



RETURN BIDS TO:

RETOURNER LES SOUMISSIONS À:

Bid Receiving Public Works & Government Services
Canada/Réception des soumissions Travaux publics et
Services gouvernementaux Canada

1713 Bedford Row

Halifax, N.S./Halifax, (N.E.)

Halifax

Nova Scotia

B3J 1T3

Bid Fax: (902) 496-5016

**SOLICITATION AMENDMENT
MODIFICATION DE L'INVITATION**

The referenced document is hereby revised; unless otherwise
indicated, all other terms and conditions of the Solicitation
remain the same.

Ce document est par la présente révisé; sauf indication contraire,
les modalités de l'invitation demeurent les mêmes.

Comments - Commentaires

Vendor/Firm Name and Address

Raison sociale et adresse du
fournisseur/de l'entrepreneur

Issuing Office - Bureau de distribution

Atlantic Region Acquisitions/Région de l'Atlantique
Acquisitions

1713 Bedford Row

Halifax, N.S./Halifax, (N.E.)

Halifax

Nova Scot

B3J 1T3

Title - Sujet Hampton Harbour Approach	
Solicitation No. - N° de l'invitation EB144-192089/A	Amendment No. - N° modif. 004
Client Reference No. - N° de référence du client EB144-19-2089	Date 2018-11-28
GETS Reference No. - N° de référence de SEAG PW-\$PWA-110-5819	
File No. - N° de dossier PWA-8-80086 (110)	CCC No./N° CCC - FMS No./N° VME
Solicitation Closes - L'invitation prend fin at - à 02:00 PM on - le 2018-12-04	Time Zone Fuseau horaire Atlantic Standard Time AST
F.O.B. - F.A.B. Plant-Usine: <input type="checkbox"/> Destination: <input checked="" type="checkbox"/> Other-Autre: <input type="checkbox"/>	
Address Enquiries to: - Adresser toutes questions à: Collier (PWA), Susan	Buyer Id - Id de l'acheteur pwa110
Telephone No. - N° de téléphone (902) 401-3352 ()	FAX No. - N° de FAX (902) 496-5016
Destination - of Goods, Services, and Construction: Destination - des biens, services et construction:	

Instructions: See Herein

Instructions: Voir aux présentes

Delivery Required - Livraison exigée	Delivery Offered - Livraison proposée
Vendor/Firm Name and Address Raison sociale et adresse du fournisseur/de l'entrepreneur	
Telephone No. - N° de téléphone Facsimile No. - N° de télécopieur	
Name and title of person authorized to sign on behalf of Vendor/Firm (type or print) Nom et titre de la personne autorisée à signer au nom du fournisseur/ de l'entrepreneur (taper ou écrire en caractères d'imprimerie)	
Signature	Date

Solicitation Amendment 004 is being raised to incorporate the following:

Delete in its entirety:

Previous Geotechnical Report

Insert:

Revised Geotechnical Report

ALL OTHER TERMS AND CONDITIONS REMAIN THE SAME.



**GEOTECHNICAL INVESTIGATION
HAMPTON WHARF
HAMPTON, NOVA SCOTIA**

Submitted to:

Public Works and Government Services Canada
1713 Bedford Row
Halifax, Nova Scotia B3H 1T6

Submitted by:

Amec Foster Wheeler Environment & Infrastructure
10 Troop Avenue Unit 100
Dartmouth, Nova Scotia B3A 1A1

14 October 2017
TV177001

TABLE OF CONTENTS

	<u>PAGE</u>
TABLE OF CONTENTS	1
1 INTRODUCTION	
1.1 PROJECT AND SITE DESCRIPTION	
1.2 INVESTIGATION PURPOSE	
1.3 PROJECT RATIONALE AND SCOPE	
1.4 Site and with obble	
1.5 and site	
1.6 and	
1.7 inferred bedrock	
1.8 ground water condition	
1.9 DESIGN REQUIREMENTS	
1.10 General	
1.11 Timber Pole	
1.12 Structural Design	
1.13 Penetration Test	
1.14 Net effective friction down dr	7
1.15 Installation of Timber Pole	
1.16 New structure	
1.17 Reduction	
1.18 Foundation settlement under the New	
1.19 R	

1 INTRODUCTION

Amec Foster Wheeler Environment & Infrastructure Division of Amec Foster Wheeler Americas Limited (Amec Foster Wheeler) has been retained by Public Works and Government Services Canada (PWGSC) in accordance with the RFP dated June 1, 2017 to carry out a geotechnical investigation at the site of the existing wharf. The site is located in Milton, Ontario.

The purpose of the investigation was to determine the subsurface conditions at the site and based on these conditions to provide geotechnical design recommendations for the proposed repair of the existing wharf.

The report provides specific and clear recommendations for the proposed project described herein and includes geotechnical design recommendations.

There should also be an ongoing communication with Amec Foster Wheeler during both the detailed design and construction phases of the project to ensure that the recommendations in this report have been interpreted and implemented correctly. Additional further clarification and/or elaboration are needed concerning the geotechnical aspects of the project. Amec Foster Wheeler should be contacted immediately.

2 PROJECT AND SITE DESCRIPTION

The existing wharf consists of a closed face timber pile and tie beam system retaining wall. It is understood that the retaining wall is a gravity retaining wall on approximate length of 10 m and extends from the bridge abutment to a more recent constructed retaining wall. According to historical records the timber pile retaining wall was constructed in 1970. The timber piles have been driven and tilted outward. The tie beam system tie rod connections were on the piles to a concrete anchor wall foundation. The existing backfill material consists of granular fill.

The wharf's site is located in Milton, Ontario. The site location and project layout are shown on Figure 1.

3 INVESTIGATION PROCEDURE

The field work for the investigation was carried out under the supervision of Amec Foster Wheeler personnel on August 10 and September 1, 2017. A total of three boreholes BH1 to BH3 were drilled at the site to determine from 0.7 to 10 m. The three boreholes were drilled out in front of the existing timber pile retaining wall at a distance of 0.1 and 0.7 m from the intersection of the wall with the bridge. The borehole locations are shown on the attached plan in Figure 2.

The boreholes were advanced using a track-mounted drilling rig provided by No. 1 Drilling Inc. The soils encountered were composed of continuous interbedded silty sand and 0.0 mm to 0.075 mm fines. In order to determine the relative density and/or consistency of the subsoil, a Standard Penetration Test (SPT) was carried out for each borehole attempt.

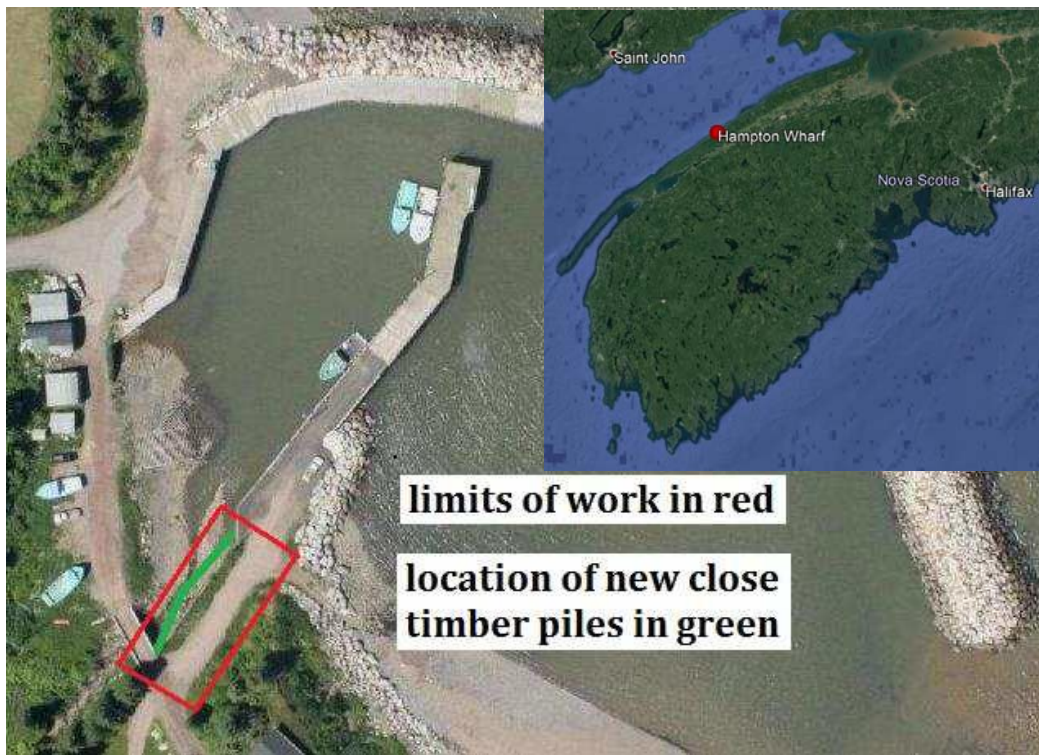


Figure 1: Site Location and Project Layout

During drilling of the borehole the conditions encountered were as follows: Consolidated. Re-represent the samples were placed in moisture-tight containers and taken to our laboratory for classification and testing.

The borehole locations were established in the field by our personnel.

4 SUBSURFACE CONDITIONS

Details of the conditions encountered at the borehole locations are provided on the borehole logs in Appendix A. The following section summarizes the conditions and describes them in accordance with the unified classification system.

It should be noted that stratigraphic boundaries indicated on the borehole logs do not necessarily represent a transition from one condition to another and do not necessarily indicate an exact line of geologic change. Subsurface conditions may vary between and beyond the borehole locations.

4.1 Silty Sand with Cobbles

A layer of red brown sand with cobbles and small boulders was encountered from ground surface at both the borehole locations. The thickness of this layer ranged from 0 m to 0 m.

P 000
 geotechnical investigation
 000000 000000000000N
 000000 0017

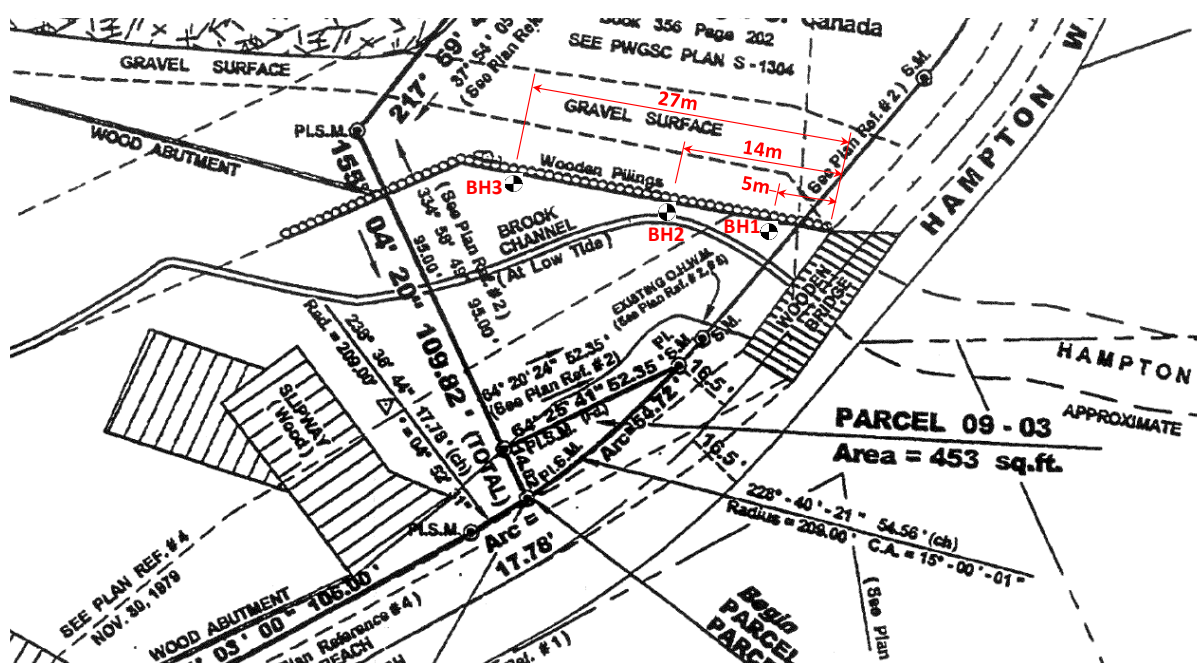


Figure 2: Borehole Location Plan

Measured 'N' values in this layer ranged from 0 to 100 indicating a very loose to compact compressive condition. The 0000 N value is attributed to the presence of cobbles.

4.2 Sandy Silty Clay

A layer of red brown sand and silt clay was encountered below the sand with cobbles at the borehole. The layer extended to the bottom of the hole. The thickness of the layer ranged from 0.7 m to over 1.0 m.

From the standard curve recorded in Appendix 1 performed on two samples of the layer indicated the material to contain 0 to 10 percent fines to sand and 0 to 10 percent fines.

An Atterberg limit test performed on one sample of the layer indicated the material to be of low plasticity with a liquid limit of 40 and a plasticity index of 7. The test results are presented on the 10 in Appendix A and on the sieve sheet in Appendix 1.

The in-situ water content from two samples of the layer ranged between 10.1 and 10.0 percent.

Measured 'N' values in this layer ranged from 0 to over 17 indicating firm to very stiff consistency.

4.3 Sandy Clay

A layer of red brown sand and clay was encountered below the sand and silt clay in the borehole. The layer extended to the bottom of the hole. The thickness of the layer was 0.1 m.

4.4 Inferred Bedrock

Bedrock was inferred below the sandstone in 1 to 2 m depth below ground surface.

4.5 Groundwater Conditions

Groundwater was not observed during drilling of the borehole. However, the area is located in the tidal zone.

5 DESIGN RECOMMENDATIONS

5.1 General

It should be noted that the design recommendations for this project are provided for the guidance of the designer. The contractor bidding on or undertaking the work should make their own assessment of the site and interpretation of the recommendations provided so to effect their construction procedure and schedule.

As mentioned above, the existing closed face timber sheet pile wall on retention wall to support the wharf. The maximum retained height of the wharf is about 2 m. The top of the sheet pile wall is tied back with tie rods to a concrete anchor wall. As mentioned above, the existing timber sheet pile wall has been damaged and tilted outward as a result of foundation settlement.

The following is understood:

- The proposed repair of the wharf will include installation of a new retention structure in front of the existing foundation wall to provide required lateral support for the existing wharf.
- The new retention structure will be constructed of precast treated timber sheet pile wall tied back to the existing concrete anchor wall.
- The new timber sheet pile wall will be 100 to 200 mm thick and 200 mm butt diameter.
- The gap between the existing wall and the new retention structure will be filled with granular material.
- There will be no settlement on the sheet pile other than their own weight.

5.2 Timber Piles

5.2.1 Structural Design

After the 2004 Indian Ocean Foundation Engineering Manual, the structural design of wood sheet pile must conform with the requirements of Section 4 of the National Building Code of Canada 2004. No special consideration needs to be taken to sand in the sheet pile but special attention must be taken to protect the sheet pile end and head from damage due to drilling the sheet pile.

5.2.2 Penetration Depth

The 2004 Manual provides general guidance for determining penetration depth of flexible sheet pile retention wall similar to the proposed retention structure at location 1.

After 2004 Manual, two different methods can be used for design of precast anchor wall system. The "free-earth" and "fixed-earth" methods. When the soft ground condition at the site, the

"free-earth" method can be considered more appropriate and suitable for design of single anchor wall system at Port of Mombasa. The "free-earth" method assumes that the wall acts as a beam supported at two points, the base of the wall and the anchor, and the pressure of the earth below the anchor bottom is free to rotate or translate throughout its bottom end.

To determine the required depth of penetration, D, the effective surcharge and water pressure on the retaining wall could be estimated from the configuration of the harbour bed and the sediment pressure distribution on the timber wall can be modified as shown below in Figure 3.

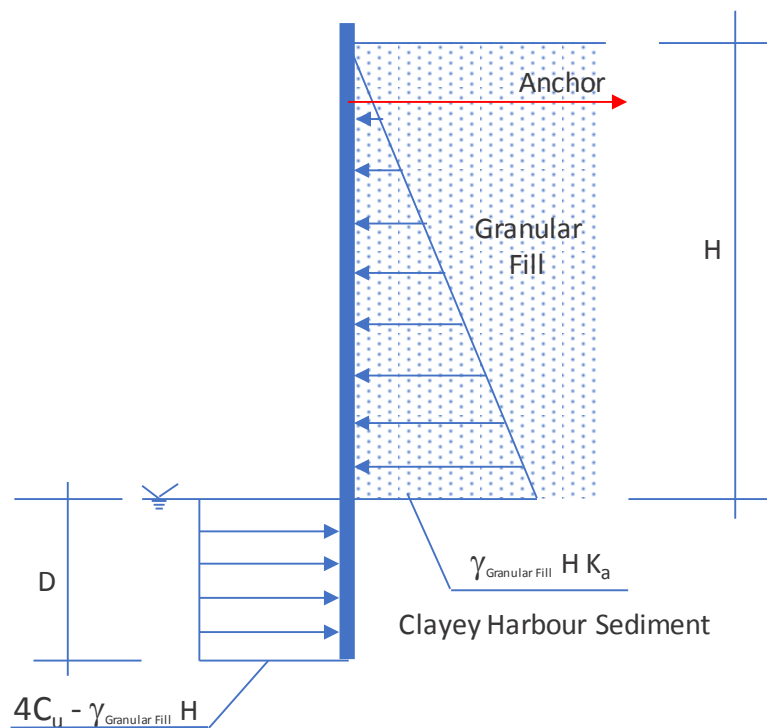


Figure 3. Schematic lateral pressure distribution on anchored sheet pile wall in clay

If the surcharge is present on the wall, the effect of that traffic on the retaining wall could be added to the pressure distribution presented above.

As shown on Figure 3, the pressure coefficient, K_a , unit weight of granular fill and undrained shear strength, c_u , of harbour sediment are required to estimate the pressure on the wall or the purpose of retaining wall in the K_a and unit weight of granular fill can be assumed 0.0 and 1.0 N/m³ respectively. The recommended for retaining design undrained shear strength of the harbour sediment is shown below on Figure 4.

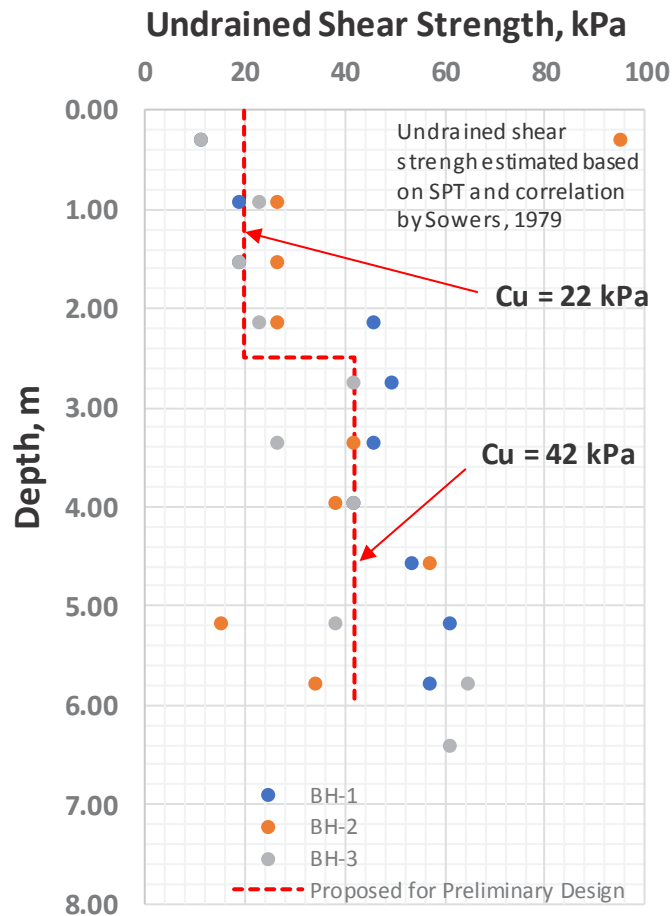


Figure 4. Proposed undrained shear strength of harbour sediment

The required depth of penetration is determined from the moment equilibrium about the support contact. It is recommended to increase the estimated depth by 0.5 to 1.0 to provide an adequate factor of safety of 1.5 or more based on our preliminary estimate of penetration depth of the new timber pile. It could be that the

It is possible that the interference induced by the new pile may not fully develop due to the pile being due to the narrow space to be filled between the existing pile and the new timber pile. In the other hand, it is unclear how the existing pile and timber pile will interact with the new pile and the new timber pile will be difficult to model the condition accurately and the model is out of our current scope. Therefore, for the purpose of preliminary design, the full capacity of the pile on the new pile will be assumed to be acceptable and simplified to more conservative model.

5.2.3 Negative Friction (down drag)

After the new pile is installed through the stratum of cohesive soil, the downward movement of the consolidated sediment will cause a drag on the pile. The downward drag may cause settlement and reduce the capacity of the pile. However, based on our

understand there will be no vertical load on the new pile other than their own weight. Therefore potential settlement and reduced capacity of the new timber pile due to down drag will be minimal to no impact on the structural integrity of the wharf.

5.2.4 Installation of Timber Piles

A 100mm M1000 when driven wood pile low-velocity hammer blow should be used for embedding and in the case of termite treatment should be re-treated immediately after incorporation of the soft curing in the case block. The rate of the hammer used for the driving depends on experience and on a number of factors. The weight of the pile, the diameter of the pile and the length of the pile should be considered. The hammer-rated energy should be about 1000 Joules and should not exceed 1000 Joules equal to 1000 Newton metre (1000 Nm) for the pile diameter in metres.

The pile head should be protected with protection in the form of a steel cap and the pile toe should be protected with a steel cap. Timber piles cannot withstand hard driving and driving will be restricted to the destruction of the pile. To avoid this, driving must be stopped when resistance to penetration is encountered. The set criteria should not exceed 100mm.

Our understanding is that the new retention wall will not be used to tie back and therefore no dredging is required. At the bottom of the trench should be excavated in the harbour bottom to accommodate installation of the new timber pile. Our understanding is that the proposed trench will be offset 1 to 2 m from the base of existing wall and should be 0.5 m deep. The trench is required to remove large cobbles and boulders from the harbour bottom that may obstruct the driving operation. The trench should be backfilled with granular fill following the completion of new pile installation.

5.3 New Granular fill

5.3.1 Fill Gradation

The new granular fill to be placed between the new and the existing pile should consist of rock fill between 20 and 100 mm in size.

5.3.2 Consolidation Settlement under the New Fill

The new fill placed between two walls and new wall introduce additional weight on the soft harbour sediment causing it to settle. The settlement process comprises of three components: immediate settlement, consolidation settlement and secondary compression creep. The magnitude of each component varies depending on the nature and properties. The consolidation settlement dominates in saturated or near saturated fine grain soils.

To accurately estimate the consolidation settlement under the new fill, advanced field monitoring program combined with advanced computer modelling is required. However, a program and testing is outside of the current scope.

Based on our preliminary estimate, the consolidation settlement under the new fill not expected to exceed 20 cm with consolidation to be completed within four years or less. The estimate were made based on the following assumption:

- The thickness of the new fill 1 m
- Offset distance between the new and the existing timber pile wall 0.5 m or less

P eotec n c n e t t o n
m t o n r f m t o n N
o t o b e r 0 1 7

- The thickness of the soft clastic sediment range between 0 and 10 m and the sediment underlain by low permeable bedrock
- The confining characteristics of the soft clastic sediment were determined based on submergence retention

6 CLOSURE

A geotechnical investigation is required on the limited amount of site. The recommendation contained in this report is based upon the condition encountered at the borehole location. It could in condition be encountered which differ from those at the borehole location. We request that we be notified immediately in order to permit re-evaluation of our recommendation.

The work has been undertaken in accordance with normal accepted electronic engineering practice. No other warrantable error is alleged or implied. The limitation of the report is reiterated in Appendix A. Advice was given that the court made of the information or reliance on or decision made based on the report is the responsibility of such third parties. Amec Cyber Security accept no responsibility for damage if any suffered by any third party as a result of decision made or action based on the report.

☐ ☐ ncere ☐ ☐

AMEC Foster Wheeler Environment & Infrastructure
A division of AMEC Foster Wheeler Americas Limited

Yours

oe rMAcPn
enoreotecncnneer

Bauer

ten PDPn
eotecncneer

APPENDIX A

BOREHOLE LOGS

GENERAL REPORT NOTES

STANDARD PENETRATION TEST—SPT

The standard penetration values are recorded on the Borehole Records as N values. The N values are the number of blows required to advance a standard, 50 mm diameter, split spoon sampler a distance of 305 mm into the soil using a 63.5 kg hammer freely falling a distance of 760 mm.

DYNAMIC CONE PENETRATION TEST----DCPT

This is a similar procedure to that used in driving a standard 50 mm split spoon sampler except that a cone is driven rather than a soil sampler. A variety of cones can be used. Often the cones are 51 mm diameter with a 60 degree taper from the tip.

SAMPLE TYPE ABBREVIATION USED ON BOREHOLE LOGS

S.S.	Split spoon	S. H.	Shelby tube	W.S.	Wash sample
A.S.	Auger sample	R. C.	Rock Core	P.	Sample pushed

SOIL DESCRIPTION

The standard terminology to describe cohesionless soils includes the compactness condition as generally determined by the SPT.

The standard terminology to describe cohesive soils includes the consistency, which is based on various methods of determining undrained shear strength, and by SPT


Cohesionless Soils.		Cohesive Soils		
<u>Condition</u>	<u>N Values</u>	<u>Consistency</u>	<u>N Values</u>	<u>Undrained Shear Strength, kPa</u>
Very loose	0 – 4	Very soft	0 – 2	< 12.5
Loose	4 – 10	Soft	2 – 4	12.5 - 25
Compact	10 – 30	Firm	4 – 8	25 – 50
Dense	30 – 50	Stiff	8 – 15	50 - 100
Very Dense	> 50	Very stiff	15 – 30	100 – 200
		Hard	>30	>200

NOTE

The soil conditions, profiles, comments, conclusions and recommendations found in this report are based upon samples recovered during the field work. Soils are heterogeneous materials, and, consequently, variations may be encountered at site locations away from where the samples were obtained. During construction, competent, qualified personnel should verify that no significant variations exist from those described in the report.

LOG OF BOREHOLE BH1

SHEET 1 OF 1


PROJECT No.: TV177001	ELEVATION: ---	
CLIENT: PWGSC	DATUM:	
PROJECT NAME: PRO Delhaven & Hampton	METHOD: SS / Auger	
LOCATION: Hampton Warf	DIAMETER: 100 mm	
DATE DRILLED: 9-14-17	WATER LEVEL:	
LOGGED BY: A. Gale	CONTRACTOR: Nova Drilling	

DEPTH (m)	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	STRATA PLOT	WATER LEVEL	SAMPLES					UNDRAINED SHEAR STRENGTH					PLASTIC LIMIT W _P	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L
					TYPE	NUMBER	RECOVERY (mm)	N-VALUE or RQD%	OTHER TESTS	△ Peak (kPa)		▲ Residual					
										20	40	60	80				
										STANDARD PENETRATION TEST Blows/0.3m				20			
WATER CONTENT (%)																	
102030																	
		Red / Brown, silty SAND with cobbles, small boulders and clay			SS	1	25	3		●							
1		Red / Brown, sandy silty CLAY (CL-ML)			SS	2	500	5		●							
					SS	3	425	5		●							
2					SS	4	600	12	S, L, M	●							
					SS	5	225	13		●							
3					SS	6	225	12		●							
					SS	7	600	11		●							
4					SS	8	450	14		●							
					SS	9	250	16		●							
5					SS	10	450	15		●							
6					SS	11	200	77 / 400mm		●							
		Inferred Grey, sand stone bedrock			AU												
		End of Borehole @ 6.7 m															

GEOTECHNICAL BOREHOLE TV177001_HAMPTON WHARF.GPJ AMEC HALIFAX.GDT 10/18/17

LOG OF BOREHOLE BH2

SHEET 1 OF 1


PROJECT No.: TV177001	ELEVATION: ---	
CLIENT: PWGSC	DATUM:	
PROJECT NAME: PRO Delhaven & Hampton	METHOD: SS / Auger	
LOCATION: Hampton Warf	DIAMETER: 100 mm	
DATE DRILLED: 9-14-17	WATER LEVEL:	
LOGGED BY: A. Gale	CONTRACTOR: Nova Drilling	

DEPTH (m)	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	STRATA PLOT	WATER LEVEL	SAMPLES					UNDRAINED SHEAR STRENGTH					PLASTIC LIMIT W _P	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L
					TYPE	NUMBER	RECOVERY (mm)	N-VALUE or RQD%	OTHER TESTS	△ Peak (kPa)		▲ Residual					
										20	40	60	80				
										STANDARD PENETRATION TEST Blows/0.3m							
0																	
1 																	

GEOTECHNICAL BOREHOLE TV177001_HAMPTON WHARF.GPJ AMEC HALIFAX.GDT 10/18/17

LOG OF BOREHOLE BH3

SHEET 1 OF 1

PROJECT No.: TV177001	ELEVATION: ---	
CLIENT: PWGSC	DATUM:	
PROJECT NAME: PRO Delhaven & Hampton	METHOD: SS / Auger	
LOCATION: Hampton Warf	DIAMETER: 100 mm	
DATE DRILLED: 9-14-17	WATER LEVEL:	
LOGGED BY: A. Gale	CONTRACTOR: Nova Drilling	

DEPTH (m)	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	STRATA PLOT	WATER LEVEL	SAMPLES					UNDRAINED SHEAR STRENGTH △ Peak (kPa) ▲ Residual				PLASTIC LIMIT	NATURAL MOISTURE CONTENT	LIQUID LIMIT
					TYPE	NUMBER	RECOVERY (mm)	N-VALUE or RQD%	OTHER TESTS	STANDARD PENETRATION TEST Blows/0.3m				W _p	W	W _L
										20	40	60	80	10	20	30
0		Red / Brown, silty SAND with cobbles, small boulders and clay			SS	1	100	3		•						
1		Red / Brown, sandy silty CLAY (CL-ML)			SS	2	125	6		•						
					SS	3	600	5		•						
2					SS	4	375	6		•						
					SS	5	225	11		•						
3					SS	6	125	7		•						
					SS	7	125	11		•						
4					AU	8										
					SS	9	250	10		•						
5					SS	10	500	17	S, M	•						
6					SS	11	400	16		•						
		End of Borehole @ 6.7 m														

GEOTECHNICAL BOREHOLE TV177001_HAMPTON WHARF.GPJ AMEC HALIFAX.GDT 10/18/17

APPENDIX B

LAB TEST RESULTS

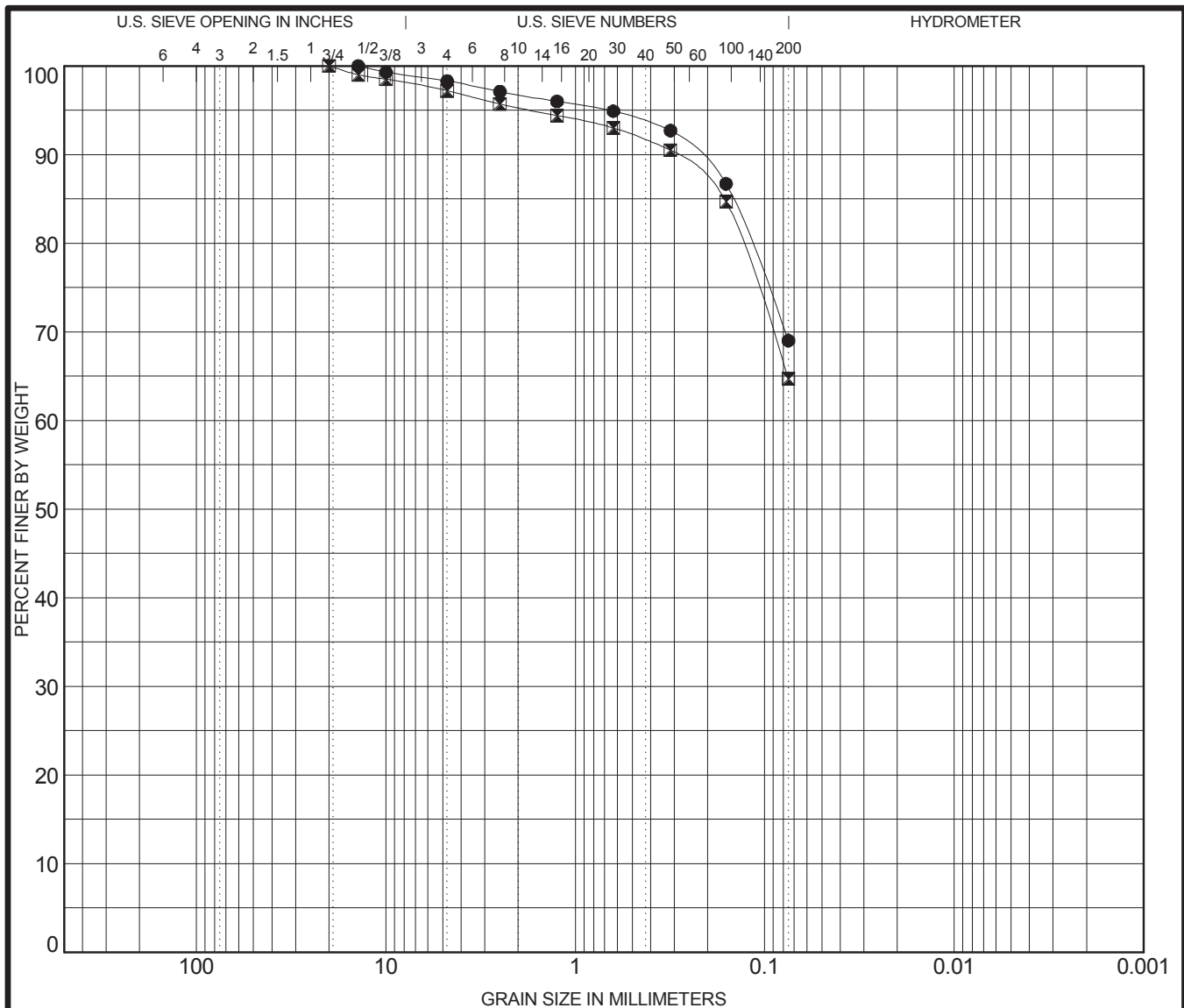


Appendix B. Summary of Laboratory Results

Project No.: TV177001
Client: PWGSC
Project Name: PRO Delhaven & Hampton
Location: Hampton Warf

GENERAL INFORMATION:		SAMPLING:		LAB TEST STATISTICS:	
Number of BH/TP:	3	Auger Cuttings	4	Moisture Content:	2
Total Length of Drilling:	22.3 m	Split Spoon	30	Atterberg Limits:	1
				Sieve Analysis:	2
				Hydrometer Analysis:	0

Borehole	Depth (m)	Liquid Limit	Plastic Limit	Plasticity Index	% Gravel	% Sand	% Silt and Clay	Class-ification	Water Content (%)	Dry Density (Mg/m ³)	Void Ratio
BH1	2.13	20	13	7	1.7	29.3	69.0	CL-ML	20.0		
BH3	5.79				2.8	32.5	64.7	CL-ML	18.1		



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

Specimen Identification		Classification				LL	PL	PI	Cc	Cu
●	BH1	2.13 m	SANDY SILTY CLAY(CL-ML)				20	13	7	
✕	BH3	5.79 m	SANDY SILTY CLAY(CL-ML)							
Specimen Identification		D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay	
●	BH1	2.13 m	14			1.7	29.3	69.0		
✕	BH3	5.79 m	20			2.8	32.5	64.7		

GRAIN SIZE DISTRIBUTION

Project No.: TV177001

Client: PWGSC

Project Name: PRO Delhaven & Hampton

Location: Hampton Warf



APPENDIX C

REPORT LIMITATIONS

REPORT LIMITATIONS

The conclusions and recommendations given in this report are based on information determined at the test hole location. The information contained herein in no way reflects on the environment or effect of the project unless otherwise stated. Subsurface and groundwater conditions between and beyond the test hole may differ from those encountered at the test hole location and conditions may become different during construction which could not be detected or anticipated at the time of the site investigation. It is recommended practice that the geotechnical engineer be retained during the construction to confirm that the subsurface conditions across the site do not deviate materially from those encountered in the test hole.

The design recommendations given in this report are applicable only to the project described in the test and then only if constructed substantially in accordance with the details stated in this report. Since a detailed design of the design may not be known, we recommend that we be retained during the final design stage to verify that the design is consistent with our recommendations and that assumptions made in our analysis are valid.

The comments made in this report relating to potential construction problems and possible methods of construction are intended only for the guidance of the designer. The number of test holes may not be sufficient to determine the effect of construction methods and cost for estimating the time of surficial or for further recommendations and uncertainties. The contractor bidding on this project or undertaking the construction should therefore make their own interpretation of the factual information presented and draw their own conclusions as to how the subsurface conditions may affect their work. This work has been undertaken in accordance with normally accepted geotechnical engineering practice. No other warranties are made or implied.

Anyone who is a third party user of this report or in reliance on or decisions to be made based on the report is responsible of such third parties. Amec Foster Wheeler Environment & Infrastructure accepts no responsibility for damages suffered by a third party as a result of decisions made or actions based on this report.