs" calculation is:

$$Cs \text{ (diametrical)} = .011 \times \text{wall thickness}$$

Although axial water swell is not normally significant for propeller shaft bearings, it can become a significant factor for large rudder bearings. The calculation for axial water swell where required is:

$$Cs \text{ (axial)} = .005 \times \text{Length}$$

Thordon swells slightly more in warm water. An additional allowance should be calculated if the water temperature is higher than 25 deg C (80 deg F). Axial swell is important when calculating the gap to leave between the last bearing spool and the ring keeper. Refer to paragraph 3:6:6.

3:4:4 Thermal Expansion

In cases where the maximum operating temperature of a bearing exceeds by more than 10 deg C (18 deg F) the ambient temperature in the machine shop where it is machined, an allowance for Thermal expansion should be included in the bearing I.D. calculation. Thermal expansion is calculated as follows:

$$Ct = 2W \times \# \times (To - Ta)$$

where:

Ct = thermal expansion allowance

W = bearing wall thickness

$\#$ = coefficient of Thermal expansion for Thordon as follows:

XL (Centigrade)= 0.000178

XL (Farenheit)= 0.000099

SXL (Centigrade)= 0.00023

SXL (Farenheit)= .000128

To = Maximum operating temperature

Ta = Machine shop ambient temperature

3:4:5 Machining Tolerance

The appropriate machining tolerance must be included in the bearing I.D. calculation.

3:4:6 SUMMARY

Maximum shaft diameter
 + Bore closure allowance
 + Running clearance
 + Water swell (if any)
 + Thermal expansion (if any)

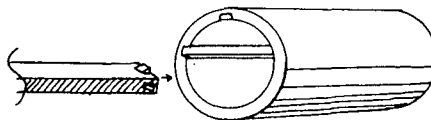
= Minimum Bearing I.D.

+ Machining tolerance

= Maximum Bearing I.D.

For standard shaft (or liner) sizes in propeller shaft bearing applications refer to Thordon Marine Bearing Standard Size List.

3:5 WATER GROOVES



3:5:1 Propeller Shaft Bearings

Thordon propeller shaft bearings should always have water grooves to facilitate an adequate flow of cooling water. Most small propeller shaft bearings are supplied with water grooves already moulded in place. When water grooves must be machined into an ungrooved tube, drawing TG-10520 (page 48) provides the necessary water groove design information. Some Thordon bearings, especially the Compac style 2:1 length/diameter ratio bearings, are supplied with water grooves in the top half only. This design improves hydrodynamic performance.

3:5:2 Rudder Bearings

There is no need for water grooves in Thordon rudder bearings.

3:6 STAXL STAVES

3:6:1 Introduction

In the past we have used several different methods for dimensioning Thordon STAXL staves. As a result of our extensive field experience in recent years, a more precise dimensioning method has evolved that we now recommend for all installations.

3.6.2 Pre Assembly

We believe that pre assembly is the most accurate method of dimensioning Thordon STAXL staves. In this method the staves, at room temperature, are placed in the housing until a gap of less than one stave width is left. For most installations with two keeper strips, each half of the bearing would be dimensioned separately. Once the staves have been placed in the housing use threaded jacking bars, a small Enerpac or other similar means to press them together to eliminate any gaps. (Refer to illustration on page 17.) With the staves pressed together measure the gap between the last stave and the keeper. Note this measurement.

3.6.3 Interference Calculation

Using the appropriate graph on pages 39-42 determine the recommended diametrical interference (as recommended for a tubular bearing in section 3:3:1). Multiply the diametrical interference by pi (3.1416) to convert it to a circumferential interference. In the typical case of two axial keeper strips, where each half of the bearing is dimensioned separately, divide the circumferential interference in two.

3:6:4 Final Stave Width

Add the calculated interference 3:6:3 (for the full or half bearing as appropriate) to the measured gap 3:6:2 to determine the required width of the final stave. Mill the last stave to this width.

3:6:5 Stave Assembly ID

IN ALL CASES THE ID OF THORDON STAXL STAVES MUST BE MACHINED TO THE APPROPRIATE DIAMETER. STAVES ARE SUPPLIED FLAT ON THE ID, BUT, UNLIKE SOME RUBBER STAVES, THEY CANNOT BE USED WITH THE FLAT ID. IT MUST BE CONTOURED.

Normally staves are line bored after installation in the housing, carrier, or machine shop dummy housing. In this case the inside diameter of the bearing will be maximum shaft diameter plus running clearance (3:4:2) plus water swell (3:4:3, plus thermal expansion allowance (3:4:4)(if required). Machining tolerance should be as indicated in 3:4:5.

3:6:6 Longitudinal Water Swell

End keepers or stops are always recommended with Thordon bearings as added security to prevent axial movement in the event of unbalanced loads, excessive vibration, or other unanticipated factors. A gap should be left between the end keeper and the staves to allow for axial water swell. This gap should be:

$$0.005 \times \text{bearing length}$$

3:6:7 Encapsulated Keeper Strips

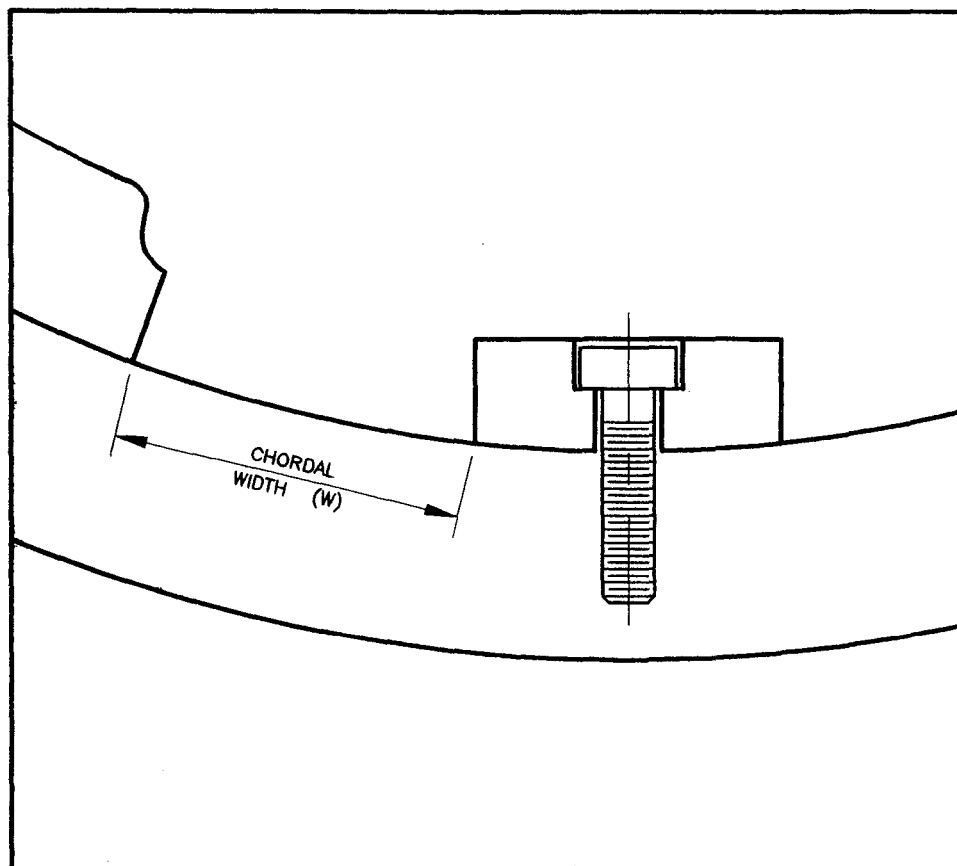
Occasionally stave installations are designed so that keeper strips fit into machined grooves in the back of staves rather than between staves. In this case dimensioning should be the same as for an installation using no keeper strips. Grooves should be machined in the backs of the appropriate staves. These grooves should provide ample clearance over the keepers so that a proper fit can be achieved even when the staves are frozen.

3:7 Dovetail Stave Assemblies

Thordon staves are also available in dovetail form for dovetail (slotted) housings.

Thordon Dovetail staves are designed for interference fitting into the slotted carriers. This ensures a snug fit throughout the length of the stave. Interference can be calculated using the same interference graphs as are used for tubular bearings (pages 39-42). For "Housing diameter" use the average slot width. The amount of interference will be the amount of oversize required on the stave width. The standard side angle of Thordon dovetail staves is 10 degrees. If the carrier has a 15 degree side angle, then the staves should be milled to suit.

The ID of the Thordon dovetail stave assembly must be machined. Although a flat interior surface is acceptable for some rubber staves, it is not acceptable for Thordon. The ID of the Thordon dovetail stave assembly should be calculated using the same approach as for tubular bearings except that bore closure need not be considered. the bearing ID will be shaft diameter plus running clearance (3:4:2) plus water swell (3:4:3) plus thermal expansion allowance (3:4:4) if required.



Use threaded jacking bars, a small Enerpac or other similar means to press the staves together so the chordal width (w) can be measured.

CHAPTER 4

MACHINING AND MEASURING THORDON

4:1 GENERAL MACHINING

Thordon is a hard tough elastomeric polymer product that can be easily machined. It is necessary, however, to remember that Thordon is a non-metallic, and must be machined differently than metal. Due to the elastomeric nature of Thordon it has a tendency to "move away" from anything that exerts pressure on it, including machine tools of all types. Thordon cannot be burnished or chipped, it must be **cut** with a **sharp** tool. The importance of sharp cutting tools can not be over emphasized if Thordon is to be successfully machined.

When thin wall bearings are being machined it is important to recognize that the exertion of excess pressure may actually deform the bearing. In some situations it may be necessary to use modified chuck jaws, to support the tube using a spider, plug or a mandrel or to mount the tube using a face plate.

Cutting speeds are also important. Low feed rates combined with too low a turning speed tend to produce a rough cut due to the toughness and elastomeric nature of Thordon. High speeds combined with a low feed rate may produce excessive frictional heat which results in a gummy galled finish. The most suitable speed/feed combinations are similar to those used when machining aluminium.

Clearances, as specified using the design information in this manual, may seem excessive in comparison to metals. Thordon, however, expands from temperature change and submersion in water as well as exhibiting bore closure shrinkage at a rate greater than 100% of interference. This is due to the incompressible nature of Thordon. The minimum installed clearance takes all of these factors into account. As well, clearance for a liquid lubrication film if the bearing is water or oil lubricated **and** safety clearance for frictional heat build up is also accounted for. The recommended running clearance should **not be decreased** without first consulting your Thordon distributor or Thordon Bearings Inc.

NOTE: Failure of the bearing is almost certain if adequate running clearance is not provided.

Virtually all operations that can be performed on metal, including machining, drilling, tapping, shaping, routing, sawing, milling and bonding, can be performed on Thordon. Thordon can also be worked or shaped with conventional hand tools. Keep in mind that carbide tipped cutting tools should be used to prevent heat build up and improve tool life.

4:2 MACHINING XL AND SXL

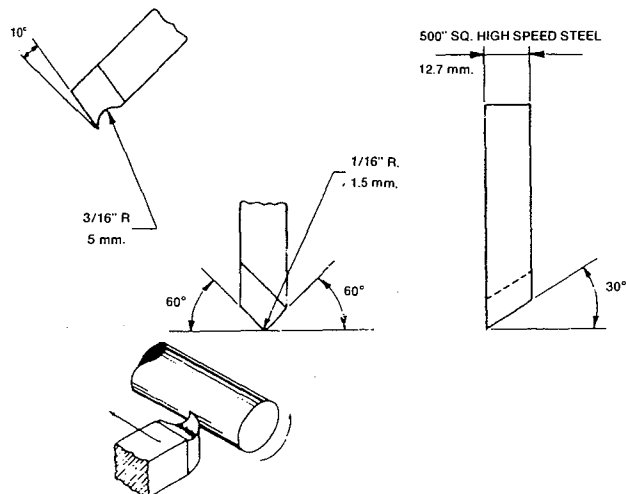
4:2:1 Cutting Tool

To machine Thordon it is critical that the correct cutting tool be used. The tool must be designed to slice and project the material away from the machined surface. When machining Thordon a continuous streamer is projected from the cutting tool. The cutting tool **must be sharp**. After grinding, the cutting tool should be honed with an oil stone to ensure a sharp cutting edge.

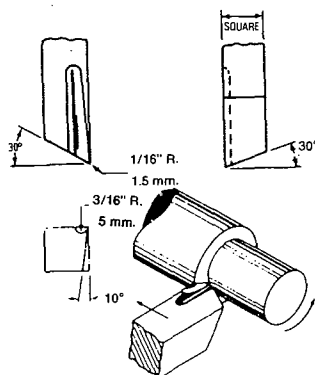
It is important when machining Thordon and particularly when boring, to ensure that the machining streamer is removed from the work. If this is not done, it will interfere with the cutting tool and a rough finish will result.

The drawings below illustrate the proper cutting tool configuration. High speed steel may be used for SXL and Composite. Tungsten carbide tool bits must be used with XL.

General Machining Tool Bit



Step Machining Tool Bit



4:2:2 Machining Speeds and Feeds

Normal turning speeds for bearings of various diameters are given in the chart below.

BEARING DIAMETER		
METRIC	IMPERIAL	RPM
75mm	3.0"	600
150mm	6.0"	450
300mm	12.0"	300
450mm	18.0"	150
600mm	24.0"	120
750mm	30.0"	95
900mm	36.0"	80

Normal cutting feed rates are as follows:

METRIC — Coarse Feed: 0.50 to 0.60 mm/Rev
Fine Feed: 0.40 mm/Rev.

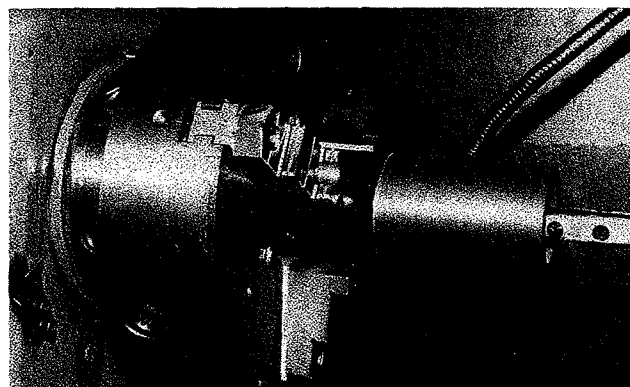
IMPERIAL — Coarse Feed: 0.020" to 0.025" /Rev
Fine Feed: 0.015"/Rev.

NOTE 1: The turning and feed speeds are provided as a guide only. The optimum speed may vary higher or lower depending on such variables as the length of tube, the wall thickness, and how the bearing is being supported, ie. simply chucked, spider at chuck or on a full length mandrel. As is common with all machining operations, some experimentation is required to obtain optimum results.

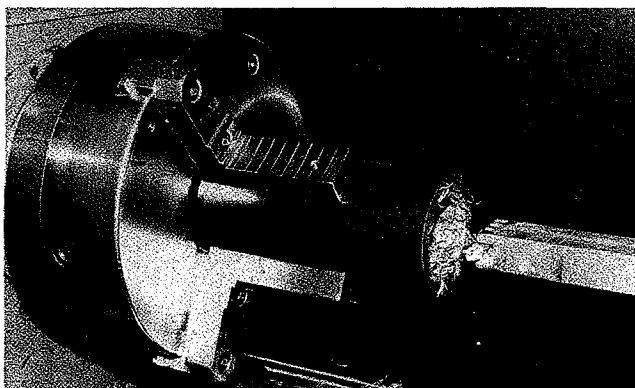
NOTE 2: Cutting lubricants are not required and are not recommended.

4:2:3 Bearing Set Up

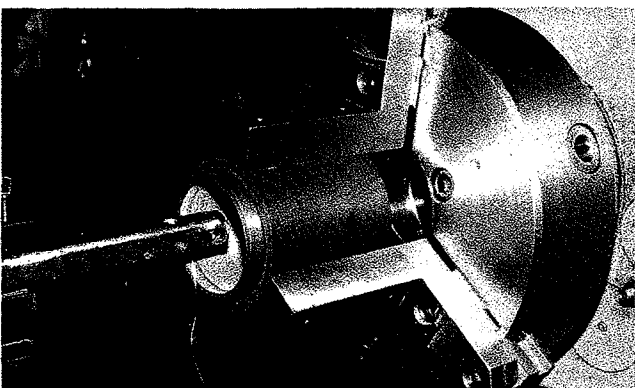
Machining - Partial length from a tube:



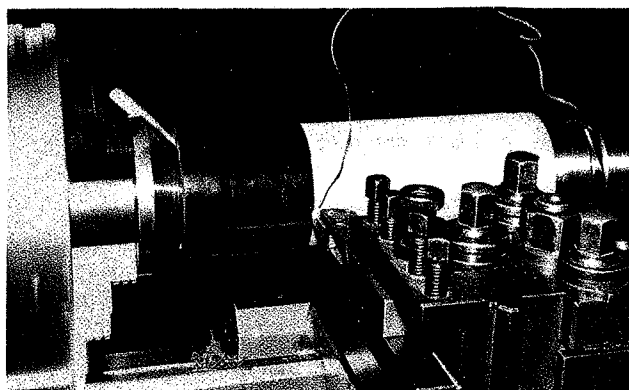
A bearing that is being made from the partial length of a tube can be chucked at one end in a normal 3 jaw chuck, the O.D. rough machined, the I.D. finish machined, the O.D. finish machined and then parted to length. Care must be taken not to over tighten the chuck and distort the tube.

Machining - I.D. - thin wall tube with soft jaw chuck:

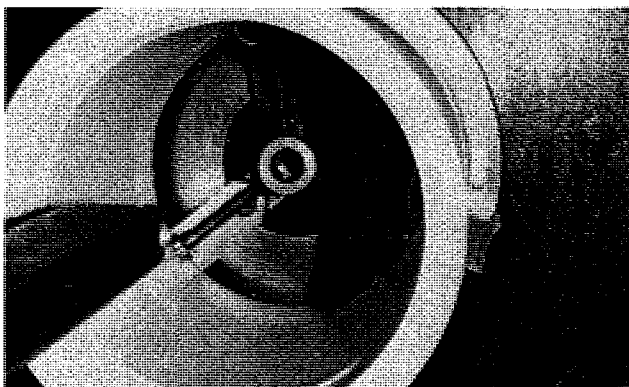
To machine the I.D. of a thin wall tube, the O.D. should be rough machined, the tube gripped in an extended soft jaw chuck and the I.D. finish machined. The extended chuck will grip and support the tube without deforming.

Machining - I.D. - thin wall tube with external sleeve:

A thin wall tube I.D. can also be machined by first machining the O.D. to size, lightly pressing the tube into a machined metal housing, chucking the housing and then machining the I.D. of the tube. It is possible to obtain tighter tolerances than those obtained with external soft jaws with this method but it is more involved and usually not necessary.

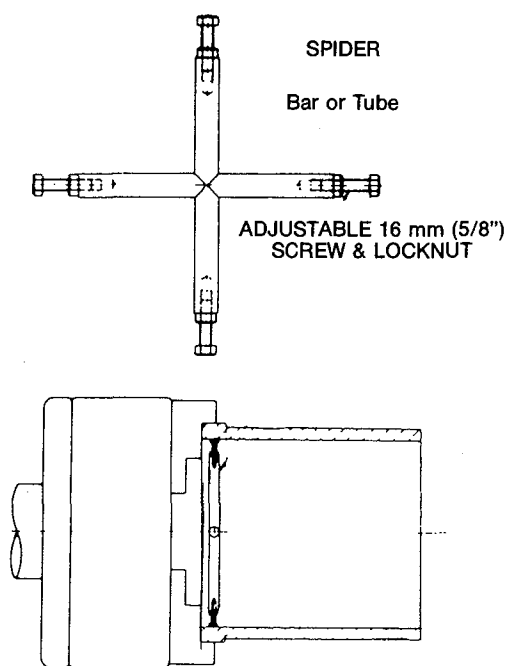
Machining - O.D. - full length of a lubrication grooved bearing - supported on centres:

After the I.D. of a bearing with lubrication grooves has been finish machined the bearing can be chucked on centres, driven by a key in one of the grooves and the O.D. finish machined.

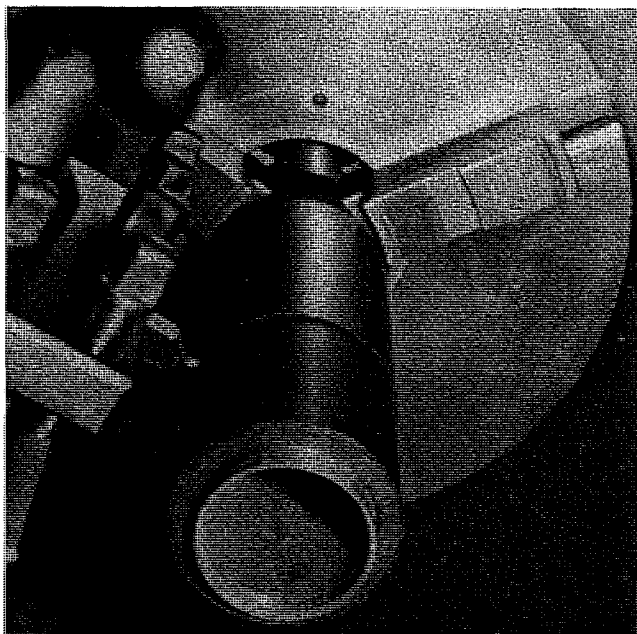
Machining - O.D. - machined steel plug or adjustable spider:

After the I.D. of a tube has been finish machined, a machined steel plug can be slip fit into the I.D. of the bearing. On larger tubes a 3 or 4 arm spider can be set to the inside diameter of the tube and located opposite the chuck jaws. Both of these devices eliminate distortion from chuck jaw pressure. A simply constructed 4 arm spider is illustrated on the following page. With either of these methods it is necessary to add a 50 mm (2.0") chucking allowance to the required length of the bearing.

Adjustable Spider

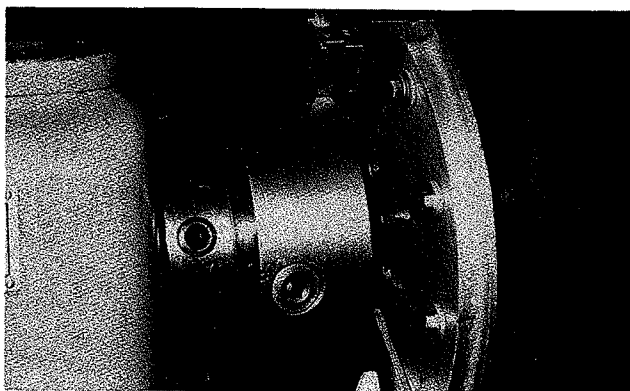


Machining - O.D. - stepped steel mandrel:



After the I.D. of the bearing has been finish machined, a stepped steel or Thordon mandrel machined to slip fit into the bearing and chucked in the jaws can be used to support the bearing for machining of the O.D. It is possible to obtain tighter tolerances with this method but it is more involved and usually not necessary.

Machining - O.D. and I.D. - tube mounted to a face plate



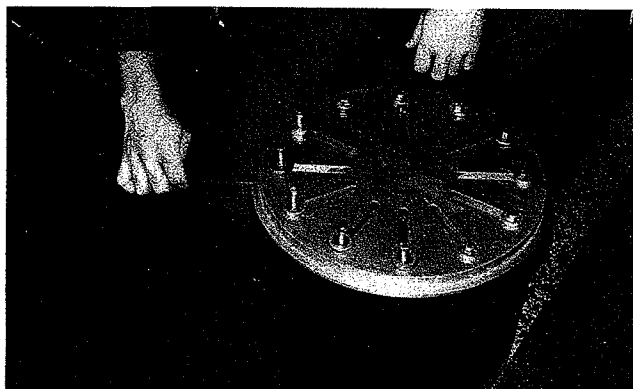
Bearings larger than 380mm (15.00") O.D. are most easily mounted for machining by lag screwing them to a face plate. The face plate can then be chucked in the lathe. An additional 50mm (2.0") must be added to the required length of the bearing as a chucking allowance.

The O.D. of the tube is rough machined first, then the I.D. finish machined, the O.D. finish machined and the bearing is then parted to length from the tube.

If the bearing is too large to safely catch as it is parted off from the tube, the following procedure should be used. Part the tube approximately 80-90% of the way through, remove face plate and tube from the lathe and knife cut the bearing from the tube.

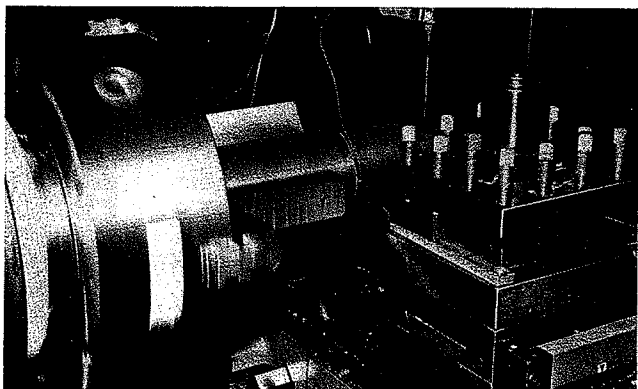
The bearing should be completely machined without stopping for extended periods of time. This prevents the bearing drooping or going out of round under its own weight.

NOTE: Ensure that the tube is securely mounted to the face plate before turning. Failure to mount the tube securely could result in the tube coming loose and causing personal injury.



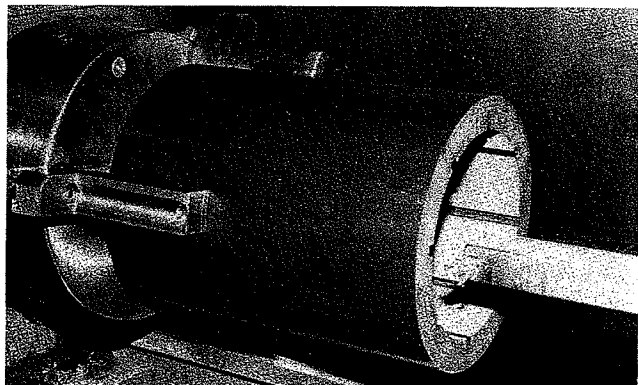
The face plate is centered as accurately as possible and then screwed to the tube. After mounting, the tube can be trued for machining, if required, by loosening the screws and adjusting the position of the tube using the slots in the face plate.

4:2:4 Parting to Length:



Thordon can be parted to length with a standard parting tool, however, additional rake and side clearance are helpful to prevent heat generation resulting from the Thordon contacting the side of the parting tool.

4:2:5 Machine lubrication Grooves:

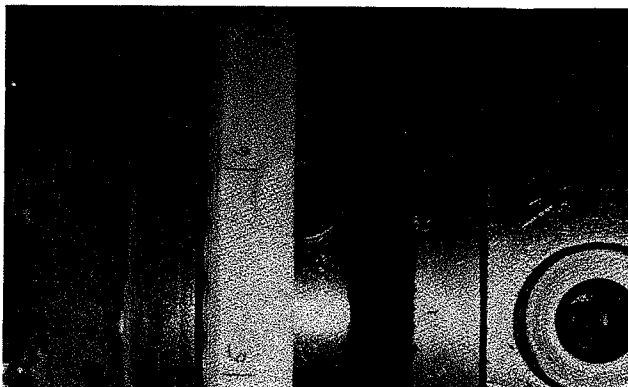


Lubrication grooves can be machined by hand or with a router.

To machine lubrication grooves by hand, a formed tool bit is mounted to the lathe boring bar and manually pushed through the bearing. Several passes may be required to achieve the final groove depth.



The grooves can be machined much more easily by mounting a router to the boring bar and then machining to the correct depth in one pass through the bearing.



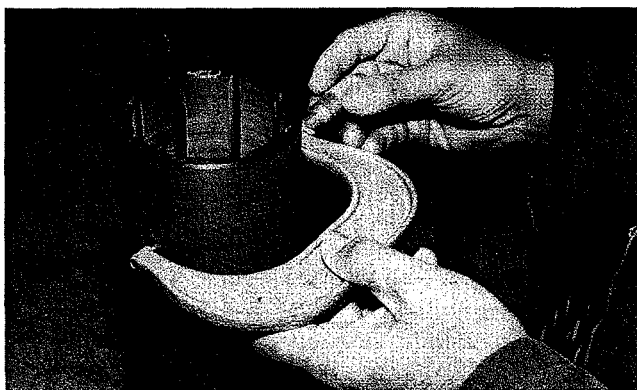
The outside diameter of the chuck can be divided and marked to act as a guide for locating the grooves in the bearing.

4:2:6 General Machining Tips:

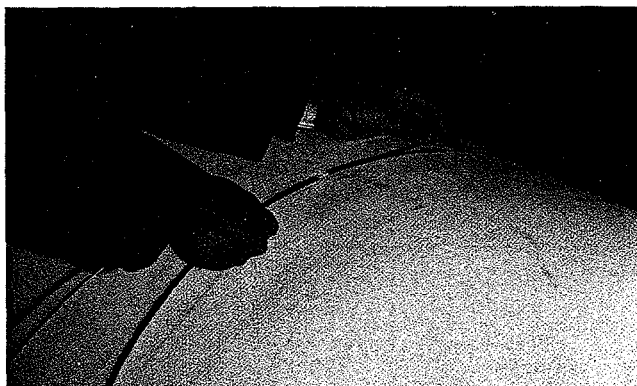
1. To obtain optimum dimensional and surface finish results the final machining cut should be 1.5 mm (0.060") to 2.5 mm (0.100") and the cutting tool razor sharp.
2. Machining must be performed in a controlled environment and with minimal heat build up. Changes in temperature can result in significant dimensional changes.
3. Due to the elastomeric nature of Thordon, if a machining error is made on the I.D. and if the wall thickness is still adequate, it may be possible to re-calculate the O.D. of the bearing and still use it. In other words, one can compensate for an I.D. machined too large by increasing the bearing interference.

4:3 DIMENSIONAL AND SURFACE FINISH MEASUREMENTS

4:3:1 Dimensional Measurements



In most cases Thordon can be measured using the same instruments and methods as any other material. It must be remembered that Thordon is an elastomer and a light touch must be used when measuring because it is possible to deform the bearing out of round. In addition, Thordon has a high coefficient of expansion compared to metals and measurements must be taken at machine shop temperature. If this is not possible then the dimensions must be corrected for the thermal expansion or contraction that has occurred because of the difference between the machine shop and ambient measuring temperatures.



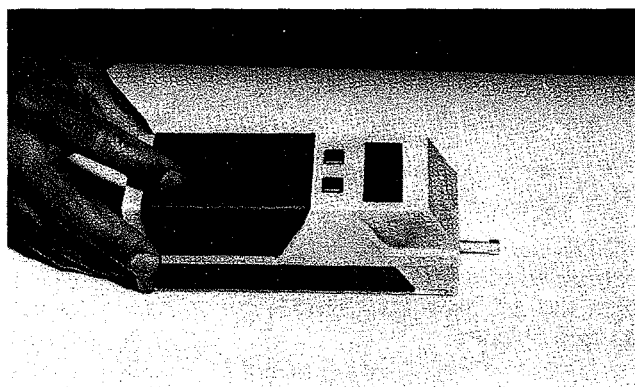
In the case of larger diameter, relatively thin wall bearings that have been machined and removed from the lathe, it is quite common to find that they go oval. This deformation can be the result of the bearing "sagging" under its own weight or from being secured to a pallet for shipping. The bearing may appear to be out of tolerance due to the fact that it has gone out of round. This is not a problem because when the bearing is pressed into a housing it will conform to the shape of the housing and will be round. To accurately measure the bearing outside the housing, use a pi tape to measure

the O.D. and then measure the wall thickness to obtain the correct I.D. dimension.

A pi tape is a precision steel tape calibrated to measure diameters by measuring circumference.

4:3:2 Surface Finish:

Thordon, due to its non-metallic elastomeric nature, cannot be machined to as smooth a surface finish as metals. This is not a problem because the bearing goes through a normal break in period during which the initial surface roughness is worn smooth. This process can be enhanced by using T-G 8, Thordon's bearing break in lubricant. It is important, however, to strive for as good a surface finish as possible to reduce friction and initial break in wear. The mechanics of obtaining a good surface finish have been covered in the machining section but it is important to know how to measure the surface finish of a Thordon bearing.



Due to the non-metallic nature of Thordon it will tend to "feel" smoother to the touch in comparison to metal than what it really is. To accurately measure Thordon surface finish a stylus type of surface finish gauge should be used. Practical experience has shown that the use of a comparator will usually result in a value that is less than the actual value. This is because Thordon is softer than metal and "feels" smoother than what it actually is when measured with a stylus.

4:3:3 Machining and Surface Finish Tolerances

Thordon is a non-metallic and consequently cannot be machined to the same tight tolerances as bronze or other rigid materials. Conversely tight "metallic" tolerances are not necessary to obtain optimum performance. The standard Thordon machining tolerances are as follows:

Bearings up to 380mm (15.00")

O.D. $-0.00\text{mm}, +0.13\text{mm}$ ($-0.000", +0.005"$)

I.D. $-0.00\text{mm}, +0.13\text{mm}$ ($-0.000", +0.005"$)

Bearings between 380 and 600mm (15.00" and 24.00")

O.D. $-0.00\text{mm}, +0.18\text{mm}$ ($-0.000", +0.007"$)

W.T. $+0.00\text{mm}, -0.13\text{mm}$ ($+0.000", -0.005"$)

Bearings over 600mm (24.00")

O.D. $-0.00\text{mm}, +0.25\text{mm}$ ($-0.000", +0.010"$)

W.T. $+0.00\text{mm}, -0.13\text{mm}$ ($+0.000", -0.005"$)

The tolerances on surface finish are as follows:

XL: 3.2 micro-metres (125 micro-inches)

SXL: 3.2 micro-metres (125 micro-inches)

Composite: 4.2 micro-metres (175 micro-inches)

NOTE: Due to the unique characteristics of Thordon, compared to metals, optimal performance can still be obtained at relatively high (compared to metal) surface finishes.

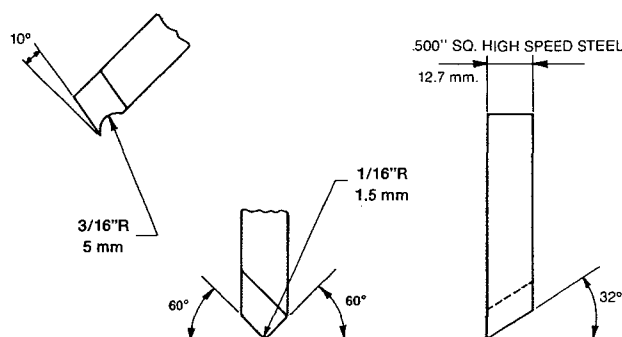
4:4 MACHINING COMPOSITE

Machining Thordon Composite is different than machining Thordon XL or SXL because of the softer Composite material that is used. The O.D., because it is regular Thordon, can be machined using the same techniques as outlined in section (b) Machining XL and SXL. The I.D., however, machines differently and that is what will be covered in this section.

4:4:1 Cutting Tool

The cutting tool for machining Composite should be made to the configuration illustrated below. As with other types of Thordon it is essential that the cutting tool is kept sharp. Even with the correct cutting tool, it is necessary to grind the inside diameter on the final cut to obtain an acceptable surface finish. This operation will be explained in detail in the grinding information section following.

High Speed Steel Cutting Tool



4:4:2 Machining Feeds and Speeds

Normal turning speeds for Composite bearings of various diameters are given in the chart below.

BEARING DIAMETER		
METRIC	IMPERIAL	RPM
150mm	6.0"	250
300mm	12.0"	100
450mm	18.0"	75
600mm	24.0"	60
750mm	30.0"	50
900mm	36.0"	40

Normal cutting feed rates are as follows:

METRIC — 0.40 mm to 0.50mm/Rev.

IMPERIAL — 0.015" to 0.020"/Rev.

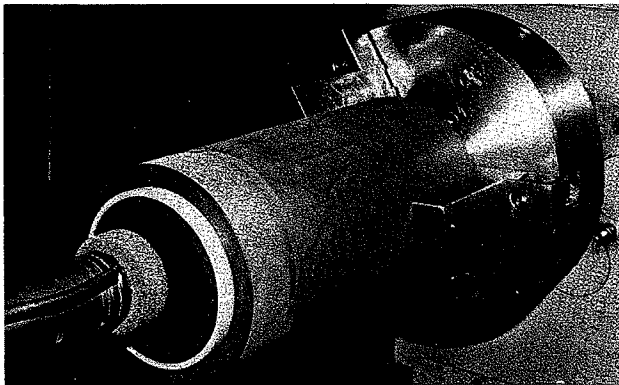
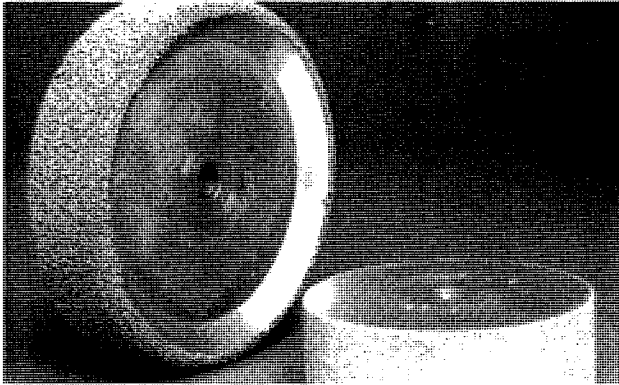
NOTE 1: The turning, feed and grinding speeds are provided as a guide only. The optimum speed may vary higher or lower depending on such variables as the length of tube, the wall thickness and how the bearing is being supported. As is common with all machining operations, some experimentation is required to obtain optimum results.

NOTE 2: Cutting lubricants are not required and are not recommended.

4:4:3 Machining Procedure (O.D. up to 250mm (10.0"))

The procedure for machining Thordon Composite bearings up to 250mm (10.0") O.D. can be summarized in the following steps.

- a) Part the bearing oversize and face to the required finished length.
- b) Mount the bearing on centres and rough machine the O.D.
- c) Press the bearing (light press fit) into a housing to support it and machine the I.D. to within 0.25 to 0.40mm (0.010" to 0.015") of the finished dimension. To achieve a satisfactory surface finish it is necessary to grind the Composite lining to its finished dimension using a fine coated tungsten carbide grinding hog (shown below).



- d) Grind the I.D. to the required dimension. The grinding pass should only be 0.25 to 0.40mm (0.010" to 0.015") deep and at a feed rate of 0.50 to 0.60mm/Rev. (0.020" to 0.025"/Rev.)

48081-E

The turning speeds when **grinding** composite based on the above are:

BEARING DIAMETER		
METRIC	IMPERIAL	RPM
150mm	6.0"	55
300mm	12.0"	50
450mm	18.0"	40
600mm	24.0"	30
750mm	30.0"	25
900mm	36.0"	20

The grinding hog should be operated with a peripheral speed between 12.5 - 15.5m/sec. (2500 - 3000 fpm) and the bearing rotated in the opposite direction to the grinding hog.

- e) Lightly press the bearing onto a mandrel and finish machine the O.D.

4:4:4 Machining Procedure (O.D. larger than 250mm (10.0"))

Composite bearings larger than 250mm (10.0") are best machined by mounting them to a face plate and then machining and grinding the I.D., machining the O.D., parting oversize and facing to length.

NOTE: Ensure that the bearing is securely mounted to the face plate before turning. Failure to mount the bearing securely could result in the bearing coming loose and causing personal injury.

4:4:5 Finish Machining a Composite Bearing without Grinding

Finish machining the I.D. of a Composite bearing by grinding is the recommended method, however it is possible to finish machine using a conventional tool bit and achieve acceptable results. The procedure that must be used is the following:

- a) Rough machine the I.D. of the bearing so that the finish machining operation can be done in two EQUAL passes approximately 2.0 to 3.0mm. (0.080" to 0.120") deep.
- b) Two equal machining passes are required because the Thordon Composite bearing lining material wears tool bits very quickly. In the course of one machining pass through the I.D. of a typical bearing tool bit wear can result in a taper of 0.15 mm. (0.006") from one end of the bearing to the other. The first pass is used to predict what the amount of taper is going to be. The second pass is then used to correct for the expected taper based on the first pass.
- c) To make the required correction a dial indicator is set up on the lathe tool post and the tool post marked in 25 mm. (1") increments. If the amount of taper is equal to 0.15mm. (0.006") over the length of a 300mm. (12.0") bearing then a correction of 0.013mm (0.0005") per 25mm. (1.0") of bore length is required. The correction on the dial indicator will be half of this amount which is 0.0065 (0.00025") per 25mm. (1.0") of bore length.
- d) The correction is made while machining by tapping the tool post over an amount equal to 0.013mm. (0.0005") at 25mm. (1.0") increments along the bore as the final machining pass is being made. It is important to note that the final pass must be at the same depth, speed and feed rate as the preceding pass. Otherwise the amount of taper may increase or decrease and the correction that is being made will not be correct.
- e) The burr that is left on the lubrication grooves must be removed using emery cloth. Although the surface finish of the bearing will be somewhat rough it will bed in quickly and perform well.

CHAPTER 5

MATING SURFACES -HOUSINGS

5:1 Mating Surfaces - Hardness

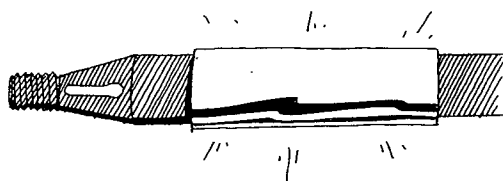
5:1:1 Bronze

Bronze is probably the most commonly used shaft liner material in marine service. It resists sea water corrosion, is easily machined, commonly available, and can be shrunk onto shafts without major problems. The only bronze we have encountered that has given adverse service has been nickel aluminum bronze. We suspect that the aluminum content is etched out by electrolytic action of sea water corrosion, producing sharp grain boundaries that have in turn been abrasive to bearings. Poor quality porous bronze castings should be avoided for similar reasons.

There is a vast range of materials commonly called bronze. Two specific types which have given good service with Thordon, and that are fully approved by Lloyds, are Gunmetal (88% Cu, 10% Sn, 2% Zn) and "70-30 Copper Nickel". Both are relatively hard.

In general bronze is not a highly wear resistant material. If abrasive content exists, regardless of the bearing material, bronze will be worn away more quickly than harder materials. It is generally true that the harder the shaft liner material, the longer its life will be against almost any bearing. Considering bearing materials in general, it is also true that harder bearing materials will tend to create more liner wear than softer materials, simply because the hard material presses the abrasive particles against the liner surface with more force than a softer material. This is one reason why we choose Composite bearings that have a special softer interior, when dealing with abrasive field conditions.

In conjunction with Thordon, bronze liners are acceptable for propeller shaft service as long as the vessel is not operating continually in abrasive conditions. In abrasive water, a harder liner material should be used.



For rudder applications bronze seems to be an acceptable liner material. Lower pintle bearing positions for vessels operating under dirty conditions should be equipped with a harder liner if wear has been experienced in this position.

5:1:2 Carbon Steel

Carbon steel shafts are relatively inexpensive in smaller sizes and as long as the corrosion problem is not too bad, (ie. fresh water service) these shafts can be fitted without liners. If, however, the vessel experiences a lay-over during which corrosion occurs on the shaft in way of the bearing a high bearing wear rate may occur upon start-up. This high wear is a result of the rough, corroded shaft surface effectively "machining" the Thordon bearing.

5:1:3 Hard Metal Sleeves

Sleeves manufactured from hard, corrosion and abrasion resistant steels are particularly common on tug or push boats operating in river systems. These operating conditions are usually very abrasive and a hard liner material is necessary for long life operation. There are many alloys available. Cost and availability play a role in selection. Some hard sleeves use a carbide coating such as boron carbide or tungsten carbide. They typically have hardnesses in the range of 50-60 Rockwell C. A flame sprayed coating of nickel, chrome or boron alloy over a stainless steel substrate provides consistently good wear performance in abrasive water conditions with Thordon Composite bearings.

5:1:4 Inconel 625

The U.S. Navy, and several other navies have experienced excellent results with submerged arc welded Inconel 625 alloy coatings. This alloy is a high nickel (60%) content, corrosion resistant, alloy that can be applied by cladding or in the form of a tubular liner or sleeve.

Note: Some classification societies will not permit welded liners, but many Naval authorities do.

5:1:5 Stainless Steel

Stainless steel is not a particularly wear resistant material, this is particularly true of its easily machinable alloys. A liner should offer both good corrosion and abrasion resistance. This combination is often difficult to achieve; the most corrosion resistant alloys often offer poor abrasion resistance. We have had occasional reports of stainless steel shafts exhibiting substantial wear when running against a Thordon bearing. It is probable that the vessels were operating in abrasive water conditions. Some types of stainless steel shafting are good under abrasive conditions. Alloys with hardness higher than 30 Rockwell C would be the most appropriate. In very abrasive conditions, however, a separate hard liner should be fitted. (see 5:1:3)

A peculiar form of corrosion can take place on stainless steel if the surface is totally deprived of oxygen. This can happen with a soft rubber bearing on a vessel that is left idle for sometime. The shaft will exhibit signs of substantial corrosion in areas masked by adhesion to the rubber. We have not experienced this problem with Thordon. The greater stiffness of Thordon does not allow the same degree of contact and will permit a film of water to cover practically the entire shaft or liner surface.

5:2 Mating Surfaces - Finish

Thordon functions better with a highly polished mating surface. Badly corroded or scored shafts or liners should be avoided. The recommended surface finish is 16-32 micro-inch RMS, maximum.

5:3 Housing - Roundness

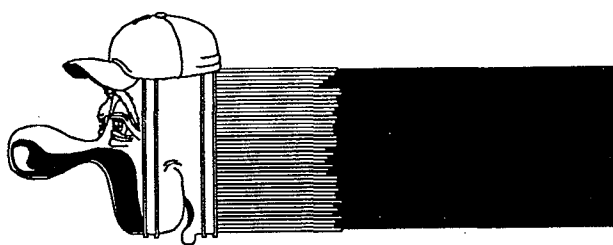
Thordon is a flexible material and will adapt to the shape of the housing into which it is pressed. For this reason, out-of-round housings must be avoided unless special fitting methods are used. For out-of-round housings, there are three alternatives. First, the bearing can be pressed into the housing and then bored to ensure it is round. (Boring of the housing instead should be considered as a more permanent solution.) Second, the bearing can be bonded into place using TG-75 adhesive, or an epoxy resin such as Chockfast. Thirdly, the housing can be repaired locally, by applying epoxy and grinding.

5:4 Corrosion Protection

Thordon, a non-metallic, avoids the type of electrolytic corrosion normally found between a metallic bearing and the housing. For this reason, Thordon is especially well suited to use in aluminum boats. Further housing corrosion protection can be achieved by painting the interior of the housing with a corrosion resistant epoxy paint prior to the installation of the Thordon bearing. Thordon, with its interference fit, usually presses against a new housing tightly enough to avoid penetration of corrosive water between the bearing O.D. and the housing.

Propeller shafts which are subject to corrosion in sea water must be protected between the liners by a corrosion resistant coating. The most common coatings used are vulcanized rubber and epoxy fiberglass. Both have disadvantages, and consequently the shaft survey interval for open systems is a maximum of only 4 years.

Thordon Bearings is developing a shaft coating system with the goal of extending this survey interval to 5-10 years. This shaft coating system is based on a sprayed elastomer and is expected to be available for evaluation in late 1995 or 1996.



CHAPTER 6

INSTALLATION METHODS

6:1 General

Thordon bearings are generally fitted with an interference fit. Actual installation is very quick and easy, especially when freeze fitting is used. The housing should always be clean and dry. No grease or oil should be used to help press or drive fitting as this will have a negative effect on the interference. The housing should be round and not tapered or bell mouthed. It should provide support to the Thordon bearing along its full length. Thordon will not function well when not fully supported. Gaps in the housing should be filled in or a sleeve fitted before installing the Thordon bearing. The relative light weight of Thordon is a significant advantage in the installation of large bearings. Large tubular bearings can be handled and freeze fitted manually or with light lifting equipment. The interference fit is sufficient to prevent bearing rotation under normal conditions, so anti rotation keying is usually not necessary. A forward stop and an end keeper ring are required to avoid any possibility of axial movement. These keeper rings must be of adequate proportion and have an inside diameter equal to the maximum bearing/liner wear down plus 10%. The removable keeper ring should be retained with bolts rather than welded.

As an alternative to interference fitting, it is possible to bond Thordon bearings into housings.

6:2 FREEZE FITTING

6:2:1 General

Because of Thordon's relatively high coefficient of thermal expansion, it contracts significantly when cooled. This makes shrink fitting the easiest way to install Thordon bearings. Dry ice is the usual cooling agent used but liquid nitrogen is the optimum cooling agent if available. When using dry ice it should be in pelleted form, or if supplied in block form, it must be broken into smaller pieces. The dry ice must make good contact with both the inside and outside surface of the bearing. The bearing should remain in the dry ice for a minimum of 3 hours and can then be checked to see if it has shrunk sufficiently for installation. If not, it should be re-packed and checked in another hour. Liquid nitrogen should only be used in a tight container where the liquid cannot leak out and cause harm. The bearing should be completely immersed or evenly coated with liquid nitrogen. When the liquid nitrogen stops boiling, the bearing has reached a temperature of -196° C (-320° F) and can be easily installed. The amount of shrinkage that can be expected can be estimated as follows:

Each 10° C decrease in temperature will result in an approximate decrease in diameter of 0.0014 mm/mm of diameter.

Each 10° F decrease in temperature will result in an approximate decrease in diameter of 0.0008 inches/inch of diameter.

CAUTION

Use of liquid nitrogen in closed or poorly ventilated areas should be avoided as the boiled off gasses tend to displace air. Similar precautions should be observed with significant quantities of dry ice.

6:2:2 Tubular Bearings

Thordon tubular bearings, when frozen, can normally be slid into the housing without difficulty. If some resistance is encountered, however, a hammer or jack can be used to finish the job.

For all tubular bearings, we recommend a machined stop or ring at an appropriate point to prevent the bearing from moving too far when being installed. We also recommend a keeper ring at the other end to eliminate any possibility of axial movement. The designed interference fit is usually sufficient to hold bearings in place, but the end stop or keeper is added insurance, especially for large bearings. A tapered housing, or cyclical unbalanced loading may occasionally cause a large bearing to move axially if it is not secured.

Most tubular Thordon bearings are supplied in more than one length. This is done to make handling and machining easier. The first section is fitted, and pushed home against the forward stop. Then subsequent sections are fitted. For large bearings with more than two sections, each section should be allowed to warm up and lock itself in place before the next section is fitted. Alternately, a small space can be left between sections to permit axial expansion during warming up.

Grooves of propeller bearings should be aligned to avoid restriction of the water flow. This can be done visually, or a piece of flat bar stock can be fitted so that it engages the grooves on adjoining sections. To avoid possible constriction problems from minor misalignment of water grooves, each section of a Thordon tubular bearing should be machined with a circular recess at one end (the same width and depth as the water grooves -see page 48). This facilitates flow of water from one set of grooves to another even if there is misalignment. Care must be taken to ensure that these recessed ends are properly installed -in the middle, not on the outside.

6:2:3 Stave Bearings

Care should be taken to ensure that all staves are cooled by alternating layers of staves and dry ice. The staves should be placed in dry ice with at least a 25mm (1") covering over the staves. They should be left in dry ice for approximately 2-3 hours. A cylinder of liquid nitrogen large enough to immerse the staves can also be used. The staves should be immersed until bubbling of the nitrogen stops.

Frozen staves are placed side by side in the housing until all staves are assembled. The machined staves should be placed next to the keeper strips. It is sometimes necessary to drive the last stave into the housing if the assembly has begun to warm up during installation. While frozen, Thordon staves, especially composite staves, may twist or warp a little, but this should not unduly affect the assembly. Any staves that come loose should be hammered back into place. While it is warming up, the assembly should be checked to ensure that all staves are tightly seated against the housing.

When staves of different length are used, an interlocking pattern is recommended -long-short and then short-long. Care should be taken to ensure that the long and short staves are matched together against the keeper strips.

When fitting staves on the upper half of the assembly they may be kept in place by using hoops, wooden discs, or other devices. Once the staves begin to warm up, no special support will be required. Once the staves are fully warmed up, they will be tightly held in place by their interference fit.

With stave bearings a forward stop and an end keeper ring should be used to eliminate any possibility of axial movement of the staves under unusual operating conditions.

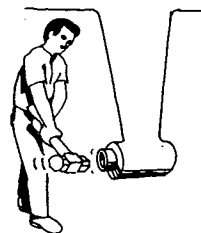
6:3 PRESS OR DRIVE FITTING

6:3:1 Cylindrical Bearings

Although freeze fitting is the preferred way to install Thordon bearings, it is also possible to use a drive or press fit when freezing facilities are not available. Driving is possible for small bearings. Hammer impact will not harm the bearings. Because of the significant amount of interference on Thordon bearings, considerable pressing force is required to install larger bearings. All press or drive fit bearings should be machined with an entry chamfer to facilitate starting them into the housing. For multiple piece bearings, a piece of flat steel bar should be fitted into adjoining grooves to ensure proper groove alignment. To avoid possible constriction problems from minor misalignment of water grooves, each section of a Thordon tubular bearing should be machined with a circular recess at one end (the same width and depth as the water grooves -see page 45). This facilitates flow of water from one set of grooves to another even if there is minor misalignment. Care must be taken to ensure that these recessed ends are properly installed -in the middle, not on the outside (see page 43-44). Pressing force required to fit a Thordon bearing can be calculated as follows:

$$F(\text{lbs.}) = \frac{\text{Interference}(\text{in}) \times \text{wall thickness}(\text{in}) \times 3 \times 100000}{\text{Housing bore}(\text{in})}$$

$$F(\text{kg.}) = \frac{\text{Interference}(\text{mm.}) \times \text{wall thickness}(\text{mm.}) \times 211}{\text{Housing bore}(\text{mm})}$$



6:4 ALTERNATIVE METHODS —BONDING

Bonding of Thordon bearings into a housing is an alternative method to interference fitting. Reasons for using bonding include:

- a) to compensate for an irregular or out-of round housing
- b) to fill recesses in a housing that would not otherwise provide adequate bearing support.
- c) when the bearing wall is too thin for an interference fit (less than recommended wall/diameter)
- d) in new construction to avoid finish machining of struts or housings.

We recommend bonding be done using Thordon's TG-75 two part epoxy type adhesive. If there are gaps between the bearing and the housing greater than 3.0mm. (0.125") a chocking compound such as Chockfast may be used.

6:4:1 Dimensioning For Bonding

A bonded fit normally involves no interference, so the bearing OD will be the Housing ID less an allowance for bond thickness, normally 0.13 - 0.38mm. (.005 - .015"). The bearing ID can be calculated as indicated in Chapter 3 except that the allowance for bore closure should be eliminated.

Thordon bearings, especially large, thin walled rudder bearings are sometimes fitted with a combination of interference and bonding. In this case the standard dimension calculations from Chapter 3 should be used.

6:4:2 TG-75

TG-75 is a flexible, high strength, two-part epoxy based adhesive that has replaced TG-4. It is used primarily to form strong bonds between cured elastomers and metals. It can fill gaps up to 3mm. (0.125"). Use of alternative adhesives should be avoided.

To bond a Thordon bearing you must:

A) Measure the housing ID (multiple readings) and machine the bearing OD to 0.25mm. (0.010") less than the smallest housing diameter reading. Maximum gap should not exceed 3mm. (.125").

B) Machine ID to appropriate dimension as indicated in 6:4:1.

C) Clean housing with Acetone, M.E.K. or any other solvent that does not leave an oily residue. Avoid solvents such as Varsol Mineral Spirits or Paint Thinners that leave an oily film that impedes bonding. Alternately use a clean new wire wheel and wipe with a clean cloth.

D) Remove any oil or grease from the machined bearing O.D.

E) Apply TG-75 as outlined in the TG-75 instruction booklet supplied with the product.

F) Apply TG-75 in the following sequence, assuming the bearings comprise more than one section in a single bore. The purpose of such sequence is to ensure the adhesive has the best chance to remain where it is needed, and to keep it from squeezing into the space between the sections where it could block either an annular groove or flushing grooves.

(1) The first section to be installed should be lightly coated with TG-75 while a heavier coat is applied to that portion of the bore where it will be positioned. (The use of plastic spreaders sold for applying auto body filler makes the job less messy.) The total amount of adhesive applied should depend on the voids to be filled. If these are small, then less adhesive should be applied, as the excess will be displaced and may tend to block the water ports, etc.

(2) Slide the first section into position, ensuring it has travelled fully to its forward limit. Don't panic, you have lots of working time to make sure everything's properly positioned.

- (3) Apply a light coat of TG-75 to the rest of the housing bore and a heavier coat to the OD of the next bearing section.
 - (4) Insert the second section into position making sure that the water grooves (if any) are aligned.
 - (5) Repeat for the third section, if applicable.
- G) Remove any TG-75 from the bearing bore or grooves immediately. Acetone works well for clean-up. Do not contaminate the bond line with solvent.
- H) Allow 8 hours after mixing at room temperature before fitting shafts and propellers or mounting the rudder.
- I) We recommend waiting 16 hours before turning the shafts, and 48 hours before any full speed trials are planned.

6:4:3 Filling Recesses

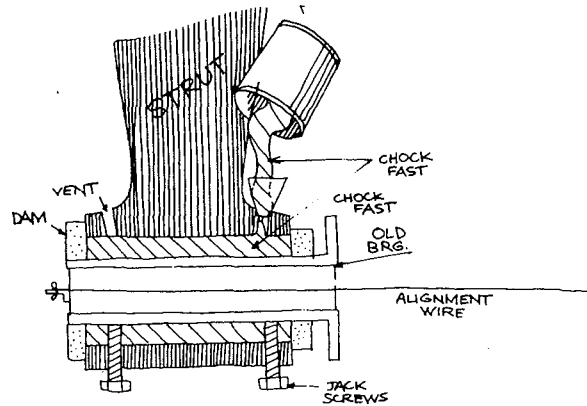
Thordon bearings must be supported along their full length if they are to perform effectively. Unsupported areas deflect with shaft pressure and can carry only a fraction of their normal pressure. This reduces the "effective length" of the bearing. To overcome this problem Thordon can, sometimes, be fitted into the bored out bronze jacket of an old rubber/metal rubber bearing. Alternately, the annular spaces can be filled with Chockfast, or another suitable epoxy compound.

6:5 Chockfast Fitting

This proprietary product made by Philadelphia Resins Inc. is a two component epoxy base material. The PR-610 (Chockfast Orange) is recommended by the manufacturer for bearing fitting. Many shipyards are familiar with Chockfast and like to use it. It can fill substantial gaps with minimal shrinkage. Potlife and viscosity are such that it can be poured into the annular space between a bearing and its housing without difficulty as long as proper venting provisions are allowed.

In the curing process Chockfast produces an exothermic heat. When the wall of the Chockfast is thick, this heat may be sufficient to damage the Thordon bearing. The manufacturer advises that wall thicknesses of 12mm.(0.5") will not generate sufficient heat to damage a Thordon bearing. For thicker cross sections of Chockfast see the special procedures outlined in section 6:5:2 or contact Thordon Bearings for further information.

Essentially there are two installation methods using Chockfast, one using chockfast as an adhesive to bond the bearings in place, and the other using Chockfast to form a housing into which a bearing can be interference fitted. The use of Chockfast is popular in new construction as an alternative to boring and aligning struts, and in repair when badly worn housings are encountered.



6:5:1) Bonding directly into the housing using Chockfast

- 1(a)** Ensure that the OD of the bearing is roughened, either by machining or grinding.
- 1(b)** When fitting multiple piece bearings, butt together the sections, with the circular groove at the join. Wrap the seam on the OD with duct tape to prevent Chockfast from entering the bearing.
- 1(c)** Install shaft
- 1(d)** Fit bearing(s) over shaft in correct position.
- 1(e)** Jack shaft up until it is positioned above the point of theoretical alignment by an amount equal to the total bearing clearance.
- 1(f)** A light wooden wedge at the bottom of the bearing in the clearance space will prevent motion during pouring.
- 1(g)** Prepare assembly for Chockfasting with appropriate dams, vent holes, etc. according to standard Chockfast instructions. Maximum recommended thickness for Chockfast orange is 1", but due to possible damaging exotherm, we recommend a 12mm. (0.5") max gap.
- 1(h)** Pour Chockfast observing set up times.

6:5:2 Chockfast with Dummy Bearing to create a housing into which a Thordon bearing can be interference fitted.

- 2(a)** A Dummy bearing (metal tube, used rubber/metal bearing with good OD, etc.) is used as a core pattern. The OD of the core should be smaller than the OD of the finished Thordon bearing to be fitted by the amount of interference on the Thordon bearing.
- 2(b)** Coat the OD of the core with a release agent so that the Chockfast will not adhere to it.
- 2(c)** Place core in housing in the appropriate position where the bearing is to be fitted.
- 2(d)** Align core with or without shaft in place.
- 2(e)** Prepare assembly for Chockfasting with appropriate dams, vent holes, etc.
- 2(f)** Pour Chockfast using standard Chockfast procedures.

2(g) When Chockfast has cured, jack out the dummy core leaving a round, aligned Chockfast housing.

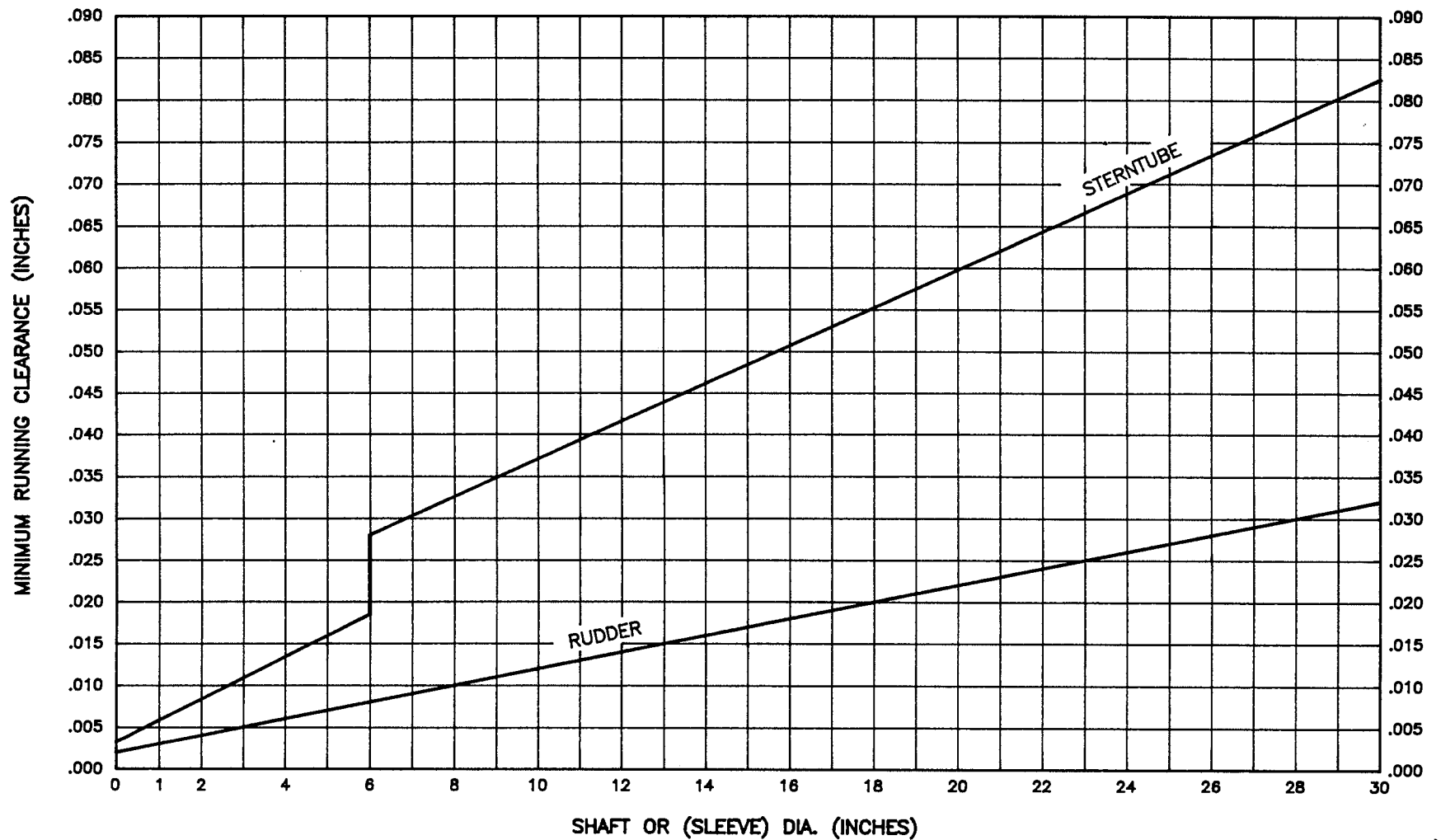
2(h) Press or shrink fit the Thordon bearing following guidelines for interference fitting.

This procedure can be used for thicker cross sections of Chockfast because the Thordon is not exposed to the Chockfast while it is curing.

6:5:3 Chockfasting stern tubes or bearing carriers

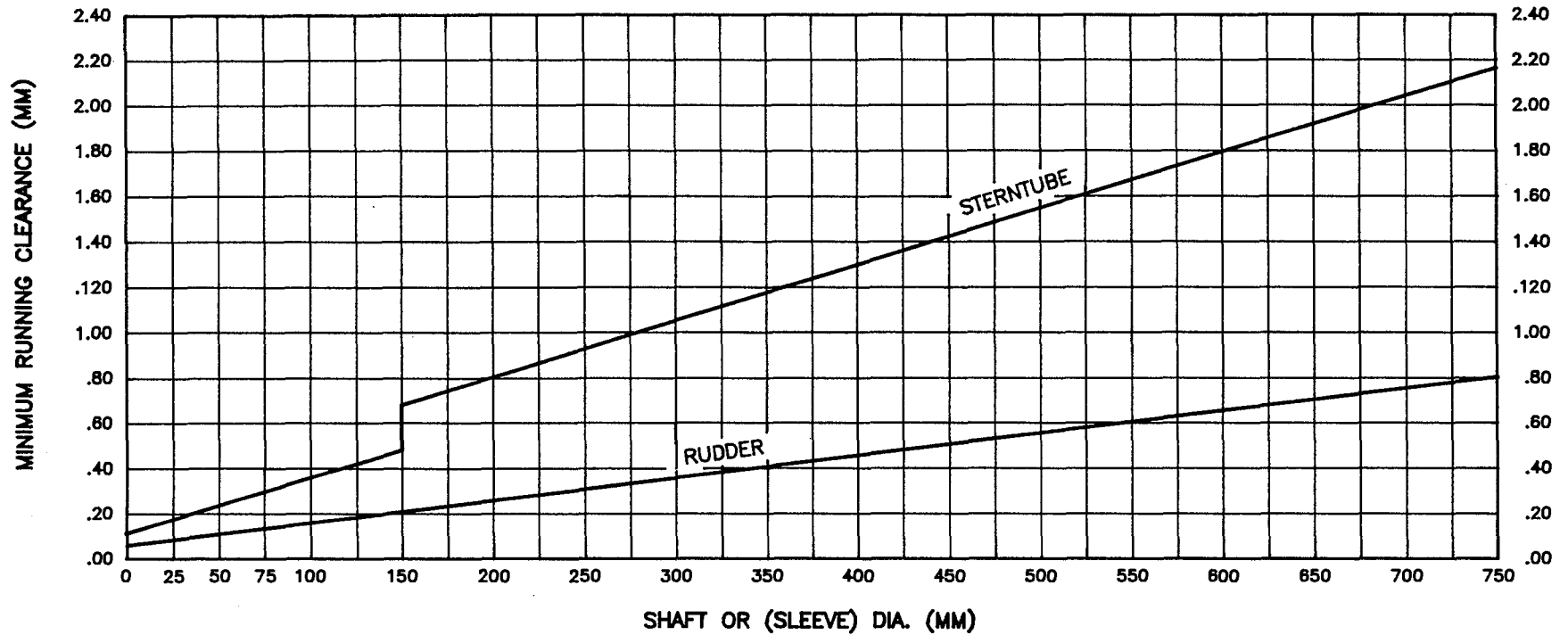
Some shipyards like to fit Thordon bearings into carriers or stern tubes, and then Chockfast the carrier or stern tube into position. This procedure is acceptable as long as a relatively thin cross section of Chockfast is used. We would not recommend more than 12mm.(0.5"). The exothermic reaction from thicker cross sections can heat transfer sufficient heat through the carrier or stern tube to stress relieve the Thordon bearing causing it to lose its interference fit. This procedure should not be used with SXL or Compac because of its lower stress relieving point.

MINIMUM RUNNING CLEARANCE FOR THORDON MARINE BEARING RELATED TO SHAFT DIAMETER IMPERIAL



NOTE: When applicable, additional allowances must be made for water absorption and thermal expansion. Refer to steps 3 and 4 in Inside Diameter Calculations.

MINIMUM RUNNING CLEARANCE FOR THORDON MARINE BEARING RELATED TO SHAFT DIAMETER METRIC

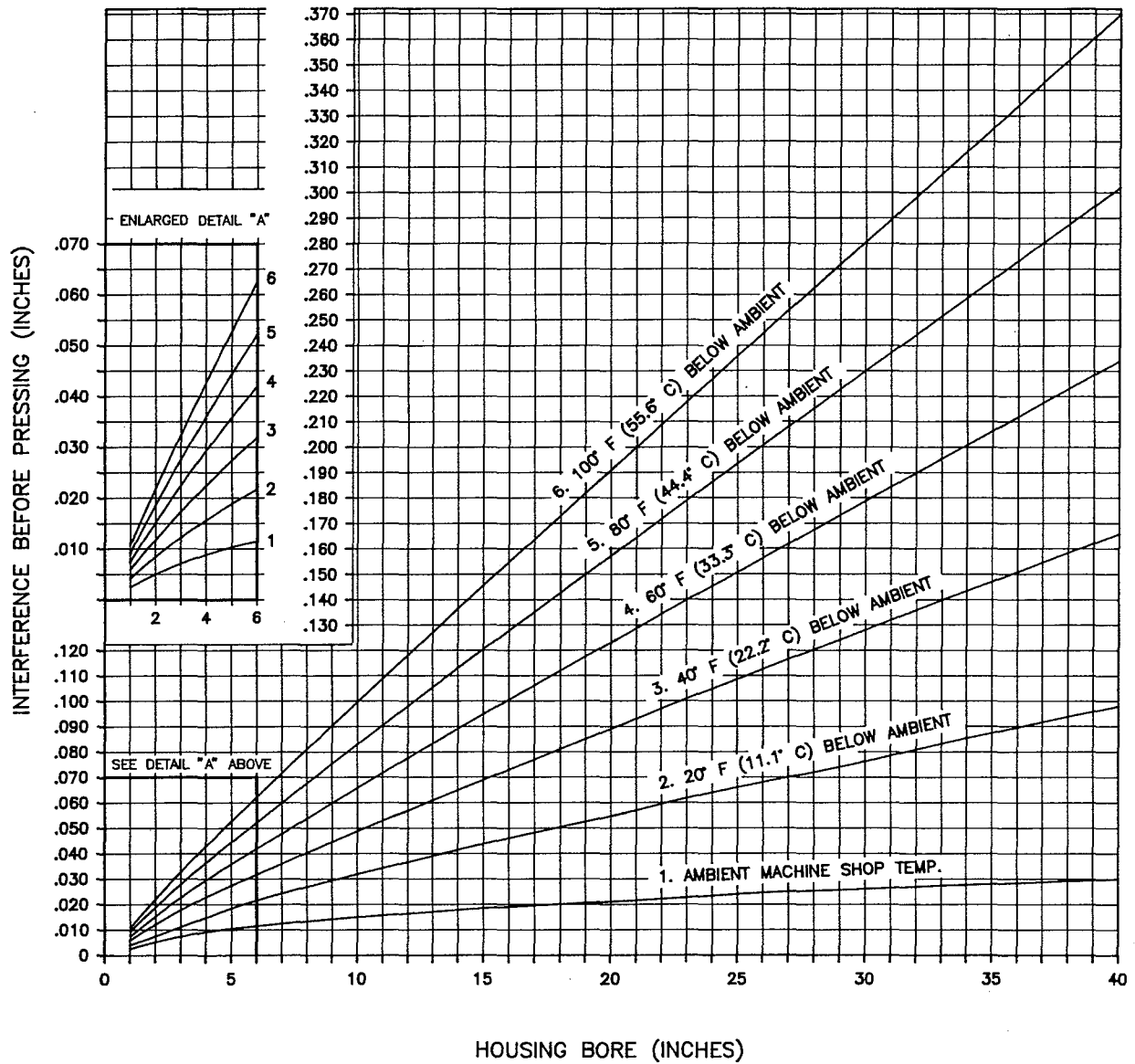


NOTE: When applicable, additional allowances must be made for water absorption and thermal expansion. Refer to steps 3 and 4 in Inside Diameter Calculations.

THORDON ELASTOMERIC PRODUCTS

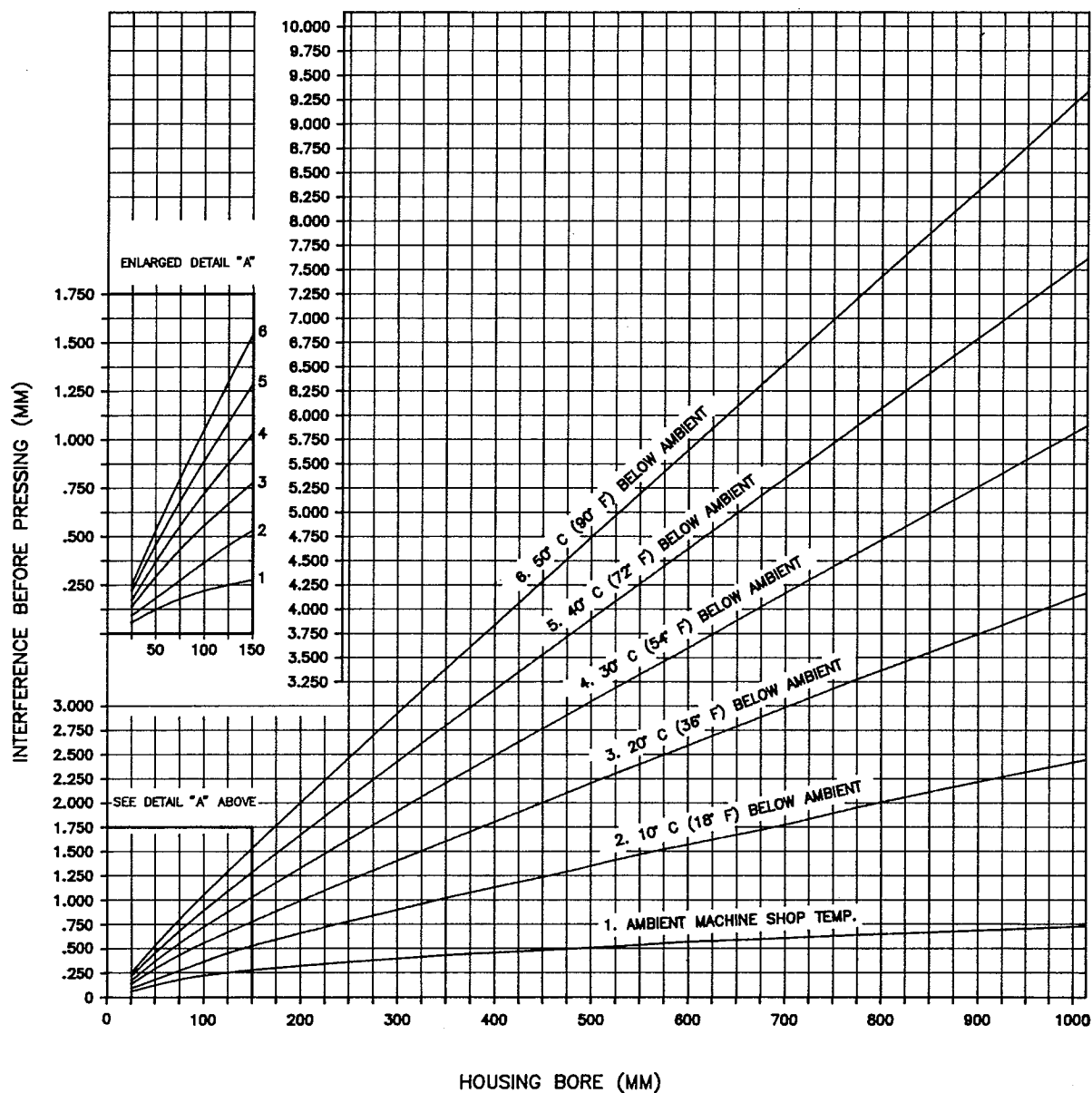
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HOUSING INTERFERENCE GRADE XL IMPERIAL UNITS



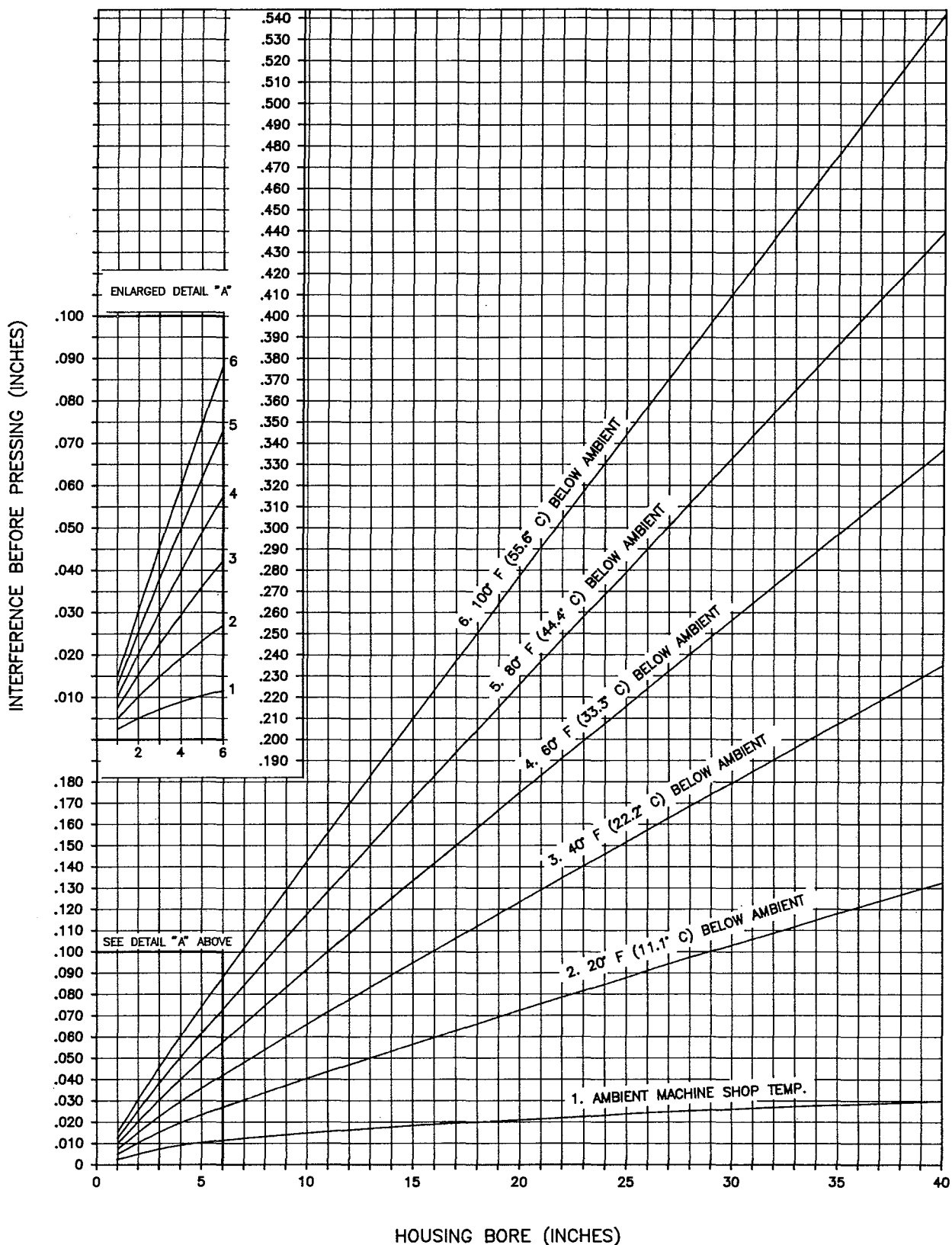
THORDON ELASTOMERIC PRODUCTS

HOUSING INTERFERENCE
GRADE XL METRIC UNITS



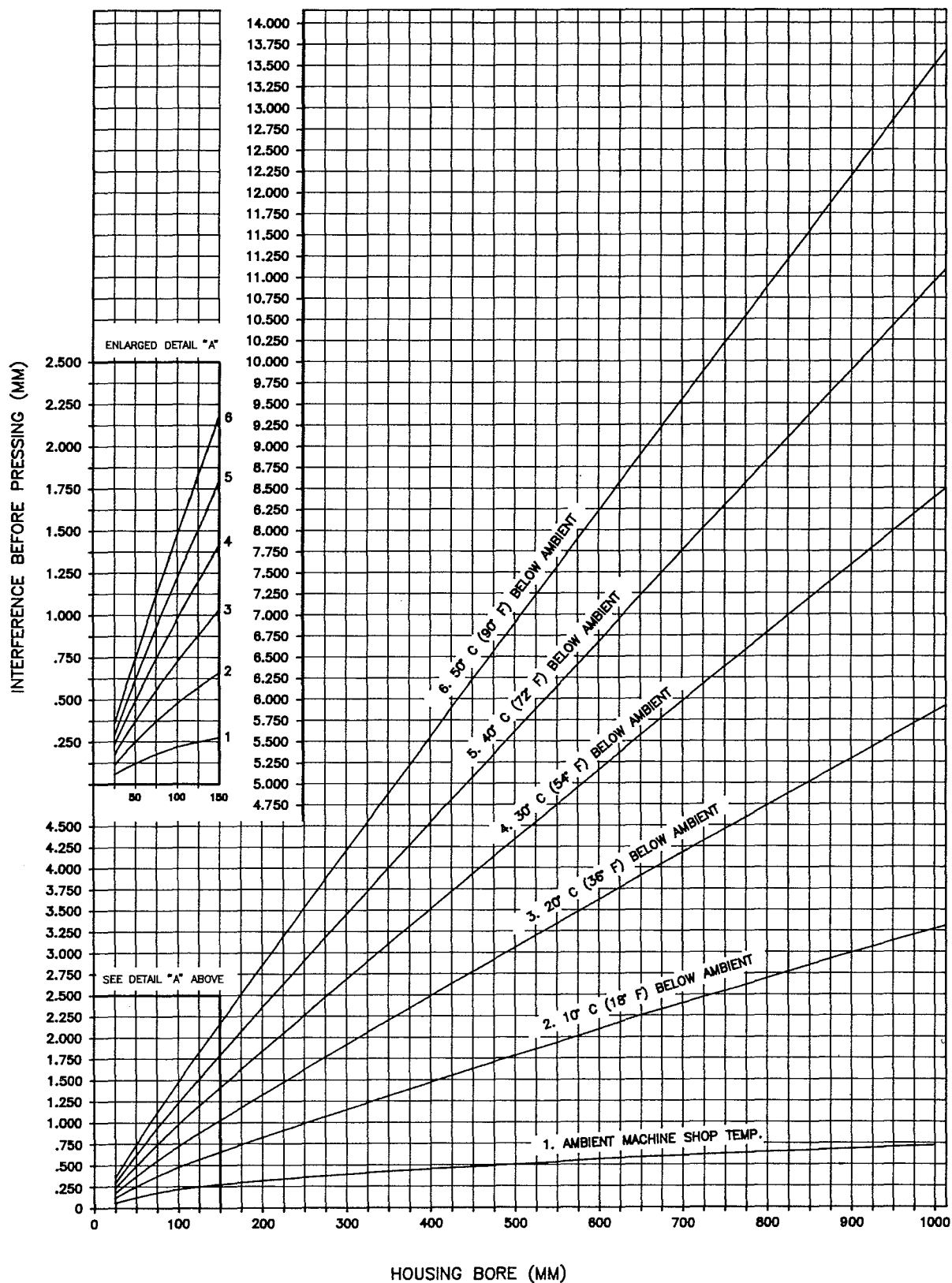
THORDON ELASTOMERIC PRODUCTS

HOUSING INTERFERENCE
GRADE SXL IMPERIAL UNITS

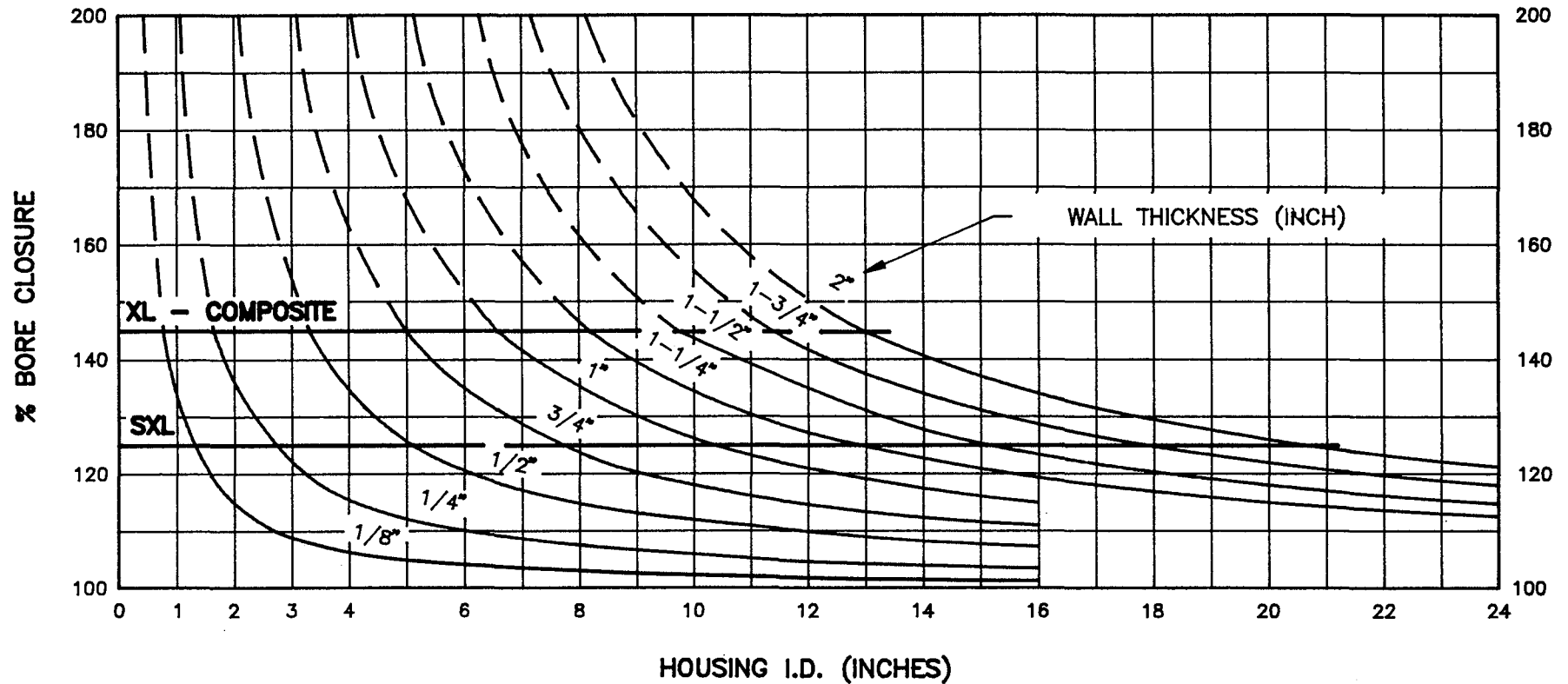


THORDON ELASTOMERIC PRODUCTS

HOUSING INTERFERENCE
GRADE SXL METRIC UNITS

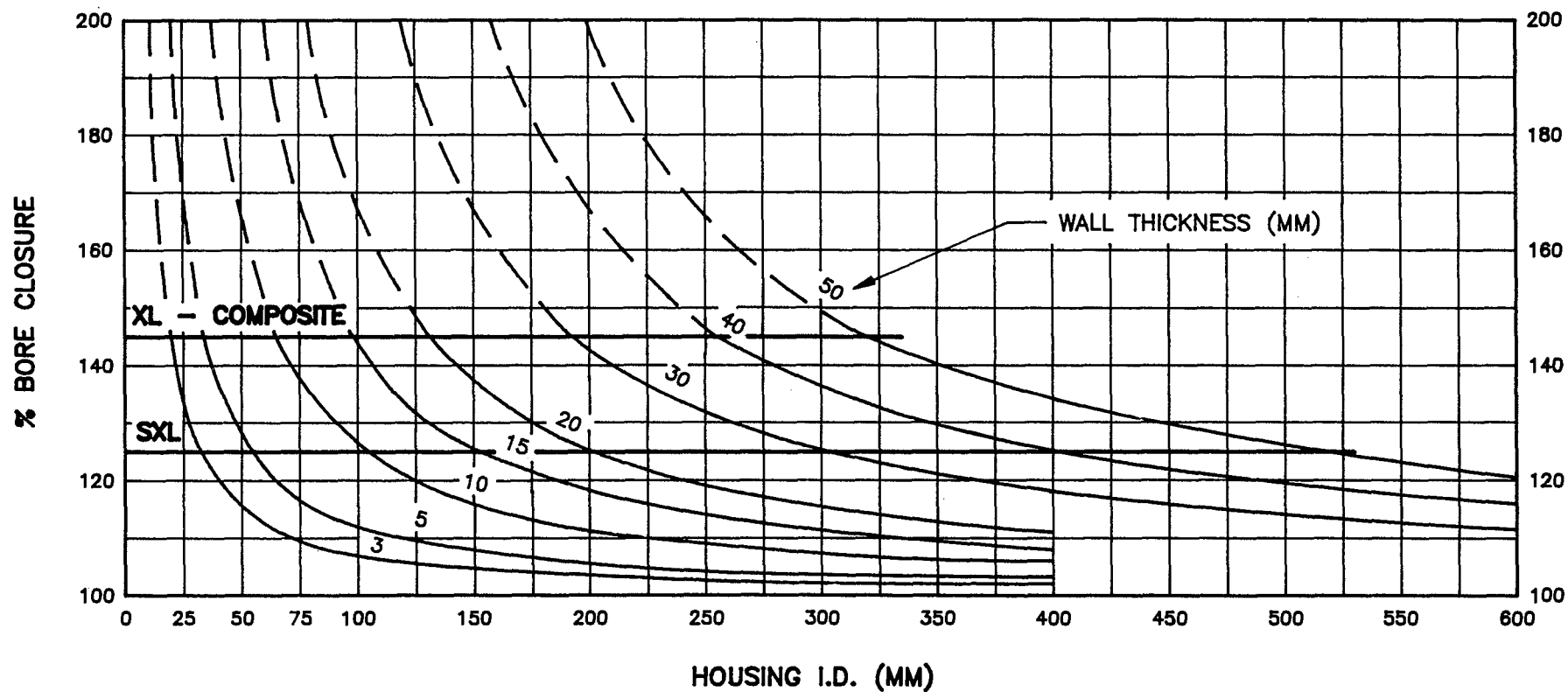


PERCENTAGE BORE CLOSURE AGAINST HOUSING DIAMETER FOR VARIOUS WALL THICKNESSES IMPERIAL



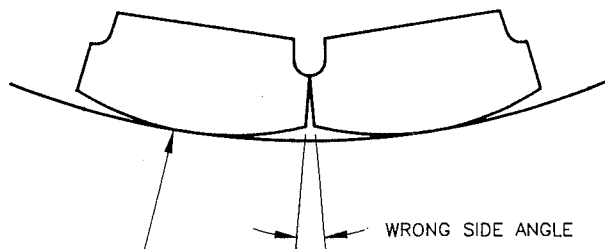
NOTE: THIS GRAPH HAS BEEN LIMITED FOR USE
UP TO A MAXIMUM OF 125% BORE CLOSURE
FOR SXL, AND A MAXIMUM 145% BORE CLOSURE
FOR XL.

PERCENTAGE BORE CLOSURE AGAINST HOUSING DIAMETER FOR VARIOUS WALL THICKNESSES METRIC



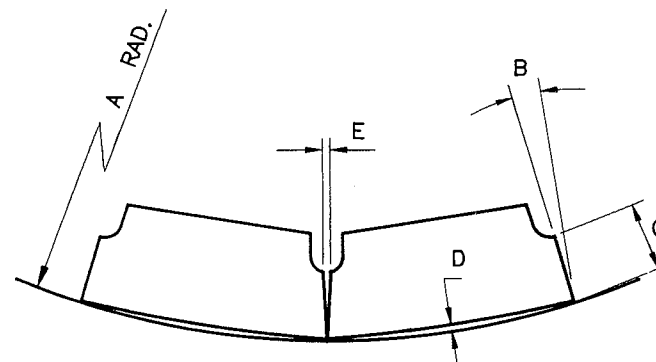
NOTE: THIS GRAPH HAS BEEN LIMITED FOR USE
UP TO A MAXIMUM OF 125% BORE CLOSURE
FOR SXL, AND A MAXIMUM 145% BORE CLOSURE
FOR XL.

INCORRECT FITTING



CONTACT AT ONE POINT IS NOT ACCEPTABLE
AS IT ALLOWS THE STAVE TO ROCK
- STAVE TO BE MACHINED TO A LARGE RADIUS

CORRECT FITTING



NOTE: ALL DIMENSIONS SHOWN IN M.M.

SEGMENT	A	B	C	D	E
"A"	390	6-3/4"	20	.457	.483
"B"	325	7-1/2"	20	.432	.457
"C"	270	8-3/4"	20	.406	.432
"D"	235	9-3/4"	20	.381	.406
"E"	205	9-3/4"	15	.356	.381
"F"	180	9-3/4"	15	.330	.356
"G"	156	9-3/4"	15	.305	.330

NOTE: ALL DIMENSIONS SHOWN IN IN.

SEGMENT	A	B	C	D	E
"A"	15.354	6-3/4"	.787	.018	.019
"B"	12.795	7-1/2"	.787	.017	.018
"C"	10.630	8-3/4"	.787	.016	.017
"D"	9.252	9-3/4"	.787	.015	.016
"E"	8.071	9-3/4"	.591	.014	.015
"F"	7.087	9-3/4"	.591	.013	.014
"G"	6.142	9-3/4"	.512	.012	.013



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DEC. .001" ± 0.01" DEC. .0005" ± 0.005" FRACTIONAL: ± 1/64" ANGULAR: ± 0.5°

TITLE:

THORDON STAVES SHOWING
INCORRECT & CORRECT FITTINGS

DATE: 90/03/12 APP'D BY:
SCALE: N.T.S. APP'D DATE:
DWN BY: RG PLOT:
CAD DIR: \CAD\BEARING\PROPOSAL
PRODUCT:

DWG NO/PART NO:

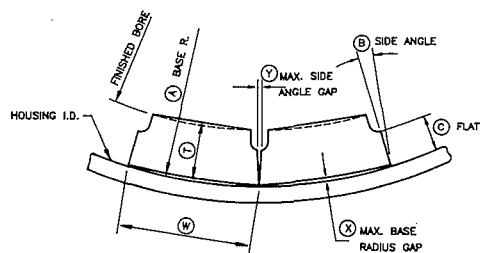
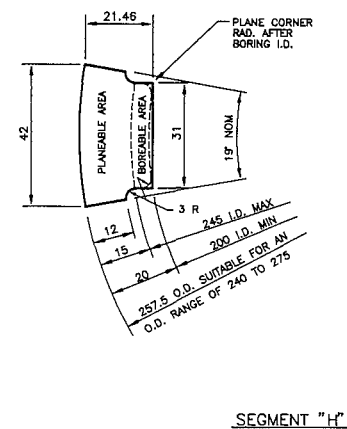
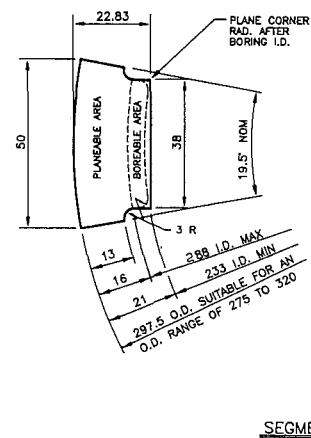
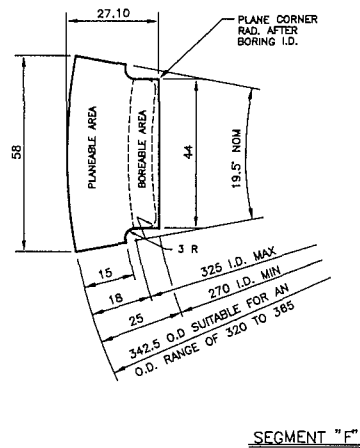
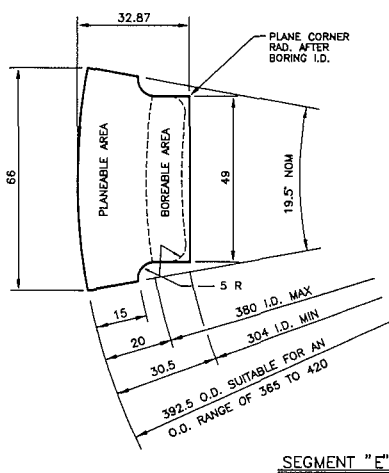
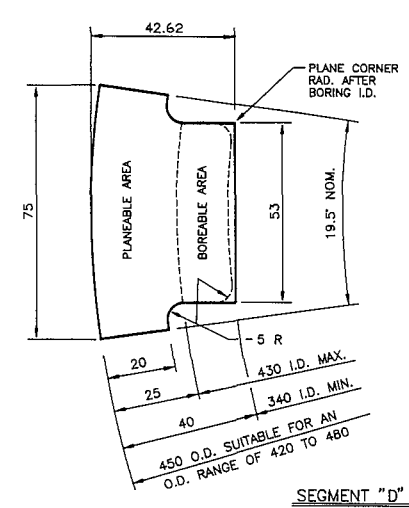
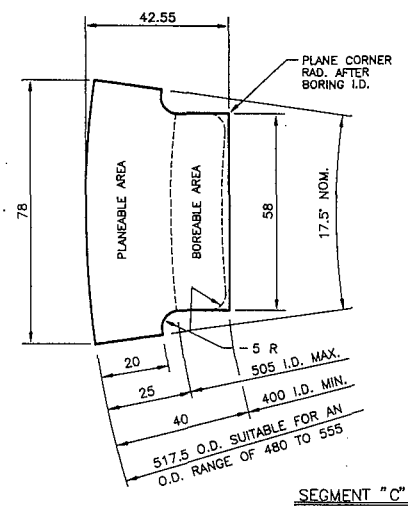
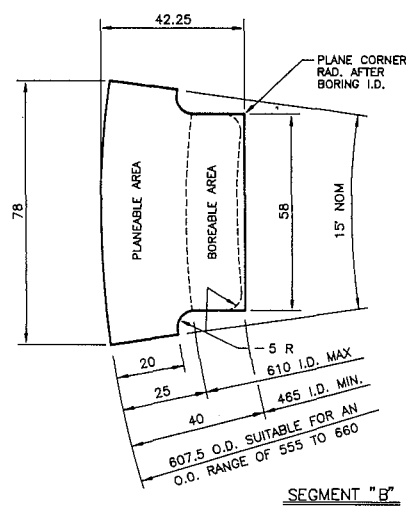
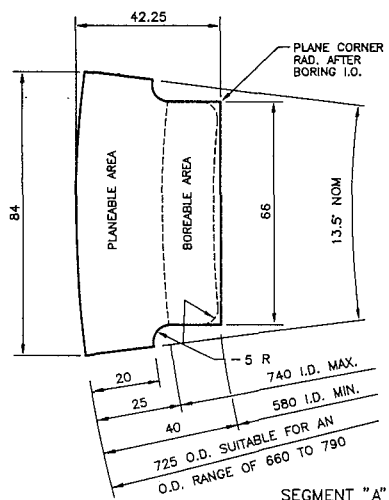
TG-11070

REV:

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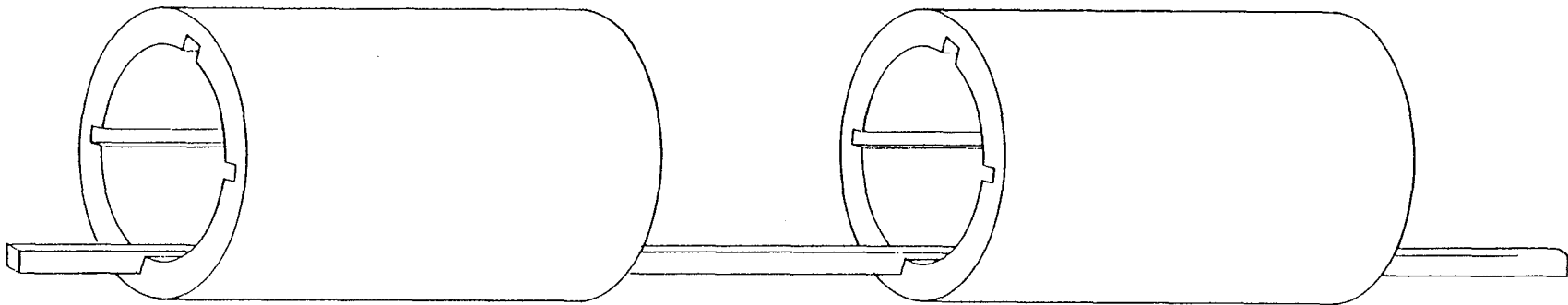
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CUSTOMER:

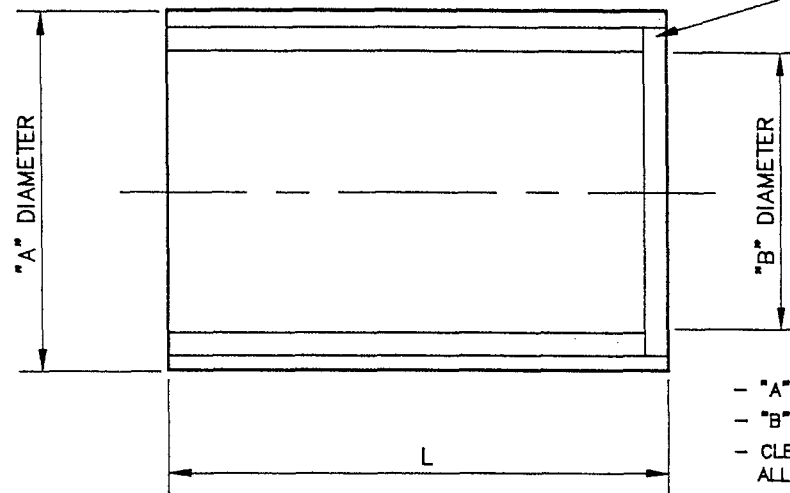
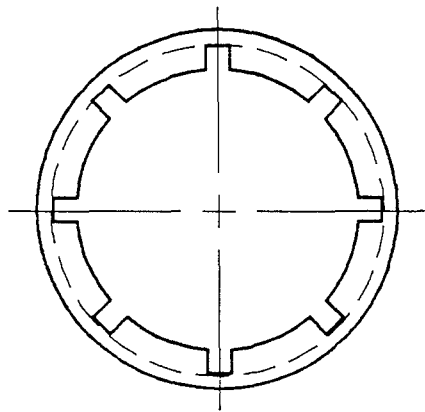


SEGMENT	SHAFT		HOUSING		SEGMENT DIMENSIONS			SEGMENT DIMENSIONS				
	MIN I.D.	MAX I.D.	MIN O.D.	MAX O.D.	(W)	(T)	LENGTH	(A)	(B)	(C)	(X)	(Y)
"A"	580	740	660	790	84	42.25	1000	390	6-3/4"	20	.457	.483
"B"	465	610	555	660	78	42.25	1000	325	7-1/2"	20	.432	.457
"C"	400	505	480	555	78	42.55	1000	270	8-3/4"	20	.406	.432
"D"	340	430	420	480	75	42.62	1000	235	9-3/4"	20	.381	.406
"E"	304	380	365	420	66	32.87	1000	205	9-3/4"	15	.356	.381
"F"	270	325	320	365	58	27.10	1000	180	9-3/4"	15	.330	.356
"G"	233	288	275	320	50	22.83	1000	156	9-3/4"	13	.305	.330
"H"	200	245	240	275	42	21.46	1000	135	9-1/2"	12	.279	.305

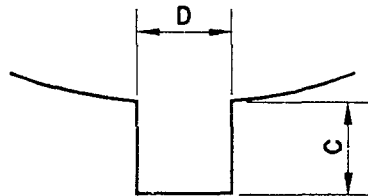
DATE		THOMSON-GORDON LTD. BURLINGTON, ONTARIO, CANADA	
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TOLERANCES UNLESS OTHERWISE SPECIFIED: DEC. .300 ± 0.01" DEC. .3000 ± 0.005" FRACTIONAL: ± 1/64" ANGULAR: ± 0.1°			
TITLE: THORDON XL MOLDED STAVES			
DATE: 8/24/15	APP'D BY:	DWG NO/PART NO:	REV:
SCALE: N.P.S.	APP'D DATE:	TG-11069	
DWN BY: RG	PLOT:	SUPERSEDES: TG-10221	
CAD DIR: YC/2015	PRODUCT: YC/2015 BEARING PROPOSAL		
CUSTOMER:		T.G.	



REV	DESCRIPTION	DATE	BY	ITEM	PART NUMBER	QT'Y.	DESCRIPTION
		<div> THOMSON - GORDON LTD. BURLINGTON, ONTARIO, CANADA</div>					
PRODUCT							
SCALE		DATE		DRAWN BY		APP	
TITLE GROOVE ALIGNMENT							
CUSTOMER							DWG NO TG-10245



SEE NOTE 2



- NOTE 1.- GROOVE DEPTH "C" IS NOT TO EXCEED ONE HALF OF THE WALL THICKNESS
- 2.- AN ANNULAR RING OR RADIAL GROOVE IS RECOMMENDED WHEN INSTALLING MORE THAN 1 LENGTH OF BEARING. THIS ENSURES PROPER WATER FLOW EVEN IN THE EVENT OF MISALIGNMENT OF ONE OR MORE BEARINGS.

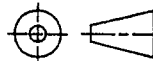

- "A" DIAMETER= HOUSING DIAMETER + INTERFERENCE FIT
- "B" DIAMETER= SHAFT DIA. + BORE CLOSURE + RUNNING
- CLEARANCE + WATER SWELL + THERMAL EXPANSION ALLOWANCE

REFER TO TECHNICAL LITERATURE OR CONTACT TG REPRESENTATIVE FOR DETAILS ON CALCULATIONS

GROOVE DETAILS
GROOVES TO BE EQUALLY SPACED

SHAFT DIA.		NO. GROOVES	C (SEE NOTE)		D	
INCH	MM.		INCH	MM.	INCH $\pm .015$	MM.
TO 1"	25	3	1/8"	3	1/8"	3
1-1/8" TO 2"	29 TO 51	6	3/16"	5	3/16"	5
2-1/8" TO 5"	54 TO 127	8	3/16"	5	1/4"	6
5-1/4" TO 7"	133 TO 178	10	1/4"	6	5/16"	8
7-1/4" TO 12"	184 TO 305	12	5/16"	8	5/16"	8
12-1/4" TO 15"	311 TO 381	14	5/16"	8	5/16"	9.5
15-1/4" TO 20"	387 TO 508	16	3/8"	9.5	3/8"	9.5
20-1/4" TO 28"	514 TO 711	20	3/8"	9.5	3/8"	9.5
28-1/4" TO 36"	717 TO 914	24	3/8"	9.5	7/16"	11

MAXIMUM RECOMMENDED SLEEVE BEARING WEAR			
SHAFT OR SLEEVE DIAMETER		CLEARANCE	
INCH	MM.	INCH	MM.
UP TO 3"	76	.120	3.0
3" TO 12"	76 TO 305	.240	6.1
OVER 12"	OVER 305	.370	9.4

APR. 22/88	JUN. 9/87	APR. 1/87	DATE	 THIRD ANGLE PROJECTION	 THOMSON-GORDON LTD. BURLINGTON, ONTARIO, CANADA		
RADIAL GROOVE ADDED	ADDED 15-1/4" TO 36" SHAFT DIA.	GROOVE RADIUS ELIMINATED AND TITLE WAS WATER LUBE BRG. DESIGN	DESCRIPTION		PRODUCT:	THORDON XL	
					TITLE:	GROOVE DETAIL FOR WATER LUBE BEARING	
					CUSTOMER:		
C	B	A	REV.	SCALE:	N.T.S.	DRAWING NO.: TG-10520	REV. C

PROPELLER SHAFT GROUNDING AND MONITORING ASSEMBLY

INSTRUCTION MANUAL

INDEX

1.0	SLIPRING ASSEMBLY
2.0	SHAFT EARTHING INSTALLATION
3.0	SLIPRING INSTALLATION CHECKS
4.0	SLIPRING MAINTENANCE
5.0	MONITORING EQUIPMENT
6.0	DRAWINGS
7.0	SPARES

1.0 **SLIPRING ASSEMBLY**

A turning propeller shaft on a ship becomes electrically insulated from the hull by the lubricating oil film in the bearings and by the use of non-metallic bearing materials in the tail shaft. When the shaft is insulated in this way an electrical potential can be measured between the shaft and the hull and this can accelerate corrosion in the ship. If the ship has a system of cathodic protection, whether it is sacrificial anodes or an impressed current system, the shaft insulation will prevent the propeller and the boss from receiving protection.

The electrical potential between the shaft and the hull can also cause a heavy current to flow in bearings when the oil film breaks down or is contaminated with seawater. This current can cause deep pitting of the bearing surface. Excessive wear on the shaft bearings can often be traced to this cause.

Trouble can be avoided and cathodic protection extended to the propeller if the shaft is properly earthed with a propeller slipring. The effectiveness of the shaft earthing system should encourage a maximum contact resistance of no greater than 0.001 ohms for a water filled bearing and 0.01 ohms for an oil filled bearing.

Our own tests indicate that high silver content brushes running on a silver track have repeatable low conductivity that can maintain these limits and ensure a low resistance contact is maintained even under dirty conditions.

The shaft earthing assembly comprises a pair of high silver content/graphite compound brushes mounted in a balanced brush holder, running on a copper slipring with a solid silver inlay track.

Each brush holder has an adjustable spring tensioner with 5 settings, which is supplied preset to the minimum, and result in a pressure of 450 grams on each brush.

At this pressure the expected life of the brushes is in excess of one year.

2.0 **SHAFT EARTHING INSTALLATION**

The shaft slipring is supplied as a complete unit with copper/silver band and clamping arrangement which can be easily installed by competent ship's engineering personnel, in the following order:

- (a) Select a suitable position on the shaft to install the slipring which should be close to a pedestal or convenient piece of ships structure where the brush holder can be installed.

Then thoroughly clean the shaft in the area where the slipring is to be fitted ensuring that all grease, dirt and impurities on the shaft are removed.

- (b) The sliprings are manufactured slightly oversized to allow for a small variation in shaft diameter so when installing, the excess material should be removed by filing or cutting joint faces before securing the clamping arrangements.
- (c) After removing the excess material the two band clamps are tightened so that the copper/silver strip is a close tight fit around the shaft.
- (d) Remove any excess banding strip from the assembly and ensure that this strip is cut back to the housing.
- (e) Fill the join between the two sliprings and soft solder to ensure a smooth surface.
- (f) Install a 20mm diameter rod (brush holder spigot) on a convenient piece of ships structure or pedestal bearing so that it is centre parallel to the shaft centre in both planes. (The mounting bracket and rod are ship or shipyard supply items.)
- (g) It is essential that the complete brush holder assembly should provide a good electrical contact between the shaft and the hull, therefore the brush holder spigot support, should either be welded to the ships structure or if bolted, a short length of 70mm² bonding cable should be connected between the brush holder and ships structure.
- (h) The brush holder should be clamped in this rod and aligned centrally over the silver track.

- (i) Install the silver graphite brushes and the brush holder and check that the clearance between the silver track and the brush holder is approximately 3mm.
- (j) After checking this dimension tighten the brush holder into position.
- (k) Connect the silver graphite brushes to their connections and check all bolts and nuts for tightness and that the brush pressure is set at 50g/kw.

NOTE

TO PREVENT BUSH 'BOUNCE' AND ENSURE MAXIMUM UTILISATION OF THE SILVER GRAPHITE BRUSHES, IT IS ESSENTIAL THAT THE JOINTS FORM A SMOOTH, FLUSH PROFILE OVER THE FULL EXTENT OF THE SLIPRINGS.

DRAWING No. AM1041 - DETAIL OF BAND CLAMP ASSEMBLY REFERS.

3.0 SLIPRING INSTALLATION CHECKS

- | | | |
|----|---|--------|
| 1. | Confirm slipring and brush gear are installed as per drawing No 1041. | |
| 2. | Is assembly clean and free from oil and grease? | YES/NO |
| 3. | Is slipring a tight fit to the shaft over its whole length?
Ensure no bumps or indentations can be felt over the whole of the working surface. | YES/NO |
| 4. | Are joints a good fit with no gap? | YES/NO |
| 5. | Is brush holder secure on its shaft? | YES/NO |
| 6. | Confirm that brush holder and its mounting are solid and that it will not be affected by vibration? | YES/NO |
| 7. | Confirm that brush faces are tangential to slipring. | YES/NO |
| 8. | Confirm that brushes are free to move in their holders. | YES/NO |
| 9. | Is there electrical continuity between tail shaft and hull? | YES/NO |

4.0 SLIPRING MAINTENANCE

This grounding assembly should be checked every seven days for cleanliness. If there has been a build-up of oil on the slipring face this should be removed with a degreaser. Inspect and clean the brushes and brush holder to prevent blocking from dirt. Inspect the brush copper leads (pig tails) to ensure they have not become loose or corroded. The brush wear-down should be noted and the compression of the hold-down springs on the brushes should be adjusted to ensure good electrical contact.

5.0**PROPELLER SHAFT MONITORING M/V METER (When fitted).**

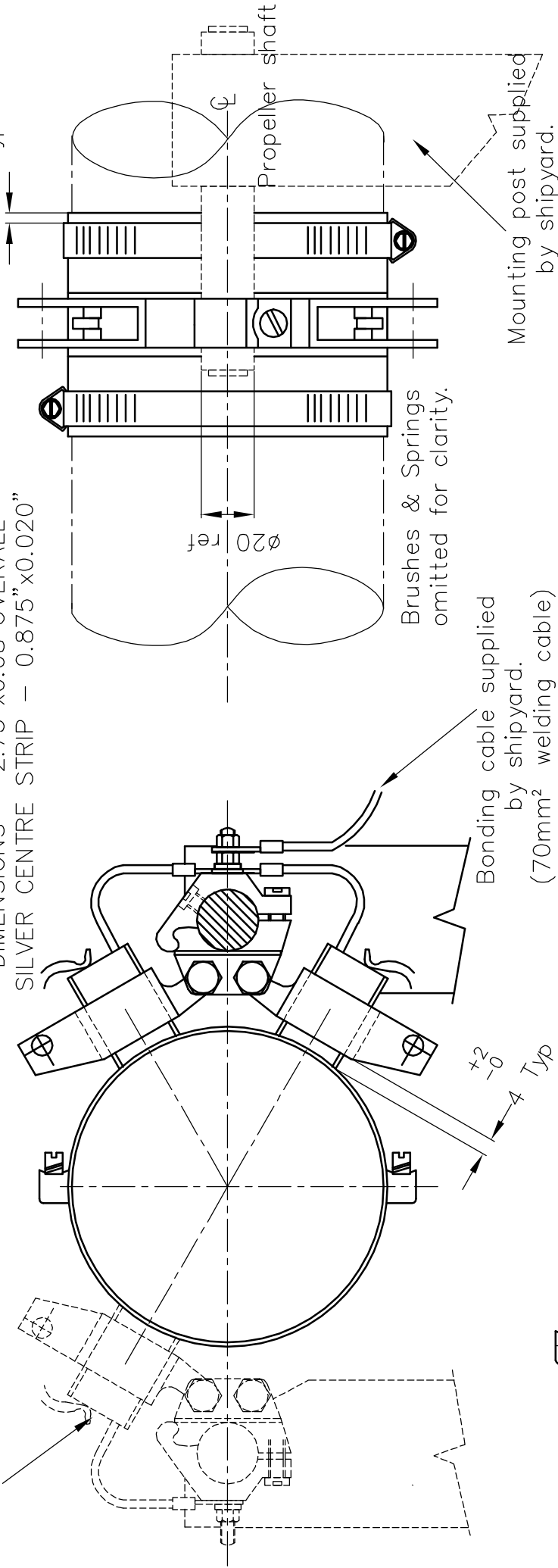
- A. Fabricate a support for an additional spindle to mount the second brush holder and brush (drawing AM1042 & AM1038).
The second brush holder must be insulated from the main hull structure mounted on either an insulated spindle or an insulated sleeve on a steel spindle (Drawing AM1043).
- B. Adjust the brush holder so that at the nearest point they are approximately 3-4mm from the surface of the silver insert in the slip-ring assembly. The brush holders are geared together to ensure symmetrical adjustment. Tighten the two brush gear adjustment screws.
- C. Tighten the brush assembly clamp screw to ensure the assembly in position on the spindle with the brush holders central over the silver insert.
- D. Adjacent to the propeller shaft slip-ring assembly and easily visible mount the potential monitoring panel (Drawing AM709 / AM709-1) on a vertical surface.
- E. Place the brush in its holder and connect the cable tail to the clamp back to the brush holder assembly. Adjust the slip-ring so that the brush pressure is 450 grams.
- F. Provide and install the inter-connecting cables between the brush holder on the insulated spindle and the hull [hull to terminal 2] use a 1.5mm² flexible cable.
- G. Provide and install a cable between the ship structure and the other terminal of the millivolt meter [shaft to terminal one] use a 1.5mm² flexible cable.
- H. A reading of 25.0 to 50.0 mV is acceptable. However a potential greater than 50 mV is an indication of a dirty slip-ring which should be cleaned.

6.0

DRAWINGS.

See drg. AM 1043
for Monitor Brush Assy.

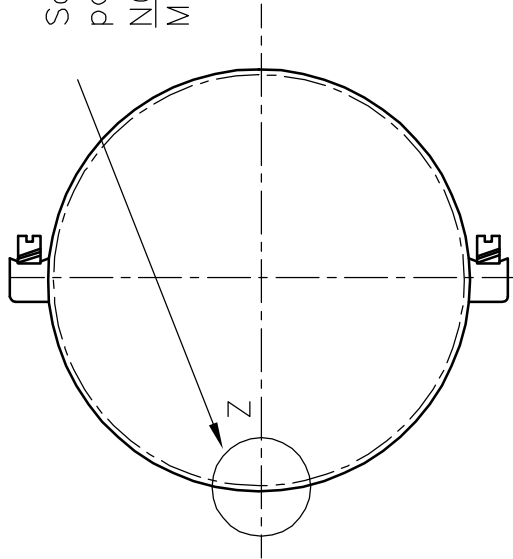
MATERIAL – COPPER/SILVER INLAY
DIMENSIONS – 2.75" x 0.08" OVERALL
SILVER CENTRE STRIP – 0.875" x 0.020"



Soft solder infill – file and
polish at final assembly. (See detail Z)

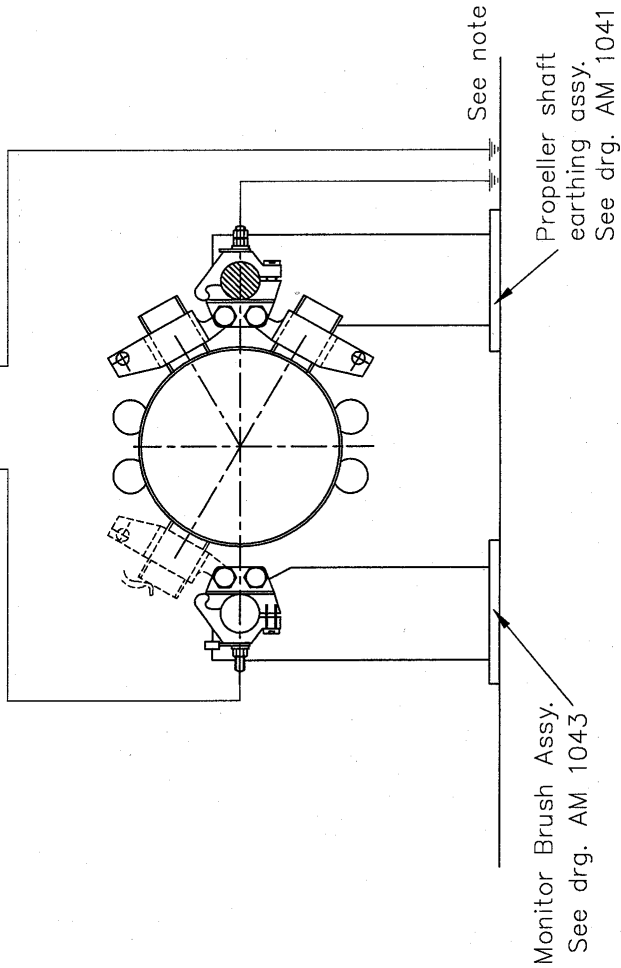
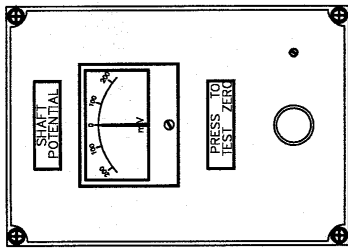
NOTE

Mating faces MUST BE FLUSH




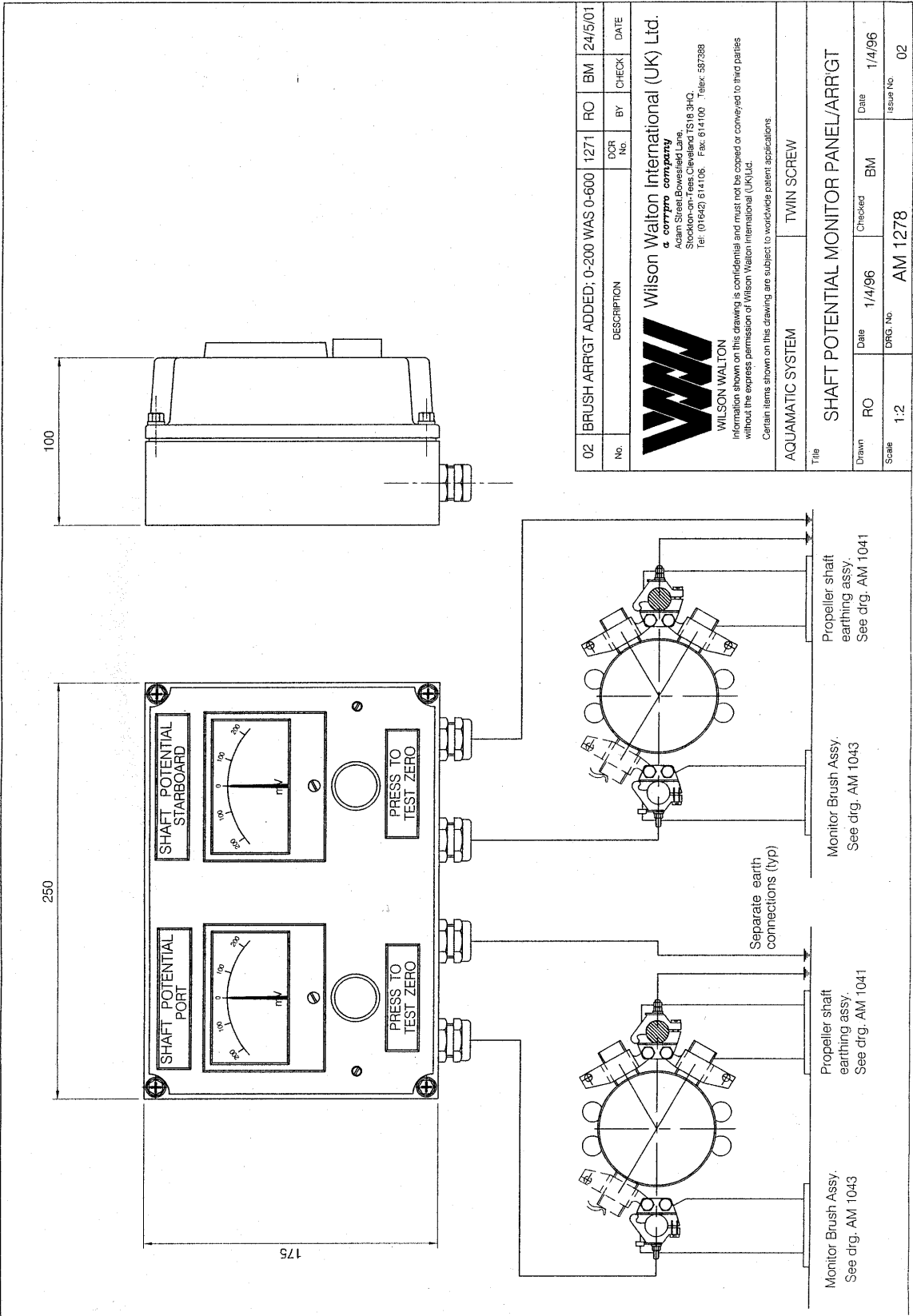
Details of Band Clamp
Assembly.
(stainless steel)

O	REDRAWN ONTO CAD	C.G.	21/3/96
No.	DESCRIPTION	DCR No.	DATE
Wilson Walton International (UK) Ltd. a corpo company Adam Street, Boverfield Lane, Stockton-on-Tees, Cleveland TS18 3HQ. Tel: (01642) 614106. Fax: 614100. Telex: 567386			
WILSON WALTON Information shown on this drawing is confidential and must not be copied or conveyed to third parties without the express permission of Wilson Walton International (UK) Ltd. Certain items shown on this drawing are subject to worldwide patent applications.			
P & O			
PROPELLER SHAFT EARTHING ASSEMBLY FOR COPPER / SILVER INLAY SLIPRING			
Drawn	C.G.	Date	21/3/96
Scale	N.T.S.	DRG. No.	AM 1041
		Checked	PR
		Date	18/4/96
		Issue No.	00



NOTE
Earth connections to be
separate from each other.

O	REDRAWN ONTO CAD	C.G.	25/3/96				
No.	DESCRIPTION	DWG No.	BY	CHECK	DATE		
<div><div></div><div>WILSON WALTON a corpo company Adams Street, Bownessfield Lane, Stockton-on-Tees, Cleveland TS18 3JQ. Tel: (01642) 814106. Fax 814100 Telec 897388</div></div> <p>Information shown on this drawing is confidential and must not be copied or conveyed to third parties without the express permission of Wilson Walton International (UK) Ltd.</p> <p>Certain items shown on this drawing are subject to worldwide patent applications.</p>							
<div><div></div><div>MONITOR UNIT & SLIPRING INTERCONNECTION DIAGRAM</div></div>							
Drawn	C.G.	Date	25/3/96	PR	Checked	Date	22/4/96
Scale	N.T.S.	DWG No.	AM 1045			Issue No.	0



7.0

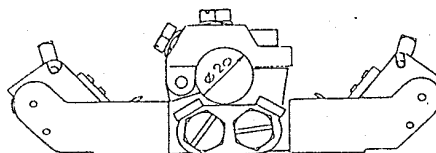
SPARES.

AQUAMATIC SPARE PARTS LIST.
PROPELLER SHAFT GROUNDING
&
MONITORING ASSEMBLY.

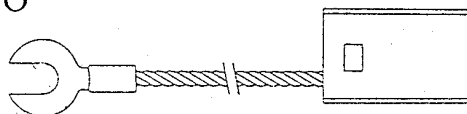
EQUIPMENT	QUANTITY	DRAWING.
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GROUNDING ASSEMBLY.

DOUBLE BRUSH HOLDER ONE

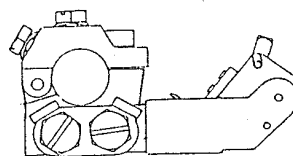


SILVER GRAPHITE BRUSH TWO

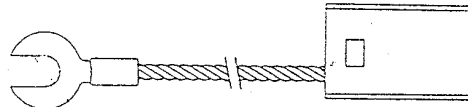


MONITORING ASSEMBLY.

SINGLE BRUSH HOLDER ONE



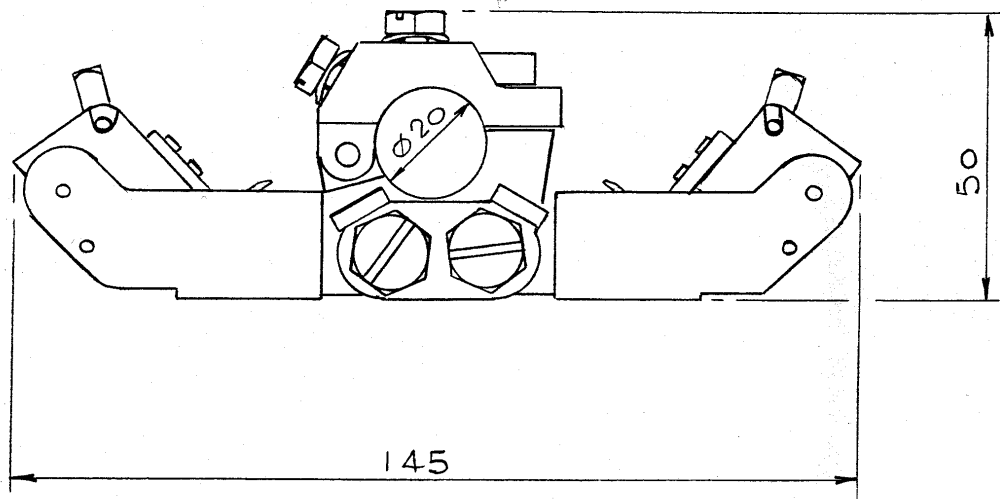
SILVER GRPHITE BRUSH ONE



NOTE

UNIT AS DRAWN TO BE USED AS EARTHING ASSY
SEE DRG. N° AM.1041.

ONE ARM TO BE REMOVED FOR USE AS MONITORING
ASSY. SEE DRG. N° AM 1043.



FOR USE WITH SILVER GRAPHITE BRUSH DRG N° AM 1042



Wilson, Walton International (UK) Ltd.

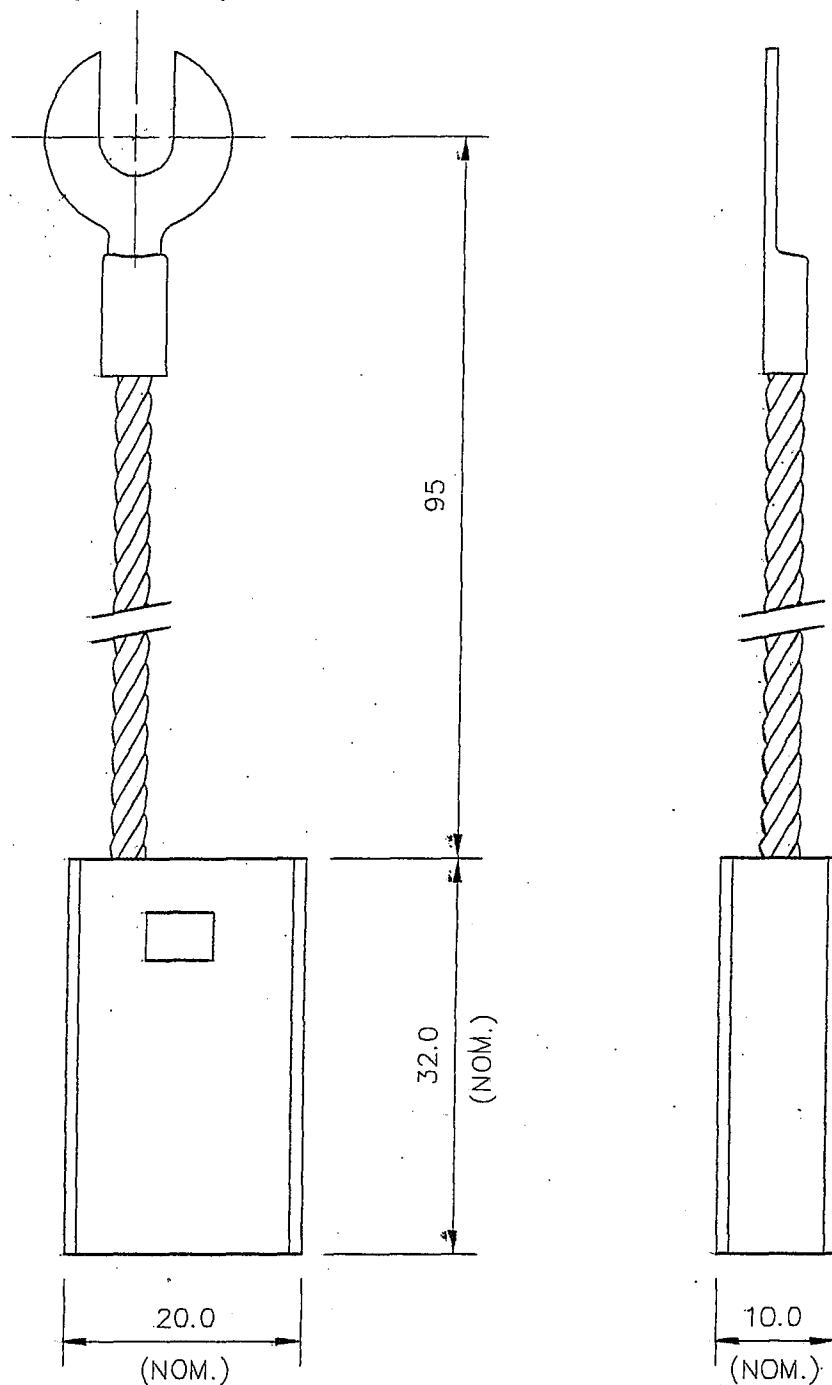
Adam Street, Bowesfield Lane,
Stockton-on-Tees, Cleveland TS18 3HQ.
Tel: (0642) 614106 Telex: 587388

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must not be copied or conveyed to third parties without the
express permission of Wilson, Walton International (UK) Ltd.

BRUSH HOLDER (SILVER GRAPHITE BRUSH)

DRAWN	RO	DATE	7/3/88	SCALE	1:1
-------	----	------	--------	-------	-----

DRAWING No.	AM 1038	ISSUE
-------------	---------	-------



MATERIAL : GRADE SM9173



Wilson Walton International (UK) Ltd.

a corporate company
Adam Street, Bowesfield Lane,
Stockton-on-Tees, Cleveland TS18 8HQ.
Tel: (01642) 614106. Fax: 614100. Telex: 887388

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Certain items shown on this drawing are subject to worldwide patent applications.

SILVER GRAPHITE EARTHING AND MONITORING BRUSH

Drawn	Date	Checked	Date	Chill No.	Scale
DPS	3/10/95	<i>[Signature]</i>	26/10/95	N/A	NTS
DRG.No. AM 1042/1					ISSUE 01

Oiltech PWO

INSTALLATIONS- OCH SERVICEANVISNINGAR ♦ INSTALLATION AND SERVICING INSTRUCTIONS
INSTALLATIONS- UND WARTUNGSANLEITUNG ♦ NOTICE D'INSTALLATION ET DE
MAINTENANCE ♦ INSTALLATIE EN ONDERHOUD INSTRUCTIES ♦ INSTRUCCIONES DE
FUNCIONAMIENTO Y MANTENIMIENTO ♦ ISTRUZIONI DI MONTAGGIO E MANUTENZIONE



Följ denna anvisning noga vid installation av Oiltechs vattenoljekylare typ PWO.

Anslutning av in- och utgående olja och vatten

För standard PWO vattenoljekylare:

Oljeanslutningarnas diametrar är alltid större än vattenanslutningarnas.

Anslut olja in till undre vänstra anslutningen. (F3)

Anslut olja ut till övre vänstra anslutningen. (F1).

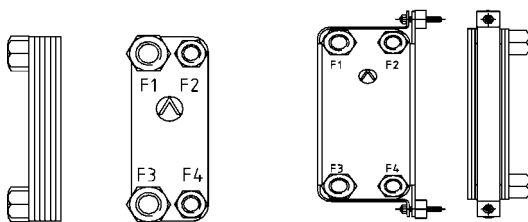
Anslut vatten in till övre högra anslutningen. (F2).

Anslut vatten ut till undre högra anslutningen. (F4)

Observera att PWO B56 har en annorlunda in-koppling!

Använd filter om det finns risk för att partiklar i vätskan kan sätta igen kylaren.

Partiklar mindre än 1 mm utgör normalt inga problem.



Placering

Kylaren kan monteras i vilket läge som helst. Finns behov av att kunna tömma något av omloppen, bör hänsyn dock tas till detta. För att minimera risken för igensättning på vattensidan, montera PWO vertikalt enligt bild.

Hur man undviker materialspänning

Alla enheter, som inte är försedda med stödben, bör monteras med hjälp av Oiltechs fästklämma runt kylaren. Vissa större enheter bör dessutom utrustas med fixeringsskruvar på anslutningssidan. Kylaren bör dock inte hänga enbart i dessa skruvar. Kylaren bör ej monteras i stel ram. Använd flexibla hydraulslangar för mjuk och elastisk installation. All rördragning skall utföras på så sätt att spänningar och vibrationer på anslutningar och kylare minimeras. I hydraulsystem där kylaren är ansluten till retursidan, använd slangar och eventuellt en by-passventil på oljeinloppet för att undvika övertryck.

Tecken på igensättning

För att fastställa igensättning, kontrollmät kylarens ingående och utgående vattentemperatur. Igensättning minskar värmeöverföringsförmågan, vilket resulterar i ökad vattenförbrukning, minskad skillnad mellan in- och utgående vattentemperatur och förhöjd oljetemperatur.

En annan metod är att mäta tryckfallet över kylaren. Igensatta och tränga passager ger ökad flödeshastighet och ökat tryckfall. Det är viktigt att vattenflödet är rätt när mätningar görs. Avvikelser från angivet flöde påverkar naturligtvis temperaturen och tryckfallet.

Rengöring

Som regel får man bort alla mjuka avlagringar genom att spola kylaren med vatten i riktning motsatt den normala flödesvägen. Vid hårda avlagringar, skölj kylaren med svag syra. Använd 5% fosforsyra eller om kylaren görs rent ofta med 5% oxalsyra eller annan liknande svag organisk syra. Skölj därefter med stora mängder vatten. All syra måste avlägsnas innan systemet startas igen. Vänta aldrig med rengöring tills kylaren är helt igensatt.

Material AISI 316. Max arbetstryck 31 bar, max arbetstemperatur 185°C. Alla PWO vattenoljekylare är trycktestade vid 47 bar innan leverans.

Lean cuidadosamente esta información antes de instalar el intercambiador agua/aceite PWO.

Conexión de entrada y salida para aceite y agua

PWO modelo estándar:

El diámetro de conexión del aceite, siempre tiene que ser mayor que la del agua.

La entrada del aceite tiene que ser por abajo izquierda (F3).

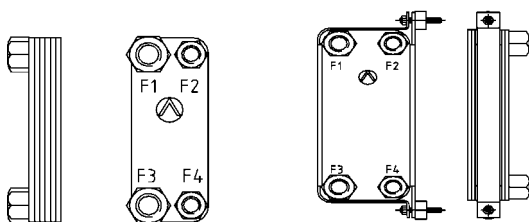
La salida del aceite tiene que ser por arriba izquierda (F1).

La entrada del agua tiene que ser por arriba derecha (F2).

La salida del agua tiene que ser por abajo derecha (F4).

El modelo PWO B56 lleva otro tipo de conexión.

Para evitar obstrucciones, utilizar un filtro. Partículas menores de 1 mm, no suelen causar problemas.



Montaje

El intercambiador puede colocarse en cualquier posición. Se ha de tener en cuenta la necesidad de purgar el circuito. Para minimizar obstrucciones en el circuito de agua, colocar el PWO en posición vertical como se indica en las figuras arriba.

Cómo evitar fatigas de material

Todos los intercambiadores - sin soporte - se deben montar mediante abrazaderas. Algunos modelos grandes equipan también pasadores roscados, situados en el lado conexión, que sin embargo no debe emplearse como sujeción única del intercambiador. Evitar montajes rígidos. Utilizar conexiones flexibles. Todos los conexiones deben realizarse para minimizar las vibraciones. En aquellos circuitos hidráulicos donde el intercambiador se instala en retorno, emplear tuberías flexibles para reducir pulsaciones y ev. una válvula by-pass en la entrada del aceite para evitar sobrepresiones.

Síntomas de obstrucción

El estado de obstrucción puede valorarse, verificando las temperaturas de entrada y salida del agua, ya que hace disminuir la transferencia térmica y por lo tanto aumenta el consumo de agua con valores de temperatura del agua inferiores a los especificados, y temperatura de aceite elevada.

Otra manera de analizar la obstrucción es controlando la pérdida de carga. Las obstrucciones reducen la sección, aumenta la velocidad y por lo tanto mayor pérdida de carga. Antes de aplicar estos criterios verificar que el caudal de agua es el especificado. Un caudal de agua diferente afecta a la temperatura y a la pérdida de carga, como es de prever.

Limpieza

En general, los depósitos no incrustantes pueden eliminarse, enjuagando el intercambiador a contracorriente y los depósitos incrustantes utilizando un ácido débil, como por ejemplo ácido fosfórico al 5%. Si el intercambiador debe limpiarse frecuentemente, utilizar ácido oxálico al 5%, u otro ácido orgánico similar. Una vez limpio, y antes de su conexión al circuito, debe enjuagarse con abundante agua para eliminar toda traza de ácido. Limpiar el intercambiador sin esperar a que se obstruya totalmente.

Material AISI 316. Presión máxima de servicio: 31 bar. Temperatura máxima de servicio: 185°C. Todos los intercambiadores PWO han sido probados hidráulicamente a 47 bar.

Attenersi scrupolosamente alle istruzioni per l'installazione dello scambiatore acqua - olio Oiltech PWO.

Collegamento degli attacchi dell'olio e dell'acqua

Scambiatore standard acqua-olio PWO:

I diametri degli attacchi olio sono sempre maggiori di quelli per l'acqua.

L'ingresso dell'olio deve essere collegato all'attacco inferiore sinistro. (F3)

L'uscita dell'olio deve essere collegata all'attacco superiore sinistro. (F1)

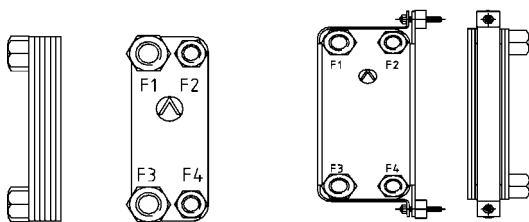
L'ingresso dell'acqua deve essere collegato all'attacco superiore destro. (F2)

L'uscita dell'acqua deve essere collegata all'attacco inferiore destro. (F4)

N.B. Il collegamento olio/acqua è differente per lo scambiatore modello PWO B56.

Inserire un filtro se nel fluido fossero presenti particelle che potrebbero intasare lo scambiatore.

Particelle fino ad 1 mm di diametro non causano alcun inconveniente.



Posizionamento dello scambiatore

Lo scambiatore può essere montato in qualsiasi posizione, considerando la messa a scarico del circuito.

Per ridurre le incrostazioni lato acqua, installare il PWO in verticale come presentato nella figura.

Come evitare la fatica del materiale

Tutte gli scambiatori - senza supporto - sono montate con una staffa che avvolge lo scambiatore. Alconi modelli grandi sono dotate di prigionieri, da non considerarsi come bulloni di sostegno, posizionati sul lato attacchi olio/acqua.

Non montare lo scambiatore rigidamente, ma interporre supporti elastici Armaflex o equivalenti (antivibranti). I collegamenti con le tubazioni devono essere eseguiti in modo da ridurre al

minimo le vibrazioni. Nei sistemi idraulici, dove lo scambiatore viene montato sulla linea di ritorno, occorre prevedere tubi flessibili e eventuali by-pass sulla linea d'ingresso dell'olio per evitare sovrappressioni.

Verifica del grado d'incrostazione

La misurazione delle temperature dell'acqua, in ingresso ed in uscita dallo scambiatore, indica se si è verificato un fenomeno di incrostazione in quanto si riduce lo scambio termico ed aumenta il consumo dell'acqua; riduce infatti la differenza delle temperature dell'acqua e aumenta la temperatura dell'olio.

Un altro metodo è il controllo della caduta di pressione attraverso lo scambiatore. L'aumento della velocità e aumento della caduta di pressione, possono verificarsi a causa di incrostazioni e passaggi ridotti.

E' importante controllare che la portata dell'acqua sia come da specifica, poiché ogni variazione della stessa può influenzare la temperatura e la caduta di pressione.

Pulizia

Quando è necessario, un lavaggio controcorrente (controflussaggio) con acqua rimuove il grosso del deposito "tenere". Per depositi duri, far circolare acido fosforico al 5% (acido debole) attraverso lo scambiatore, sempre in direzione opposta al normale flusso d'acqua; per pulizie frequenti utilizzare invece 5% di acido ossalico (o analogo acido organico). Risciacquare poi con acqua, per eliminare tutto l'acido dallo scambiatore prima di far ripartire il sistema. La pulizia si deve effettuare prima che lo scambiatore sia completamente intasato.

Materia AISI 316. Massima pressione di lavoro: 31 bar. Massima temperatura di lavoro: 185°C.

Gli scambiatori saldobrasati sono tutti testati a 47 bar per controllare le saldature e quindi la tenuta in pressione dei fluidi.

Neem deze instructies voor de installatie van Oiltech PWO water/olie koelers nauwkeurig in acht.

Aansluiting van olie en water in- en uitlaat

Standaard PWO water/olie koeler:

De diameters van de olie aansluitingen zijn altijd groter dan die van de water aansluitingen.

De olie inlaat moet worden aangesloten aan de linksonder aansluiting (F3).

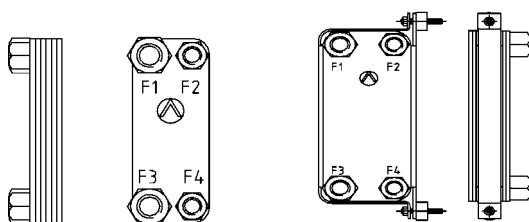
De olie uitlaat moet worden aangesloten aan de linksboven aansluiting (F1).

De water inlaat moet worden aangesloten aan de rechtsboven aansluiting (F2).

De water uitlaat moet worden aangesloten aan de rechtsonder aansluiting (F4).

Let op! Het type PWO B56 heeft afwijkende aansluitingen.

Gebruik een waterfilter, indien het koelwater opgeloste deeltjes bevat met een diameter groter dan 1 mm. Kleinere opgeloste deeltjes veroorzaken in het algemeen geen probleem.



Montage van de koeler

De PWO water/olie koeler kan in alle posities gemonteerd worden, rekening houdend met de behoefte aan aftappen. De positie van de koeler dient vertikaal te zijn zoals afgebeeld, om vervuiling van de waterzijde te voorkomen. Zie boven!

Vermijden van spanningen in het materiaal

Alle modellen zonder frame dienen te worden gemonteerd met een beugel rondom de koeler. Sommige grotere modellen zijn uitgerust met standaard aangelaste draadeinden aan de aansluitzijde. De koeler mag echter niet alleen aan deze draadeinden opgehangen worden.

Monteer de koeler niet op een onbuigzaam onderstel. Gebruik het Armaflex-systeem of vergelijkbare flexibele vorm van installatie. Alle aansluitingen moeten zodanig gebeuren dat de

trillingen op de koeler tot een minimum worden beperkt. In hydraulische systemen waar de koeler in de retourleiding geplaatst wordt dienen er flexibele slangen te worden toegepast om pulsaties te verminderen en ev. een by-pass klep in de olie inlaat om overdruk te vermijden.

Signalering van vervuiling

Door de watertemperatuur aan de in- en uitlaat van de koeler te meten kan worden bepaald of deze al dan niet vervuild is. Als de inwendige oppervlakte van de koeler vervuild is, vermindert de warmte-overdracht, het geen waterverbruik verhoogt en het watertemperatuurverschil tussen inlaat en uitlaat vermindert alsmede de olietemperatuur in het systeem verhoogt.

De vervuilingsgraad kan ook worden bepaald door de drukval over de waterzijde van de koeler te meten. Vervuiling in het watercircuit van de koeler veroorzaakt een hoge vloeistofsnelheid en een hoge drukval. Alvorens deze methode te gebruiken, moet u ervoor zorgen dat het waterdebiet gelijk is aan de gespecificeerde waarde, want een afwijkend waterdebiet heeft invloed op het temperatuurverschil en de drukval over de koeler.

Onderhoud

De meest losse aanslag verwijderen middels een waterspoeling in omgekeerde richting dan de standaard stroomrichting van het koelwater. Als een harde aanslag is gevormd, laat dan een zwak zuur door koeler circuleren. Gebruik 5% fosfor zuur of, indien dikwijls gereinigd 5% oxaalzuur of een ander zwak organisch zuur. Spoel daarna met veel water om alle zuuraanslag te verwijderen alvorens het systeem weer in gebruik te stellen. Gebruik altijd persoonlijke beschermingsmiddelen tijdens spoelwerkzaamheden.

Materiaal: AISI 316. Maximale bedrijfsdruk: 31 bar.
Maximale bedrijfstemperatuur: 185°C. Alle PWO water/olie koelers zijn getest op een druk van 47 bar.

Please read this information prior to installing Oiltech PWO water oil cooler.

Connection of oil/water inlets and outlets

Standard PWO water oil cooler:

Oil connection diameters should always be larger than water connection diameters.

Connect inlet oil to lower left connection (F3).

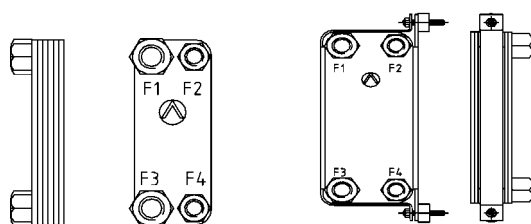
Connect oil outlet to upper left connection. (F1)

Connect water inlet to upper right connection. (F2)

Connect water outlet to lower right connection (F4).

Please note that on PWO B56 the oil/water inlets and outlets are different to above!

Use filter to prevent clogging due to contamination. However, deposits less than 1 mm will not cause any problem.



capacity, causing increased water consumption, reduced difference in water inlet and outlet temperature and a rise in oil temperature.

Another method is to check pressure drop across the cooler. Clogged and narrow passages will cause acceleration in flow rate and increased pressure drop. Always observe that water flow is as advised. Any deviation from stated flow will, of course, affect temperature and pressure drop.

Cleaning

In general, all minor deposits can be removed by back flushing the cooler with water. Fouling can be dealt with using light acid. Use 5% phosphoric acid or, when cleaned frequently, 5% oxalic acid or similar light organic acid. Rinse the cooler with a large quantity of water. Remove all acids before restarting the system. Always clean the cooler before it becomes completely clogged.

Material AISI 316. Max. working pressure 31 bar. Max. working temperature 185°C. All PWO water oil coolers are pressure tested for leakage at 47 bar prior to delivery.

Positioning

The cooler can be installed in any position, bearing in mind the need for draining. To minimise clogging on the water side, we recommend a vertical installation as shown in figure above.

How to avoid material stress

All units – without support – should be fitted with a clamp around the cooler. Some larger units are should be fitted with additional fixing screws on the connection side. However, never mount the cooler using only these screws!

Never install the cooler in a rigid frame. Use hydraulic hoses for soft and flexible installation. All tubing should be made to minimise stress and vibration. In a hydraulic system, where the cooler is connected on the return line, use flexible hoses to minimize pulsations and if necessary fit a by-pass valve on the oil inlet to avoid overpressure from static loads.

Signs of clogging

To establish clogging, check water inlet and outlet temperatures. Clogging will reduce heat transfer

Bitte beachten Sie für die Installation der Oiltech PWO Öl/Wasser Wärmetauscher folgende Hinweise.

Anschlüsse für den Öl- und Wasserkreislauf

Standard PWO Öl/Wasser Wärmetauscher:

Die Anschlüsse für den Ölkreis sind immer grösser als die Anschlüsse des Wasserkreislaufes.

Ölaustritt erfolgt am oberen linken Gewindeanschluss (F1).

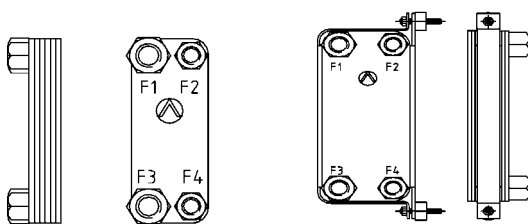
Wassereintritt erfolgt am oberen rechten Gewindeanschluss (F2).

Öleintritt erfolgt am unteren linken Gewindeanschluss (F3).

Wasseraustritt erfolgt am unteren rechten Gewindeanschluss (F4).

Bitte beachten Sie, dass bei den PWO B56 F4, F2 die Ölanschlüsse, F1, F3 die Wasseranschlüsse sind.

Verwenden Sie einen Filter, um Ablagerungen zu vermeiden. Partikel bis zu 1 mm Durchmesser bereiten normalerweise keine Probleme.



Montage

Der PWO Wärmetauscher kann in jeder Lage eingebaut werden. Es ist jedoch darauf zu achten, dass beide Kammern gegebenenfalls einwandfrei entleert werden können. Um die Verstopfungsgefahr der Wasserkanäle zu verringern, ist es von Vorteil den PWO Wärmetauscher vertikal zu montieren. Siehe Abbildung.

Vermeiden von Ermüdungsbrüchen

Alle Wärmetauscher ohne Füsse müssen mit einer Halterung seitlich befestigt werden. Einige grössere Einheiten sind auch mit Stehbolzen auf der Anschlussseite ausgerüstet. Niemals den Wärmetauscher nur mit diesen Stehbolzen befestigen.

Um Ermüdungsbrüche an den Anschlussstellen wirksam zu verhindern, empfehlen wir Schläuche

einzusetzen. Bei der Installation eines Wärmetauschers in der Rücklaufleitung, sollte ein Umgebungsventil eingesetzt werden, um eventuell auftretende Druckspitzen auffangen zu können. Der Anschluss des Wärmetauschers sollte grundsätzlich mit Schläuchen vorgenommen werden, um Spannungen in der Anschlussplatte zu vermeiden.

Primäre Gründe für Ablagerungen

Ein Zeichen dafür, dass Ablagerungen vorhanden sind, ist, wenn eine unüblich grosse Wassertemperaturdifferenz zwischen Eingang und Ausgang des Wärmetauschers gemessen wird. Ablagerungen schränken die Wärmeübertragungskapazität ein, verursachen einen erhöhten Wasserverbrauch und eine Reduzierung der Kühlleistung.

Eine weitere Möglichkeit zur Feststellung von Ablagerungen ist die Messung des Druckabfalles über den Wärmetauscher. Ablagerungen erhöhen die Geschwindigkeit und den Druckabfall. In beiden Fällen müssen die spezifizierten Durchflussmengen von Wasser und Öl gemessen werden. Jede Abweichung des Durchflusses beeinflussen die Temperaturen und den Druckabfall.

Reinigung

Nahezu alle weichen Ablagerungen können durch Rückspülen mit Wasser entgegen der normalen Wasserdurchflussrichtung entfernt werden. Bei starker Ablagerung verwenden Sie 5%-ige Phosphorsäure oder für häufige Reinigungen 5%-ige Oxalsäure oder ähnlich weiche organische Säuren. Spülen Sie in jedem Fall nach einer Säurebehandlung den Wärmetauscher ausreichend mit Wasser. Warten Sie mit der Reinigung nicht bis der Kühler verstopft ist.

Werkstoff AISI 316. Maximale Betriebsdruck: 31 bar. Maximale Betriebstemperatur: 185°C.

Um die Dichtheit zu prüfen, wird vor Auslieferung jeder PWO Öl/Wasser Wärmetauscher einer Druckprobe von 47 bar unterzogen.

Lire attentivement ces instructions avant installer l'échangeur eau/huile PWO.

Branchement des entrées et sorties d'huile et d'eau

Pour l'échangeur PWO standard:

Les diamètres des raccords d'huile sont toujours supérieurs à ceux des raccords d'eau.

L'entrée d'huile doit être branchée sur le raccord gauche inférieur (F3).

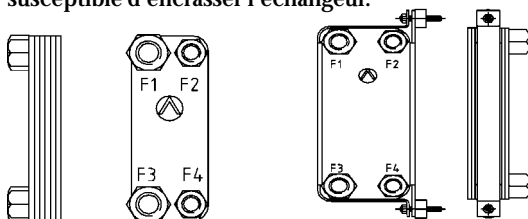
La sortie d'huile doit être branchée sur le raccord gauche supérieur (F1).

L'entrée eau doit être branchée sur le raccord droit supérieur (F2).

La sortie d'eau doit être branchée sur le raccord droit inférieur (F4).

NB: Les raccordements eau/huile sont inversés sur le modèle PWO B56.

Utiliser des filtres lorsque le fluide transporte des particules supérieures à 1 mm de diamètre susceptible d'encrasser l'échangeur.



Positionnement

L'échangeur PWO peut être monté dans toutes les positions, tout en tenant compte de la vidange éventuelle des circuits. Pour éviter tout encrassement côté eau, monter l'échangeur verticalement selon les instructions ci-dessus.

Comment éviter toute fatigue mécanique

Tous les échangeurs – sans support – se montent à l'aide d'une bride placée autour du corps. Pour les échangeurs de grande capacité en complément des brides, des goudjons sont prévus. Ces goudjons sont situés sur la face de raccordement. L'échangeur ne doit pas être uniquement supporté par ces goudjons! Ne pas monter l'échangeur sur un châssis rigide. Utiliser le système Armaflex ou tout autre support élastique similaire. Tous les raccordements doivent être réalisés de sorte que le niveau de vibration soit minimum. Pour des circuits hydrauliques où l'échangeur est relié au retour au réservoir, utiliser des tuyauteries souples pour réduire les pulsations et éventuellement un clapet by-pass sur l'entrée d'huile pour éviter toute surpression.

Facteurs d'encrassement

L'encrassement se détermine en contrôlant la température d'eau en entrée et sortie de l'échangeur. L'encrassement réduit le transfert thermique, ce qui se traduit par une consommation d'eau élevée, des différences de température d'eau inférieures aux valeurs spécifiées et une température d'huile élevée. Une autre manière de déterminer l'encrassement consiste à mesurer la perte de pression à travers l'échangeur. Etant donné que l'encrassement diminue la section de passage et, par conséquent, augmente la vitesse d'écoulement, ceci se traduira par une perte de pression plus importante. Avant d'utiliser ces méthodes, s'assurer que le débit d'eau est égal au débit spécifié. Un débit d'eau différent aura naturellement un effet sur la température et la perte de pression.

Nettoyage

Un rinçage à contrecourant à l'aide d'eau permettra l'élimination de la plupart des dépôts. Si l'encrassement consiste en des dépôts consistants, faire circuler un acide peu agressif à travers l'échangeur. Utiliser 5% acide phosphorique - 5% acide oxalique nettoyage fréquent - ou de tout autre acide organique faible. Ensuite, rincer à grande eau afin d'éliminer toute trace d'acide avant d'utiliser à nouveau le système. Ne jamais attendre l'encrassement complet de l'échangeur pour procéder au nettoyage.

Matériaux AISI 316. Pression de travail maximale: 31 bar. Température maximale de travail: 185°C. Tous les échangeurs PWO sont soumis à des tests d'épreuves à 47 bar avant livraison.