

April 9, 2018

File No. 0115-031-00

Mr. Chris Houston

Associated Engineering (Sask.) Ltd.
203 - Number Five Donald Street
Winnipeg, MB
R3L 2T4

**RE Brandon AAFC Research Centre – Watermain Upgrades and Extension
Geotechnical Investigation Report**

As requested by Associated Engineering (AE), TREK Geotechnical Inc. (TREK) has completed a geotechnical investigation for new watermain at the AAFC Brandon Research Centre located at 2701 Grand Valley Road, in Brandon, MB. The terms of reference for the investigation are included in our proposal addressed to Mr. Chris Houston of Associated Engineering (AE), dated March 2, 2018. TREK's scope of work includes a sub-surface investigation, laboratory testing, and the provision of recommendations for design and construction of the watermain.

Background Information

Two new watermain at the facility are planned for construction at the site including a new 300 mm diameter line from 18th Street and a new 250 mm diameter extension to an existing watermain at Braecrest Drive. Overall, approximately 2.5 km of new watermain are planned at the site to service the facility. The water lines will consist of PVC pipe and will be buried 3 m below ground surface.

Field Program*Sub-Surface Investigation*

A sub-surface investigation was completed on March 23, 2018 under the supervision of TREK personnel to determine the soil stratigraphy and groundwater conditions at the site. Six test pits (TP18-01 to 06) were excavated to depths ranging between 2.4 and 5.2 m below ground surface using a Kobelco 260sk, track-mounted excavator equipped with a 0.6 m wide bucket. The test pits were backfilled with the excavated material and compacted with the excavator bucket. TP18-01 was discontinued at 2.4 m depth after an unknown line was exposed; it did not appear as though the line was damaged and a representative form AAFC was informed.

Sub-surface soils observed during excavation were visually classified based on the Unified Soil Classification System (USCS). Disturbed grab samples were retrieved from the bucket during

excavation at regular intervals and a relatively undisturbed Shelby tube sample was obtained. All samples retrieved during excavation were transported to TREK's soils laboratory in Winnipeg, MB for further testing and classification. Laboratory testing consisted of water content determination on all samples, as well as bulk unit weight measurements and unconfined compression testing on the Shelby tube sample. Grain size distribution, Atterberg limits, and acidity, resistivity, and water-soluble sulphate testing were also completed on select samples.

The test pit locations were selected by AE prior to the investigation and were located in the field using a handheld GPS. TP18-04 to 06 were relocated to avoid conflict with buried utility lines. The actual test pit locations are shown the Test Pit Location Plan (Figure 01) and UTM coordinates are provided on the test pit logs. Test pit elevations were not recorded. Test pit logs are attached which describe the soil units encountered and other pertinent information such as groundwater conditions and a summary of the laboratory testing results. Laboratory testing results are also attached to this letter.

Soil Stratigraphy

A brief description of the soil units encountered during test pit excavation is provided below. All interpretations of soil stratigraphy for the purposes of design should refer to the detailed information provided on the attached test pit logs.

The soil stratigraphy in TP18-02 to 04 generally consists of loose, poorly graded, fine to coarse-grained sand extending to the depth of exploration (4.6 m below ground surface). In TP18-05 and 06, the stratigraphy consists of clay extending to depths of 4.3 and 3.8 m below ground surface. The upper 1.5 m of the clay contains organics and is stiff, moist, and of intermediate plasticity. Below 1.5 m, the clay is free of organics, stiff to very stiff, dry to moist, and of high plasticity. Loose, poorly graded, coarse-grained sand to coarse-grained gravel is present below the clay in TP18-05 and extends to the depth of exploration of 4.6 m below ground surface. Loose, poorly graded, fine to coarse-grained sand is present below the clay in TP18-06 and extends to the depth of exploration of 5.2 m below ground surface. In TP18-01, loose, poorly graded, fine-grained sand fill was encountered to the depth of exploration at 2.4 m below ground surface.

Groundwater Conditions

Seepage was encountered in TP18-01 and 05 at respective depths of 0.6 and 4.3 m below ground surface. Less than 100 mm of water accumulated at the bottom of these test pits immediately after excavation was completed. Sloughing and/or caving were observed below a depth of 3.4 and 3.7 m in TP18-03 and 06. These test pits remained open to depths of 4 and 4.9 m immediately after completion of test pitting.

These observations are short-term and should not be considered reflective of (static) groundwater levels at the site which would require monitoring over an extended period of time to determine. It is important to recognize that groundwater conditions may vary seasonally, annually, or as a result of construction activities.

Recommendations

Temporary Excavations and Shoring

Excavations for the proposed watermain trenches are anticipated to extend approximately 3 m below the existing ground surface. Slope stability analyses were conducted to provide recommendations for slope geometry of temporary, open-cut excavations to this depth. The analyses were conducted using a limit-equilibrium slope stability model (Slope/W) from the GeoStudio 2016 software package (Geo-Slope International Ltd.) using the Morgenstern-Price method of slices to calculate factors of safety (FS) of theoretical slip surfaces identified using a grid and radius slip surface method. A static piezometric line at 3 m depth was assumed to represent groundwater levels.

The analysis was performed assuming two cases, including, 1) and an excavation entirely in stiff clay, and 2) an excavation entirely in loose sand. Effective stress shear strength parameters were assumed in the analysis and selected based on our observations and experience with similar soils. These parameters are summarized in Table 01. In order to maintain a minimum safety factor of 1.3 (considered an acceptable target for temporary excavations), open-cut excavations should be sloped at 2H:1V (2horizontal:1vertical) or flatter to 3 m depth. Slope stability outputs for each case are attached. TREK should be contacted to revise our analyses if open-cut excavations greater than 3 m deep are required.

Table 01. Soil Properties used in the Stability Analysis

| Soil Description | Unit Weight (kN/m ³) | Cohesion (kPa) | Friction Angle (degrees) |
|------------------|----------------------------------|----------------|--------------------------|
| Sand | 18 | 0 | 30 |
| Clay | 17.5 | 5 | 17 |

Maintaining the stability of the excavation slopes for the duration of construction should be the responsibility of the Contractor. Stockpiles of excavated material and heavy equipment should be kept away from the edge of the excavation by a distance equal to or greater than the depth of excavation. Dewatering measures should be completed as necessary to maintain a dry excavation and permit proper completion of the work. If seepage is encountered, it should be directed to a sump pit and pumped out of the excavation. If saturated sands are encountered, shoring or slope flattening may be required. To prevent wet sands from entering the excavation, gravel buttressing could be used in conjunction with sump pits for dewatering. Surface water should be diverted away from the excavation and the excavation should be backfilled as soon as possible following construction

If temporary shoring is necessary due to space constraints, cantilevered walls will be required to support the excavations. Table 02, provides the recommended earth pressure coefficients and bulk unit weights for the clay and sand layers for calculation of lateral earth pressures. Surcharge loads

(if present) and hydrostatic water pressure (assuming a groundwater level at 3 m below ground surface) should be incorporated into the design of cantilevered walls, as well as an adequate factor of safety against instability.

Table 02 Earth Pressure Coefficients

| Design Parameter | Earth Pressure Coefficients and Bulk Unit Weights | |
|-------------------------------|---------------------------------------------------|------|
| | SAND | CLAY |
| Active (K_a) | 0.3 | 0.5 |
| At-rest (K_0) | 0.5 | 0.7 |
| Passive (K_p) | 3.0 | 2.0 |
| Bulk Unit Weight (kN/m^3) | 18 | 17 |

A certain amount of ground movement behind the shoring will occur and is largely unavoidable. The amount of movement that will occur cannot be accurately predicted, mainly because the movement is as much a function of installation procedures and workmanship as it is a function of theoretical considerations. It is anticipated that the design of temporary shoring will be the responsibility of the Contractor. Once the proposed shoring design is complete, it should be reviewed by TREK prior to construction to ensure the design is appropriate and to assess the need for groundwater control. Performance of the excavation system should be monitored from the onset of installation to removal of the shoring system.

Concrete

Buried concrete structures should be designed in accordance with CSA A23.1-14 (Concrete Materials and Methods of Construction). Water soluble sulphate (SO_4) testing was completed on two samples to assess the degree of exposure for concrete subjected to sulphate attack and the results are presented in Table 02.

Table 02. Water Soluble Sulphate Testing Results

| Test Hole ID | Sample Depth | Sample ID | Soil Type | Water Soluble Sulphate |
|--------------|--------------|-----------|-----------|------------------------|
| TP18-02 | 2.7 to 2.9 m | G05 | Sand | <0.010 % |
| TP18-06 | 2.1 to 2.7 m | T21 | Clay | <0.010 % |

Based on these results, the degree of exposure for concrete subjected to sulphate attack is considered negligible as per Table 3, CSA A23.1-14 (Concrete Materials and Methods of Concrete Construction). Concrete that may be exposed to freezing and thawing should be adequately air entrained to improve freeze-thaw durability in accordance with Table 4, CSA A23.1-14.

Acidity, and Resistivity Testing

Soil samples have been submitted for acidity and resistivity testing. The testing had not been completed at the time of this letter. When the testing is complete, TREK will issue an addendum with the results and requirements for sulphate resistant cement for buried concrete structures.

Watermain Construction

Construction of the new watermain should follow City of Brandon Standard Construction Specifications Section No. 02660 *Watermains* and Section No. 02210 *Excavation, Bedding & Backfill* with the following supplemental recommendations:

1. The sub-grade (i.e. watermain foundation) should be free of organics, fill materials, and any other deleterious material such that it consists of undisturbed, native soil.
2. The sub-grade should be protected from freezing, drying, or inundation with water at all times. If any of these conditions occur, the sub-grade should be scarified, moisture conditioned as appropriate, and re-compacted to a minimum of 95% of the Standard Proctor Maximum Dry Density.

Frost related movements are not anticipated to be a factor for design since the watermains are to be installed to a depth of 3 m below ground surface, which is deeper than the anticipated maximum depth of frost penetration (2.5 m) for the area. The watermains can be placed above the depth of frost penetration (if required) provided insulation (e.g. Styrofoam Highload) is incorporated into the design to provide an equivalent frost protection depth of 2.5 m. TREK should be contacted to review the insulation design prior to construction to confirm it is adequate to reduce frost penetration to the intended depth.

CLOSURE

The geotechnical information provided in this report is in accordance with current engineering principles and practices (Standard of Practice). The findings of this report were based on information provided (field investigation and laboratory testing). Soil conditions are natural deposits that can be highly variable across a site. If subsurface conditions are different than the conditions previously encountered on-site or those presented here, we should be notified to adjust our findings if necessary.

All information provided in this report is subject to our standard terms and conditions for engineering services, a copy of which is provided to each of our clients with the original scope of work or standard engineering services agreement. If these conditions are not attached, and you are not already in possession of such terms and conditions, contact our office and you will be promptly provided with a copy.

This report has been prepared by TREK Geotechnical Inc. (the Consultant) for the exclusive use of the Associated Engineering Ltd. (the Client) and their agents for the work product presented in the report. Any findings or recommendations provided in this report are not to be used or relied upon by any third parties, except as agreed to in writing by the Client and Consultant prior to use.

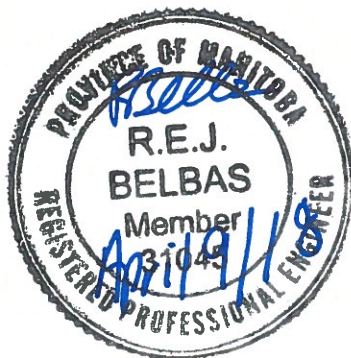
If you have any questions or require any additional information, please contact the undersigned.

Kind Regards,

TREK Geotechnical Inc.

Per:

Reviewed By:



Ryan Belbas, M.Sc., P.Eng.
Geotechnical Engineer



Kent Bannister, M.Sc., P.Eng.
Senior Geotechnical Engineer

Attach.



Figure

ANSI full bleed B (11.00 x 17.00 inches)

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Figure 01
Test Pit Plan

Test Pit Logs

GENERAL NOTES

- Classifications are based on the United Soil Classification System and include consistency, moisture, and color. Field descriptions have been modified to reflect results of laboratory tests where deemed appropriate.
- Descriptions on these test hole logs apply only at the specific test hole locations and at the time the test holes were drilled. Variability of soil and groundwater conditions may exist between test hole locations.
- When the following classification terms are used in this report or test hole logs, the primary and secondary soil fractions may be visually estimated.

| Major Divisions | | USCS Classification | Symbols | Typical Names | Laboratory Classification Criteria | | Particle Size | | Material | | | |
|-----------------------------------------------------------------------------------------|-----------------------------------------------------------------------|--------------------------------------|---------|---------------|--------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------|------------------|--------------------------------------------------|-------------------------------|---------------------------------------------------|--|
| Coarse-Grained soils (More than half the material is larger than No. 200 sieve size) | Gravels (More than half of coarse fraction is larger than 4.75 mm) | Clean gravel (Little or no fines) | GW | | Well-graded gravels, gravel-sand mixtures, little or no fines | Determine percentages of sand and gravel from grain size curve, depending on percentage of fines (fraction smaller than No. 200 sieve) coarse-grained soils are classified as follows: Less than 5 percent..... GW, GP, SW, SP More than 12 percent..... GM, GC, SM, SC 6 to 12 percent..... Borderline cases requiring dual symbols* C _u = $\frac{D_{60}}{D_{10}}$ greater than 4; C _c = $\frac{(D_{30})^2}{D_{10} \times D_{60}}$ between 1 and 3 Not meeting all gradation requirements for GW Atterberg limits below "A" line or P.I. less than 4 Above "A" line with P.I. between 4 and 7 are borderline cases requiring use of dual symbols Atterberg limits above "A" line or P.I. greater than 7 C _u = $\frac{D_{60}}{D_{10}}$ greater than 6; C _c = $\frac{(D_{30})^2}{D_{10} \times D_{60}}$ between 1 and 3 Not meeting all gradation requirements for SW Atterberg limits below "A" line or P.I. less than 4 Above "A" line with P.I. between 4 and 7 are borderline cases requiring use of dual symbols Atterberg limits above "A" line or P.I. greater than 7 | mm | ASTM Sieve sizes | #10 to #4 #40 to #10 #200 to #40 < #200 | | | |
| | | | GP | | Poorly-graded gravels, gravel-sand mixtures, little or no fines | | | | | | | |
| | | | GM | | Silty gravels, gravel-sand-silt mixtures | | | | | | | |
| | | | GC | | Clayey gravels, gravel-sand-silt mixtures | | | | | | | |
| | Sands (More than half of coarse fraction is smaller than 4.75 mm) | Clean sands (Little or no fines) | SW | | Well-graded sands, gravelly sands, little or no fines | | | | | | | |
| | | | SP | | Poorly-graded sands, gravelly sands, little or no fines | | | | | | | |
| | | | SM | | Silty sands, sand-silt mixtures | | | | | | | |
| | | | SC | | Clayey sands, sand-clay mixtures | | | | | | | |
| Fine-Grained soils (More than half the material is smaller than No. 200 sieve size) | Silts and Clays (Liquid limit less than 50) | | ML | | Inorganic silts and very fine sands, rock floor, silty or clayey fine sands or clayey silts with slight plasticity | | mm | ASTM Sieve Sizes | Boulders Cobbles Gravel Coarse Fine | | | |
| | | | CL | | Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays | | | | | | | |
| | | | OL | | Organic silts and organic silty clays of low plasticity | | | | | | | |
| | Silts and Clays (Liquid limit greater than 50) | | MH | | Inorganic silts, micaceous or distomaceous fine sandy or silty soils, organic silts | | | | | | | |
| | | | CH | | Inorganic clays of high plasticity, fat clays | | | | | | | |
| | | | OH | | Organic clays of medium to high plasticity, organic silts | | | | | | | |
| | Highly Organic Soils | | Pt | | Peat and other highly organic soils | | | | | Von Post Classification Limit | Strong colour or odour, and often fibrous texture | |

LEGEND OF ABBREVIATIONS AND SYMBOLS

| | |
|---------------------------------|-------------------------------------------------------------|
| LL - Liquid Limit (%) | ▽ Water Level at Time of Drilling |
| PL - Plastic Limit (%) | ▼ Water Level at End of Drilling |
| PI - Plasticity Index (%) | ▽ Water Level After Drilling as Indicated on Test Hole Logs |
| MC - Moisture Content (%) | |
| SPT - Standard Penetration Test | |
| RQD- Rock Quality Designation | |
| Qu - Unconfined Compression | |
| Su - Undrained Shear Strength | |
| VW - Vibrating Wire Piezometer | |
| SI - Slope Inclinator | |

FRACTION OF SECONDARY SOIL CONSTITUENTS ARE BASED ON THE FOLLOWING TERMINOLOGY

| TERM | EXAMPLES | PERCENTAGE |
|-------------|---------------|------------------|
| and | and CLAY | 35 to 50 percent |
| "y" or "ey" | clayey, silty | 20 to 35 percent |
| some | some silt | 10 to 20 percent |
| trace | trace gravel | 1 to 10 percent |

TERMS DESCRIBING CONSISTENCY OR COMPACTION CONDITION

The Standard Penetration Test blow count (N) of a non-cohesive soil can be related to compactness condition as follows:

| <u>Descriptive Terms</u> | <u>SPT (N) (Blows/300 mm)</u> |
|--------------------------|-------------------------------|
| Very loose | < 4 |
| Loose | 4 to 10 |
| Compact | 10 to 30 |
| Dense | 30 to 50 |
| Very dense | > 50 |

The Standard Penetration Test blow count (N) of a cohesive soil can be related to its consistency as follows:

| <u>Descriptive Terms</u> | <u>SPT (N) (Blows/300 mm)</u> |
|--------------------------|-------------------------------|
| Very soft | < 2 |
| Soft | 2 to 4 |
| Firm | 4 to 8 |
| Stiff | 8 to 15 |
| Very stiff | 15 to 30 |
| Hard | > 30 |

The undrained shear strength (Su) of a cohesive soil can be related to its consistency as follows:

| <u>Descriptive Terms</u> | <u>Undrained Shear Strength (kPa)</u> |
|--------------------------|---------------------------------------|
| Very soft | < 12 |
| Soft | 12 to 25 |
| Firm | 25 to 50 |
| Stiff | 50 to 100 |
| Very stiff | 100 to 200 |
| Hard | > 200 |



Sub-Surface Log

Test Pit TP18-01

1 of 1

Client: Associated Engineering (Sask.) Ltd. **Project Number:** 0115-031-00
Project Name: Brandon AAFC Research Centre Watermain Upgrades **Location:** UTM N-5524698, E-429645
Contractor: AW Group **Ground Elevation:** Not Measured
Method: Kobelco SK260 Excavator **Date Drilled:** 23 March 2018

| Sample Type: | | Particle Size Legend: | | Sample Type | | Sample Number | RQD (%) | SPT (N) | Bulk Unit Wt (kN/m ³) | | Undrained Shear Strength (kPa) | |
|--------------|-------------|-------------------------------------------------------|--|-------------|--|---------------|---------|---------|-----------------------------------|--|--------------------------------|--|
| | | | | | | | | | | | | |
| Depth (m) | Soil Symbol | MATERIAL DESCRIPTION | | | | | | | Particle Size (%) | | Test Type | |
| | | | | | | | | | | | | |
| | | TOPSOIL (ORGANICS) | | | | | | | | | | |
| | | SAND (FILL) - silty, trace to some gravel, trace clay | | | | | | | | | | |
| | | - light brown | | | | | | | | | | |
| | | - dry to moist, loose to compact | | | | | | | | | | |
| | | - poorly graded, fine-grained | | | | | | | | | | |
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











Sub-Surface Log

Test Pit TP18-02

1 of 1

Client: Associated Engineering (Sask.) Ltd. Project Number: 0115-031-00
Project Name: Brandon AAFC Research Centre Watermain Upgrades Location: UTM N-5524760, E-429997
Contractor: AW Group Ground Elevation: Not Measured
Method: Kobelco SK260 Excavator Date Drilled: 23 March 2018

| Sample Type: | |  Grab (G) |  Shelby Tube (T) |  Split Spoon (SS) |  Split Barrel (SB) |  Core (C) | | | |
|-----------------------|------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------|------------------------------------------------------------|
| Particle Size Legend: | |  Fines |  Clay |  Silt |  Sand |  Gravel |  Cobbles |  Boulders | |
| Depth (m) | Soil Symbol | MATERIAL DESCRIPTION | Sample Type | Sample Number | RQD (%) | SPT (N) |  Bulk Unit Wt (kN/m ³) | Undrained Shear Strength (kPa) | |
| | | | | | | | Particle Size (%) | | Test Type |
| | | | | | | | 0 20 40 60 80 100 | | △ Torvane △ ✦ Pocket Pen. ✦ ☒ Qu ☒ ○ Field Vane ○ |
| | | | | | | | 0 20 40 60 80 100 | | 0 50 100 150 200 250 |
| 0.0 |  | TOPSOIL (ORGANICS) - grasses, rootlets |  | G03 | | | | | |
| 0.5 |  | SAND - trace clay, trace silt, trace gravel - light brown - dry to moist, loose to compact - poorly graded, fine to medium-grained | | | | | | | |
| 1.0 | | | | | | | | | |
| 1.5 |  | |  | G04 | | |  | | |
| 2.0 | | | | | | | | | |
| 2.5 | | | | | | | | | |
| 3.0 | | - fine to coarse-grained sand below 2.7 m |  | G05 | | |  | | |
| 3.5 | | | | | | | | | |
| 4.0 | | - moist below 3.7 m | | | | | | | |
| 4.5 | | |  | G06 | | |  | | |

END OF TEST PIT AT 4.6 m IN SAND

Notes:

- 1) No sloughing or seepage observed.
- 2) Test pit open to 2.4 m and dry immediately after completion of excavation.
- 3) Test pit backfilled with excavated material and tamped with bucket to ground surface.

Logged By: Jenna Roadley Reviewed By: Kent Bannister Project Engineer: Ryan Belbas



Sub-Surface Log

Test Pit TP18-03

1 of 1

Client: Associated Engineering (Sask.) Ltd. **Project Number:** 0115-031-00
Project Name: Brandon AAFC Research Centre Watermain Upgrades **Location:** UTM N-5524791, E-430349
Contractor: AW Group **Ground Elevation:** Not Measured
Method: Kobelco SK260 Excavator **Date Drilled:** 23 March 2018

| Sample Type: | | Particle Size Legend: | | Sample Type: | | Sample Number | | RQD (%) | | SPT (N) | | Bulk Unit Wt (kN/m ³) | | Undrained Shear Strength (kPa) | |
|--------------|--|-----------------------|--|--------------|--|---------------|--|---------|--|---------|--|-----------------------------------|--|--------------------------------|--|
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END OF TEST PIT AT 4.6 m IN SAND

Notes:

- 1) Sloughing observed below 3.4 m.
- 2) No seepage observed.
- 2) Test pit open to 4.0 m and dry immediately after completion of excavation.
- 3) Test pit backfilled with excavated material and tamped with bucket to ground surface.

Logged By: Jenna Roadley **Reviewed By:** Kent Bannister **Project Engineer:** Ryan Belbas



Sub-Surface Log

Test Pit TP18-04

1 of 1

Client: Associated Engineering (Sask.) Ltd. Project Number: 0115-031-00
Project Name: Brandon AAFC Research Centre Watermain Upgrades Location: UTM N-5524436, E-430675
Contractor: AW Group Ground Elevation: Not Measured
Method: Kobelco SK260 Excavator Date Drilled: 23 March 2018

| Sample Type: | | Particle Size Legend: | | Sample Type | | RQD (%) | SPT (N) | Bulk Unit Wt (kN/m³) | | Undrained Shear Strength (kPa) | |
|--------------|--|-----------------------|--|-------------|--|---------|---------|----------------------|--|--------------------------------|--|
| | | | | | | | | Particle Size (%) | | Test Type | |
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Sub-Surface Log

Test Pit TP18-06

1 of 1

Client: Associated Engineering (Sask.) Ltd. Project Number: 0115-031-00
Project Name: Brandon AAFC Research Centre Watermain Upgrades Location: UTM N-5524452, E-429702
Contractor: AW Group Ground Elevation: Not Measured
Method: Kobelco SK260 Excavator Date Drilled: 23 March 2018

Sample Type: ☒ Grab (G) ☐ Shelby Tube (T) ☐ Split Spoon (SS) ☐ Split Barrel (SB) ☐ Core (C)

Particle Size Legend: ☒ Fines ☒ Clay ☐ Silt ☐ Sand ☐ Gravel ☐ Cobbles ☐ Boulders

| Depth (m) | Soil Symbol | MATERIAL DESCRIPTION | Sample Type | Sample Number | RQD (%) | SPT (N) | Bulk Unit Wt (kN/m ³) | | Particle Size (%) | | Undrained Shear Strength (kPa) | |
|-----------|-------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------|---------------|---------|---------|-----------------------------------|----|-------------------|----|-------------------------------------------------------------------------|----|
| | | | | | | | 16 | 17 | 18 | 19 | 20 | 21 |
| | | | | | | | 0 20 40 60 80 100 | | 0 20 40 60 80 100 | | 0 50 100 150 200 250 | |
| | | | | | | | PL MC LL | | | | Test Type △ Torvane △ ✱ Pocket Pen. ✱ ☒ Qu ☒ ○ Field Vane ○ | |
| 0.5 | | CLAY - silty, trace sand, trace organics - dark grey - frozen to 1.5 m, moist and stiff when thawed - intermediate plasticity | | G19 | | | | | | | | |
| 1.5 | | CLAY - silty, trace sand, trace oxidation - brown - dry to moist, very stiff - high plasticity - blocky | | G20 | | | | | | | | |
| 2.5 | | | | T21 | | | | | | | | |
| 3.0 | | | | G22 | | | | | | | | |
| 4.0 | | SAND - trace clay, trace silt, trace to some gravel - light brown - dry to moist, loose - poorly graded, fine to coarse-grained - moist below 4.3 m | | G23 | | | | | | | | |
| 5.0 | | | | G24 | | | | | | | | |

END OF TEST PIT AT 5.2 m IN SAND

Notes:

- 1) No seepage observed.
- 2) Caving observed below 3.7 m depth.
- 3) Test pit open to 4.9 m and dry immediately after completion of excavation.
- 3) Test pit backfilled with excavated material and tamped with bucket to ground surface.

Logged By: Jenna Roadley Reviewed By: Kent Bannister Project Engineer: Ryan Belbas

Laboratory Testing Results

ALS ENVIRONMENTAL ANALYTICAL REPORT

| Sample Details/Parameters | | Result | Qualifier* | D.L. | Units | Extracted | Analyzed | Batch |
|---------------------------------|-----------------------|--------|------------|-------|-------|-----------|-----------|----------|
| L2073943-1 | TP18-02 G05 (9'-9.5') | | | | | | | |
| Sampled By: CLIENT on 23-MAR-18 | | | | | | | | |
| Matrix: GRAB-SOIL | | | | | | | | |
| Miscellaneous Parameters | | | | | | | | |
| Water Soluble Sulfate | | <0.010 | | 0.010 | % | 06-APR-18 | 06-APR-18 | R4005984 |
| L2073943-2 | TP18-06 T21 (7'-9') | | | | | | | |
| Sampled By: CLIENT on 23-MAR-18 | | | | | | | | |
| Matrix: GRAB-SOIL | | | | | | | | |
| Miscellaneous Parameters | | | | | | | | |
| Water Soluble Sulfate | | 0.016 | | 0.010 | % | 06-APR-18 | 06-APR-18 | R4005984 |
| | | | | | | | | |

* Refer to Referenced Information for Qualifiers (if any) and Methodology.



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Moisture Content Report ASTM D2216-10

Project No. 0115-031-00
Client Associated Engineering (Sask.) Ltd.
Project Brandon AAFC Research Centre Waterline

Sample Date 23-Mar-18
Test Date 27-Mar-18
Technician EH

| Test Pit | TP18-01 | TP18-01 | TP18-02 | TP18-02 | TP18-02 | TP18-02 |
|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|
| Depth (m) | 0.3 - 0.5 | 1.5 - 1.7 | 0.2 - 0.3 | 1.4 - 1.5 | 2.7 - 2.9 | 4.3 - 4.4 |
| Sample # | G01 | G02 | G03 | G04 | G05 | G06 |
| Tare ID | E27 | N52 | C12 | AC17 | N106 | A109 |
| Mass of tare | 8.6 | 8.6 | 8.4 | 6.6 | 8.4 | 8.4 |
| Mass wet + tare | 263.0 | 265.0 | 229.2 | 369.4 | 219.2 | 195.0 |
| Mass dry + tare | 233.4 | 227.0 | 146.8 | 348.8 | 210.2 | 183.4 |
| Mass water | 29.6 | 38.0 | 82.4 | 20.6 | 9.0 | 11.6 |
| Mass dry soil | 224.8 | 218.4 | 138.4 | 342.2 | 201.8 | 175.0 |
| Moisture % | 13.2% | 17.4% | 59.5% | 6.0% | 4.5% | 6.6% |

| Test Pit | TP18-03 | TP18-03 | TP18-03 | TP18-03 | TP18-04 | TP18-04 |
|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|
| Depth (m) | 0.3 - 0.5 | 1.1 - 1.2 | 2.6 - 2.7 | 4.1 - 4.3 | 0.5 - 0.6 | 1.7 - 1.8 |
| Sample # | G07 | G08 | G09 | G10 | G15 | G16 |
| Tare ID | Z52 | W54 | AB73 | K32 | N22 | D19 |
| Mass of tare | 8.4 | 8.4 | 6.6 | 8.6 | 8.4 | 8.6 |
| Mass wet + tare | 248 | 242.8 | 315.6 | 293 | 212 | 210 |
| Mass dry + tare | 224.6 | 232.6 | 295.8 | 261.2 | 184.2 | 180.4 |
| Mass water | 23.4 | 10.2 | 19.8 | 31.8 | 27.8 | 29.6 |
| Mass dry soil | 216.2 | 224.2 | 289.2 | 252.6 | 175.8 | 171.8 |
| Moisture % | 10.8% | 4.5% | 6.8% | 12.6% | 15.8% | 17.2% |

| Test Pit | TP18-04 | TP18-04 | TP18-05 | TP18-05 | TP18-05 | TP18-05 |
|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|
| Depth (m) | 2.4 - 2.6 | 4.3 - 4.4 | 0.3 - 0.5 | 1.5 - 1.7 | 2.7 - 2.9 | 4.4 - 4.6 |
| Sample # | G17 | G18 | G11 | G12 | G13 | G14 |
| Tare ID | Z06 | D33 | N33 | F14 | N24 | P11 |
| Mass of tare | 8.4 | 8.2 | 8.4 | 8.6 | 8.6 | 8.6 |
| Mass wet + tare | 208.6 | 220.4 | 281.0 | 292.2 | 405.0 | 228.2 |
| Mass dry + tare | 192.2 | 208.2 | 216.4 | 228.0 | 306.4 | 201.4 |
| Mass water | 16.4 | 12.2 | 64.6 | 64.2 | 98.6 | 26.8 |
| Mass dry soil | 183.8 | 200.0 | 208.0 | 219.4 | 297.8 | 192.8 |
| Moisture % | 8.9% | 6.1% | 31.1% | 29.3% | 33.1% | 13.9% |



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Moisture Content Report ASTM D2216-10

Project No. 0115-031-00
Client Associated Engineering (Sask.) Ltd.
Project Brandon AAFC Research Centre Waterline

Sample Date 23-Mar-18
Test Date 27-Mar-18
Technician EH

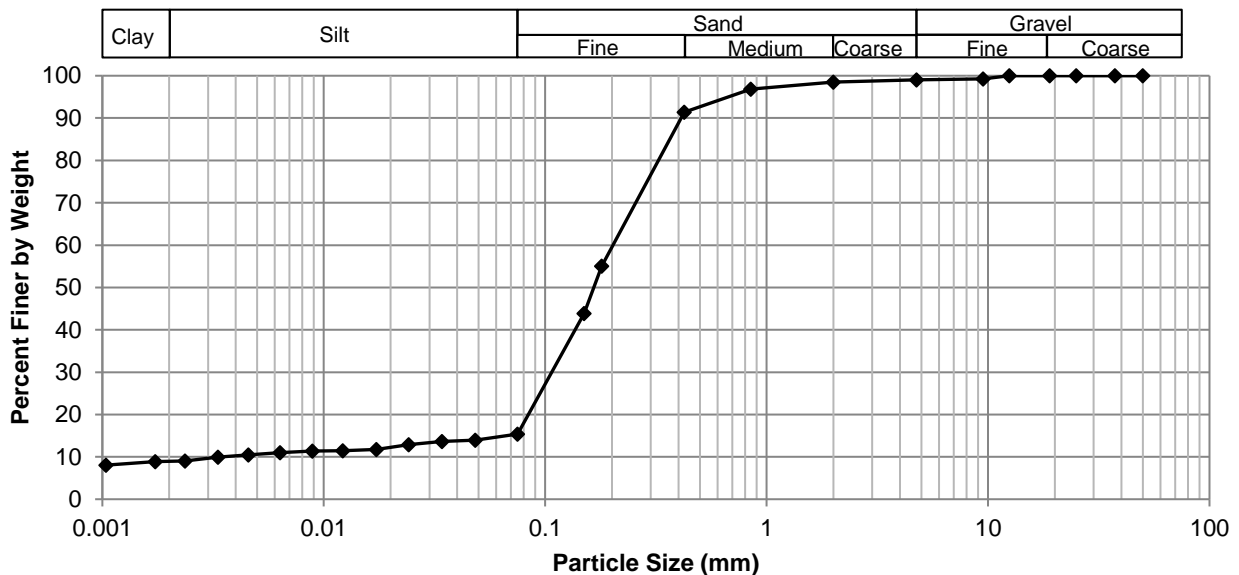
| Test Pit | TP18-06 | TP18-06 | TP18-06 | TP18-06 | TP18-06 | |
|-----------------|-----------|-----------|-----------|-----------|-----------|--|
| Depth (m) | 0.5 - 0.6 | 1.5 - 1.7 | 2.9 - 3.0 | 3.7 - 3.8 | 4.7 - 4.9 | |
| Sample # | G19 | G20 | G22 | G23 | G24 | |
| Tare ID | W96 | N25 | E103 | Z130 | W14 | |
| Mass of tare | 8.6 | 8.6 | 8.4 | 8.4 | 8.4 | |
| Mass wet + tare | 203.4 | 236.2 | 258.8 | 245.8 | 259.2 | |
| Mass dry + tare | 168.6 | 193.6 | 197.4 | 223.6 | 246.2 | |
| Mass water | 34.8 | 42.6 | 61.4 | 22.2 | 13.0 | |
| Mass dry soil | 160.0 | 185.0 | 189.0 | 215.2 | 237.8 | |
| Moisture % | 21.8% | 23.0% | 32.5% | 10.3% | 5.5% | |

Project No. 0115-031-00
Client Associated Engineering (Sask.) Ltd.
Project Brandon AAFC Research Centre Waterline

Test Hole TP18-02
Sample # G04
Depth (m) 1.4 - 1.5
Sample Date 23-Mar-18
Test Date 2-Apr-18
Technician EH

| | |
|---------------|-------|
| Gravel | 1.0% |
| Sand | 83.6% |
| Silt | 6.4% |
| Clay | 8.9% |

Particle Size Distribution Curve



| Gravel | | Sand | | Silt and Clay | |
|--------------------|-----------------|--------------------|-----------------|--------------------|-----------------|
| Particle Size (mm) | Percent Passing | Particle Size (mm) | Percent Passing | Particle Size (mm) | Percent Passing |
| 50.0 | 100.00 | 4.75 | 98.99 | 0.0750 | 15.38 |
| 37.5 | 100.00 | 2.00 | 98.50 | 0.0484 | 13.96 |
| 25.0 | 100.00 | 0.850 | 96.81 | 0.0342 | 13.65 |
| 19.0 | 100.00 | 0.425 | 91.38 | 0.0242 | 12.86 |
| 12.5 | 100.00 | 0.180 | 55.08 | 0.0173 | 11.77 |
| 9.50 | 99.23 | 0.150 | 43.84 | 0.0122 | 11.48 |
| 4.75 | 98.99 | 0.075 | 15.38 | 0.0089 | 11.35 |
| | | | | 0.0063 | 11.03 |
| | | | | 0.0046 | 10.46 |
| | | | | 0.0033 | 9.93 |
| | | | | 0.0024 | 9.04 |
| | | | | 0.0017 | 8.86 |
| | | | | 0.0010 | 8.05 |



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Atterberg Limits ASTM D4318-10e1

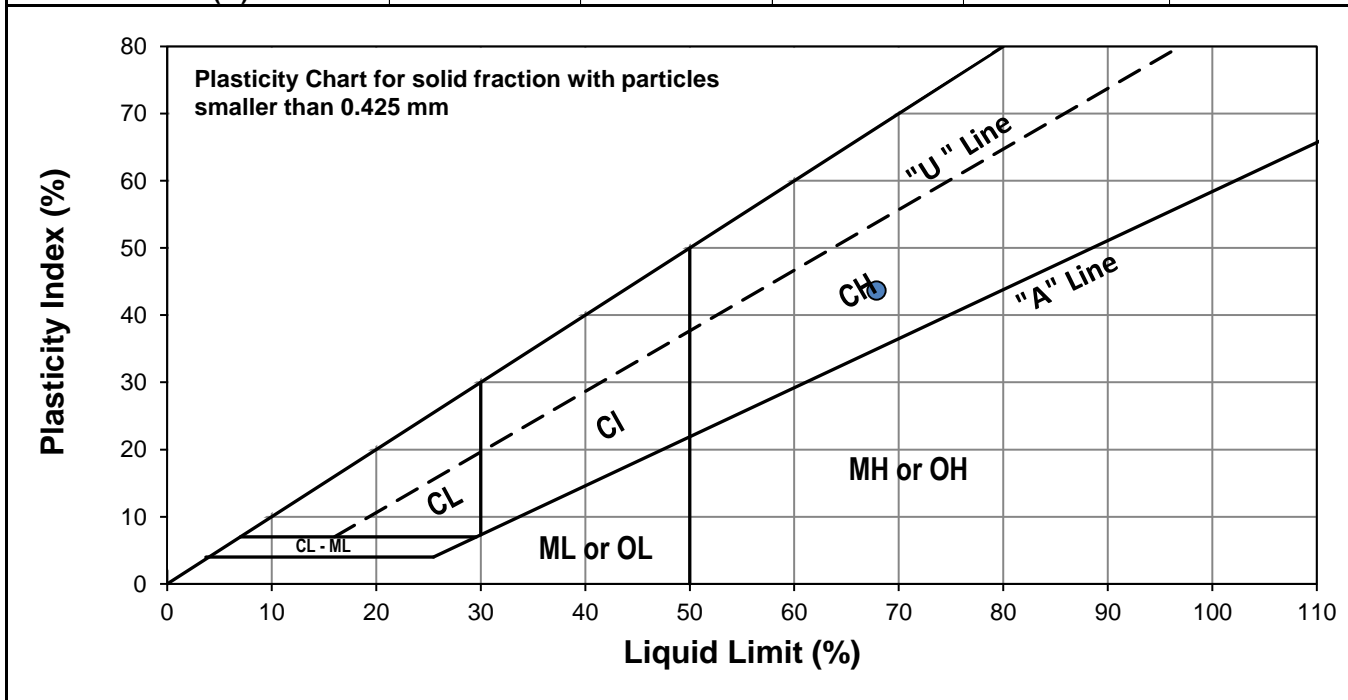
Project No. 0115-031-00
Client Associated Engineering (Sask.) Ltd.
Project Brandon AAFC Research Centre Waterline

Test Hole TP18-05
Sample # G13
Depth (m) 2.7 - 2.9
Sample Date 23-Mar-18
Test Date 29-Mar-18
Technician EH

| | |
|-------------------------|----|
| Liquid Limit | 68 |
| Plastic Limit | 24 |
| Plasticity Index | 44 |

Liquid Limit

| Trial # | 1 | 2 | 3 | | |
|--------------------------|--------|--------|--------|--|--|
| Number of Blows (N) | 18 | 25 | 33 | | |
| Mass Wet Soil + Tare (g) | 23.115 | 25.169 | 24.746 | | |
| Mass Dry Soil + Tare (g) | 19.396 | 20.743 | 20.584 | | |
| Mass Tare (g) | 14.095 | 14.258 | 14.234 | | |
| Mass Water (g) | 3.719 | 4.426 | 4.162 | | |
| Mass Dry Soil (g) | 5.301 | 6.485 | 6.350 | | |
| Moisture Content (%) | 70.157 | 68.250 | 65.543 | | |



Plastic Limit

| Trial # | 1 | 2 | 3 | 4 | 5 |
|--------------------------|--------|--------|---|---|---|
| Mass Tare (g) | 20.206 | 21.116 | | | |
| Mass Wet Soil + Tare (g) | 19.035 | 19.749 | | | |
| Mass Dry Soil + Tare (g) | 14.121 | 14.186 | | | |
| Mass Water (g) | 1.171 | 1.367 | | | |
| Mass Dry Soil (g) | 4.914 | 5.563 | | | |
| Moisture Content (%) | 23.830 | 24.573 | | | |



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Shelby Tube Visual

Project No. 0115-031-00
Client Associated Engineering (Sask.) Ltd.
Project Brandon AAFC Research Centre Waterline

Test Hole TP18-06
Sample # T21
Depth (m) 2.1 - 2.7
Sample Date 23-Mar-18
Test Date 27-Mar-18
Technician EH

Tube Extraction

Recovery (mm) 285

| | | | |
|-----------------------|------------------|--------|--------------------|
| Bottom - 2.4 m | 2.35 m | 2.17 m | Top - 2.1 m |
| Keep | Moisture Content | | PP |
| | Visual | | Tv |
| | Bulk | | |
| 40 mm | 180 mm | 65 mm | |

Visual Classification

| | |
|----------------------------------|-------|
| Material | Clay |
| Composition | silty |
| trace silt inclusions (<15 mm Ø) | |
| trace oxidation | |
| trace rootlets | |

| | |
|--------------------|-----------------|
| Color | grey |
| Moisture | damp |
| Consistency | very stiff |
| Plasticity | high plasticity |
| Structure | |
| Gradation | |

| | |
|---------------------------------------|-------|
| Torvane | |
| Reading | 0.63 |
| Vane Size (s,m,l) | s |
| Undrained Shear Strength (kPa) | 154.5 |

Pocket Penetrometer

| | | |
|---------------------------------------|----------------|-------|
| Reading | 1 | 3.90 |
| | 2 | 3.70 |
| | 3 | 3.70 |
| | Average | 3.77 |
| Undrained Shear Strength (kPa) | | 184.7 |

Moisture Content

| | |
|----------------------------|-------|
| Tare ID | N62 |
| Mass tare (g) | 8.6 |
| Mass wet + tare (g) | 312.7 |
| Mass dry + tare (g) | 237.9 |
| Moisture % | 32.6% |

Unit Weight

| | | |
|---------------------------|--------|--------|
| Bulk Weight (g) | 1092.3 | |
| Length (mm) | 1 | 142.23 |
| | 2 | 141.91 |
| | 3 | 142.20 |
| | 4 | 142.37 |
| Average Length (m) | | 0.142 |

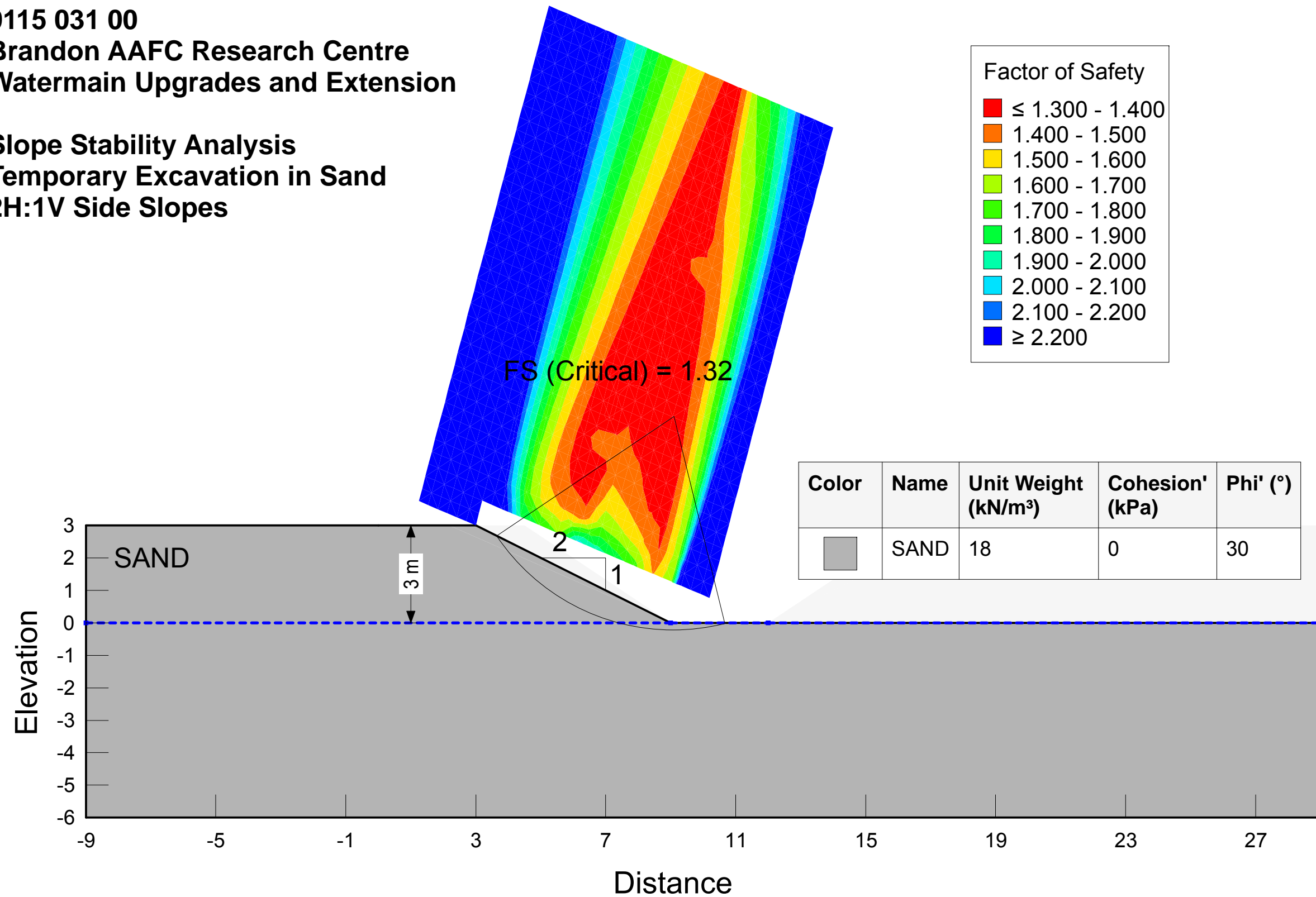
| | | |
|-----------------------------|---|-------|
| Diam. (mm) | 1 | 71.75 |
| | 2 | 72.23 |
| | 3 | 72.01 |
| | 4 | 72.47 |
| Average Diameter (m) | | 0.072 |

| | |
|--------------------------------------------|----------|
| Volume (m³) | 5.81E-04 |
| Bulk Unit Weight (kN/m³) | 18.4 |
| Bulk Unit Weight (pcf) | 117.4 |
| Dry Unit Weight (kN/m³) | 13.9 |
| Dry Unit Weight (pcf) | 88.5 |

Slope Stability Outputs

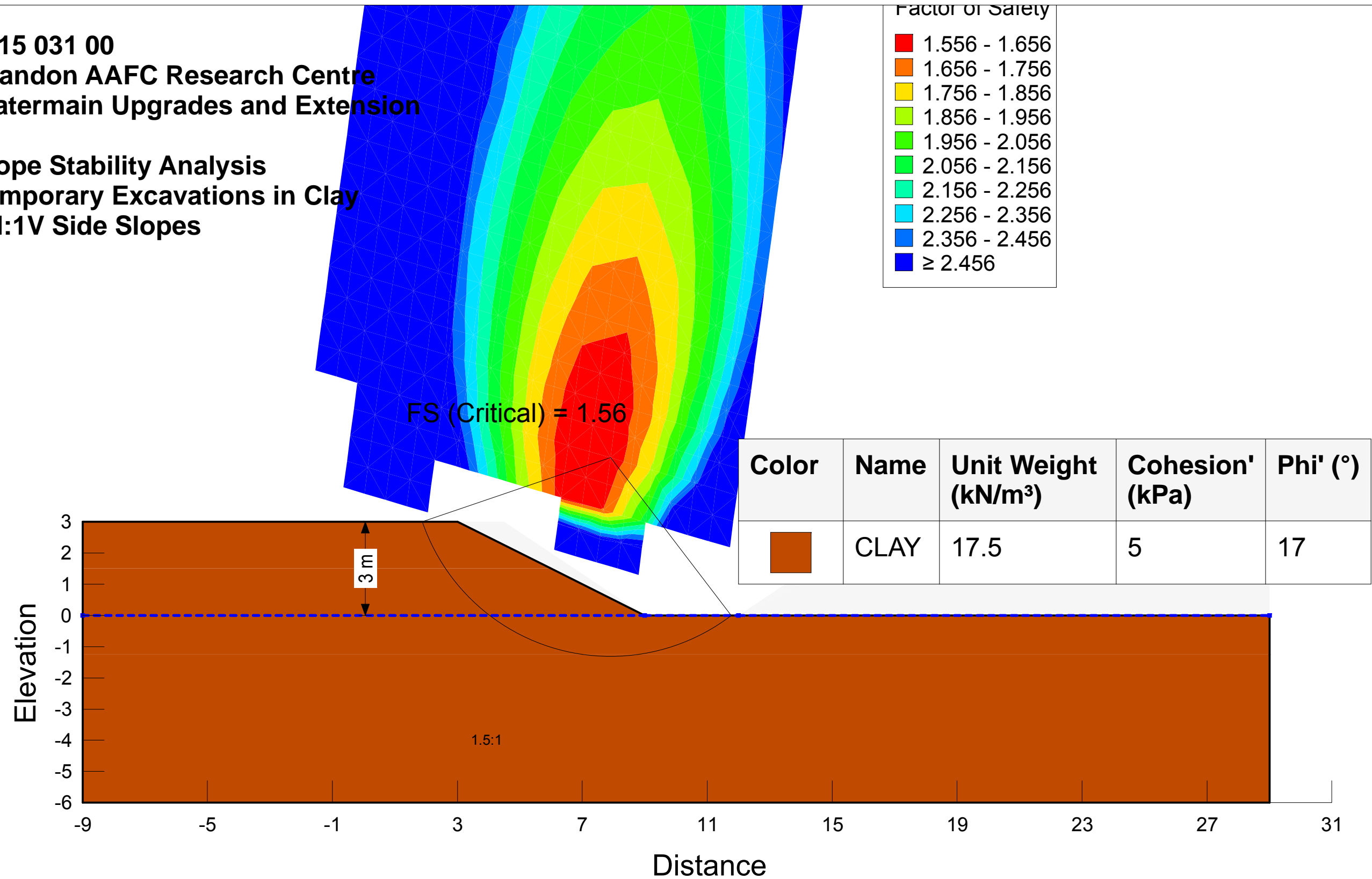
0115 031 00 Brandon AAFC Research Centre Watermain Upgrades and Extension

Slope Stability Analysis Temporary Excavation in Sand 2H:1V Side Slopes



0115 031 00
Brandon AAFC Research Centre
Watermain Upgrades and Extension

Slope Stability Analysis
Temporary Excavations in Clay
2H:1V Side Slopes





Quality Engineering | Valued Relationships

April 12, 2018

File No. 0115-031-00

Mr. Chris Houston

Associated Engineering (Sask.) Ltd.

203 - Number Five Donald Street

Winnipeg, MB

R3L 2T4

**RE Brandon AAFC Research Centre – Watermain Upgrades and Extension
Geotechnical Investigation Report Addendum No. 1 – Laboratory Testing Results**

This letter is an addendum to the geotechnical report issued by TREK on April 9, 2018 to Associated Engineering (Sask.) Ltd. for the proposed watermain at the AAFC Brandon Research Centre. The addendum provides results of laboratory testing that was not completed at the time the report was issued.

Two soil samples (G05 from TP18-02 and G13 from TP18-02) were tested by ALS Environmental (ALS) for resistivity, conductivity, and acidity (pH). A summary of the results is provided in the table below and the laboratory testing report provided by ALS is attached.

| Test Hole ID | Sample Depth | Sample ID | Soil Type | Resistivity | Conductivity | Acidity (pH) |
|--------------|--------------|-----------|-----------|------------------|--------------|--------------|
| TP18-02 | 2.7 to 2.9 m | G05 | Sand | 14,300 ohm-cm | 0.0699 mS/cm | 7.95 |
| TP18-05 | 2.7 to 2.9 m | G13 | Clay | 3,190 ohm-cm | 0.313 mS/cm | 7.86 |

If you have any questions or require any additional information, please contact the undersigned.

Kind Regards,

TREK Geotechnical

Per:

Ryan Belbas M.Sc., P.Eng.

Geotechnical Engineer

Attach.



TREK Geotechnical Inc.
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Date Received: 05-APR-18
Report Date: 11-APR-18 12:20 (MT)
Version: FINAL

Client Phone: 204-975-9433

Certificate of Analysis

Lab Work Order #: L2076421
Project P.O. #: 0115-031-00
Job Reference: 0115-031-00
C of C Numbers:
Legal Site Desc:

Craig Riddell, B.Sc.Ag
Account Manager

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ALS ENVIRONMENTAL ANALYTICAL REPORT

| Sample Details/Parameters | Result | Qualifier* | D.L. | Units | Extracted | Analyzed | Batch |
|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------|------------|-------------------------------------------|----------------------------------------------|-----------------------|--------------------------------------------------------------|--------------------------------------------------|
| L2076421-1 TP18-02 G05 (9.0'-9.5') Sampled By: CLIENT on 23-MAR-18 Matrix: Soil - GRAB Miscellaneous Parameters % Moisture Resistivity Conductivity pH | 4.11 14300 0.0699 7.95 | | 0.10 1.0 0.0040 0.10 | % ohm*cm mS/cm pH units | 10-APR-18 | 10-APR-18 11-APR-18 11-APR-18 10-APR-18 | R4007957 R4008146 R4007517 |
| L2076421-2 TP18-02 G13 (9.0'-9.5') Sampled By: CLIENT on 23-MAR-18 Matrix: Soil - GRAB Miscellaneous Parameters % Moisture Resistivity Conductivity pH | 24.4 3190 0.313 7.86 | | 0.10 1.0 0.0040 0.10 | % ohm*cm mS/cm pH units | 10-APR-18 | 10-APR-18 11-APR-18 11-APR-18 10-APR-18 | R4007957 R4008146 R4007517 |
| | | | | | | | |

* Refer to Referenced Information for Qualifiers (if any) and Methodology.

Reference Information

Test Method References:

| ALS Test Code | Matrix | Test Description | Method Reference** |
|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------|-------------------------|-------------------------|
| EC-WT | Soil | Conductivity (EC) | MOEE E3138 |
| A representative subsample is tumbled with de-ionized (DI) water. The ratio of water to soil is 2:1 v/w. After tumbling the sample is then analyzed by a conductivity meter. | | | |
| Analysis conducted in accordance with the Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act (July 1, 2011). | | | |
| MOISTURE-WT | Soil | % Moisture | Gravimetric: Oven Dried |
| PH-WT | Soil | pH | MOEE E3137A |
| A minimum 10g portion of the sample is extracted with 20mL of 0.01M calcium chloride solution by shaking for at least 30 minutes. The aqueous layer is separated from the soil and then analyzed using a pH meter and electrode. | | | |
| Analysis conducted in accordance with the Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act (July 1, 2011). | | | |
| RESISTIVITY-CALC-WT | Soil | Resistivity Calculation | APHA 2510 B |
| Resistivity are calculated based on the conductivity using APHA 2510B where Conductivity is the inverse of Resistivity. | | | |
| RESISTIVITY-CALC-WT | Soil | Resistivity Calculation | MOECC E3138 |
| Resistivity are calculated based on the conductivity using APHA 2510B where Conductivity is the inverse of Resistivity. | | | |

** ALS test methods may incorporate modifications from specified reference methods to improve performance.

The last two letters of the above test code(s) indicate the laboratory that performed analytical analysis for that test. Refer to the list below:

| Laboratory Definition Code | Laboratory Location |
|----------------------------|-----------------------------------------------|
| WT | ALS ENVIRONMENTAL - WATERLOO, ONTARIO, CANADA |

Chain of Custody Numbers:

GLOSSARY OF REPORT TERMS

Surrogates are compounds that are similar in behaviour to target analyte(s), but that do not normally occur in environmental samples. For applicable tests, surrogates are added to samples prior to analysis as a check on recovery. In reports that display the D.L. column, laboratory objectives for surrogates are listed there.

mg/kg - milligrams per kilogram based on dry weight of sample

mg/kg ww - milligrams per kilogram based on wet weight of sample

mg/kg lwt - milligrams per kilogram based on lipid-adjusted weight

mg/L - unit of concentration based on volume, parts per million.

< - Less than.

D.L. - The reporting limit.

N/A - Result not available. Refer to qualifier code and definition for explanation.

Test results reported relate only to the samples as received by the laboratory.

UNLESS OTHERWISE STATED, ALL SAMPLES WERE RECEIVED IN ACCEPTABLE CONDITION.

Analytical results in unsigned test reports with the DRAFT watermark are subject to change, pending final QC review.