



LEVELTON CONSULTANTS LTD.

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12 March 2014
Levelton File # R714-0308-00

WSP Canada Inc.
Suite 400 – 401 Garbally Road
Victoria, BC
V8T 5M3

Attention: Mr. Ron Akehurst, P. Eng.

**RE: GEOTECHNICAL ASSESSMENT
HIGHWAY NO. 4 – PACIFIC RIM NATIONAL PARK**

1.0 INTRODUCTION

As requested, Levelton Consultants Ltd. (Levelton) has carried out a geotechnical assessment relating to two specific sections of Highway 4 within the Pacific Rim National Park that have been performing poorly. The sections included approximately 300 m of southbound lane near Station 16+000 (as measured from the southern limit of the park) and approximately 50 m of southbound lane near Station 13+000.

Levelton's scope of work was described in our 7 January 2014 proposal (File Reference: P713-3036-00). Authorization to proceed with the work was received from WSP on 3 February 2014.

2.0 SITE REVIEW

The subject sections of road are located on Highway No. 4 near the Esowista Reserve and directly south of the Tofino Airport, as approximately shown on Figure 1. Levelton visited the site on 11 February 2014 to review the site conditions and lay out the locations of boreholes for the subsurface assessment (see below). Select photographs taken during the site visit are attached. A summary of our observations from the site review is presented below.

2.1 Station 16+000

This section of highway was about 300 m in length and had various sections of the east bound lane that appeared to be performing poorly. The worst area appeared at the westernmost part of this section near the Esowista Reserve. This area was a curved and sloped section of road where the terrain sloped down from north to south and from west to east. Concrete barriers (“no-posts”) lined the south shoulder of the road and the terrain dropped down steeply to the south to about 6 m in elevation below of the concrete barriers.

Several large longitudinal cracks were observed in this area. The cracks were open at the surface, with the most obvious near the south shoulder where the crack had opened about 60 mm. A tape measurer could reach to a depth of 200 mm before encountering resistance.

The terrain in the easterly part of this section was generally level in an east-west direction along the highway and gently sloped from north down to south across the highway. The slope beyond the south shoulder of road was steep in some areas with an elevation change in the order of 1.5 m to 1.8 m below the road. There was a watercourse with a 1.2 m diameter culvert in this area. Water was present on the inlet (north) and outlet (south) side of the culvert, but flow was only observed entering the inlet side of the culvert.

In 2010, Levelton carried out a subsurface assessment near the eastern part of this section as part of a sewer project. As part of that project, a borehole (BH10-07) was drilled and logged by Levelton about 140 m east of the area on the north side of the road. At that time, the conditions in the borehole consisted of 180 mm of layered asphalt, overlying 580 mm of sand and gravel fill, overlying organic silt. A significant amount of wood debris was encountered at the surface of the organic silt. The approximate location of BH10-07 is shown on Figure 2 and the summary borehole log is attached for reference.

2.2 Station 13+000

The section of highway at Station 13+000 was sloped and curved. The terrain sloped down from the north to south and from the east to west. No-post concrete barriers lined the south side of the road. There was a linear crescent-shaped crack, about 30 to 50 m in length, along the south side of the road. The crack was open at the surface about 12 mm in some areas. Adjacent to the crack, the shoulder of the road was relatively narrow and the terrain dropped down steeply about 10 m in elevation to the south from within about 300 mm from the outside edge of the no-post barriers.

In 2010, Levelton carried out a subsurface assessment near this road section as part of a sewer project. As part of that project, a borehole (BH10-17) was drilled through the south shoulder about 400 m to the west, and a borehole (BH10-20) was drilled through the south shoulder about 250 m to the east. At that time, the conditions in BH10-17 consisted of about 450 mm of sand and gravel fill, overlying natural sand deposits. BH10-20 encountered 450 mm of sand and gravel fill, overlying about 600 mm of silt, overlying silty clay. The approximate locations of BH10-17 and BH10-20 are shown on Figure 3 and their summary logs are attached for reference.

3.0 SUBSURFACE ASSESSMENT

Four boreholes (BH14-01 through BH14-04) were advanced as part of the current assessment at the approximate locations shown on Figures 2 and 3. The boreholes were located in areas where there was visible distress (i.e., cracks) in the east bound lane of the road.

Each borehole was advanced using a track mounted auger drill that was owned and operated by Drillwell Enterprises Ltd. of Duncan, BC. BH14-01, 02, and 03 were advanced within the 300 lineal metre area of road described as 'Station 16+000' in this report. BH14-04 was located within the 50 lineal metre area described as 'Station 13+000'. At each location, the existing asphalt was removed and a Dynamic Cone Penetrometer (DCP) was driven from the point below asphalt to a depth that was greater than the height of the road prism above natural grade to the south. The DCP provides an indication of soil consistency and is recorded as the number of blows per 300 mm depth driven by a 63.5 kg hammer falling 760 mm. Where suspected soft soils were encountered, a field vane was used to measure peak and remolded shear strengths. A solid stem continuous flight auger was advanced at each borehole location to log the subsurface conditions encountered and to recover samples for laboratory testing.

A detailed description of the subsurface conditions encountered is provided on the attached borehole logs. In summary of these logs, a general description is presented as follows:

- Asphalt (in layers 180 mm to 330 mm thick); overlying
- Compact SAND AND GRAVEL (19 mm crush road base) FILL; overlying
- Loose to compact SAND and GRAVEL FILL with some organics; overlying
- Firm to stiff SILTY CLAY.

BH14-02 varied from the above in that loose, organic "midden like" material was encountered at a depth of about 1.5 m to 2.4 m below the sand and gravel fill. Loose sand was found below this material and above the silty clay, which was encountered at a depth of 4.0 m. Groundwater was encountered at a depth of about 1.5 m in this borehole. In addition, geotextile was encountered at a depth of 1.3 m below surface in BH14-04.

3.1 Laboratory Testing

Samples were selected based on the findings for laboratory testing, which included moisture content determination, grain size analysis, and Atterberg Limits testing. The testing results are shown on the borehole logs and the attached sieve analyses sheet, and are summarized in Tables 1 and 2.

Table 1: Summary of Grain Size Analyses

Location	Depth (m)	% Fines*	% Sand	% Gravel
BH14-01	0.3 to 1.2	10.5	77.4	12.1

* Fines include silt and clay size particles.

The above noted grain size analysis is based upon a percentage by mass. Within the 'sand' component, there was a significant amount of wood debris, estimated to be about 50% by volume.

Atterberg Limits were performed on a sample of the fine-grained material from BH14-01, BH14-02, and BH14-04 at a depths of 4.0 m, 4.3 m, and 2.1 m, respectively. The results are presented in the following Table 2:

Table 2: Results of Atterberg Limits

Location	Depth (m)	Plastic Limit %	Liquid Limit %	Plasticity Index	Moisture Content %	Classification
BH14-01	4.0	27.4	81.0	53.6	64.8	CH
BH14-02	4.3	19.1	38.7	19.6	29.7	CM
BH14-04	2.1	44.9	76.4	31.5	68.0	OH

The fine-grained material described in Table 2 is classified as inorganic clays of medium (CM) to high (CH) plasticity and organic clay (OH) - based upon the Canadian Foundation Engineering Manual – 4th Edition.

Outside of moisture content determination, no specific laboratory tests were performed on the midden-like material noted in BH14-02. However, upon drying the sample, a fragment of bone was observed.

4.0 Geotechnical Comments and Recommendations

4.1 General

The results of our field and laboratory testing indicate that the subject road sections are located over compressible soils that are susceptible to long term consolidation settlement under applied loads. It is apparent from the condition of the road sections that settlement is ongoing, especially where there is a relatively steep embankment slope and a relatively narrow shoulder. The potential for larger settlements occur in the highly compressible soils with high moisture content (which were found in BH14-01 and BH14-04), and in areas where organic soils were encountered. In the absence of survey monitoring data, and/or laboratory consolidation data, it is difficult to predict the magnitude of future settlements for these areas. Where organics are encountered, this settlement will continue independently of applied load, as the organics break down over time.

Levelton understands that it was common to use logs to spread the load over these compressible soils during early road construction. During drilling, there was evidence of wood pieces at the interface of fill and underlying natural soils that may be the remains of this type of road construction. There was also an attempt to use geotextile to improve road conditions in the area of BH14-04. Levelton observed the placement of this geotextile material in the 1980's as part of a pavement resurfacing program. The geotextile has not demonstrated to be overly effective in the east bound lane and would not prevent consolidation settlement.

Road repairs in the past have also consisted of placing additional layers of asphalt, which is also evidence that the road has continued to settle over a significant period of time. Placing additional layers of asphalt has added more load to these compressible soil areas.

The midden-like material that was encountered in BH14-02 contained a significant amount of organics and would be prone to settlement. Organic silt deposits found in BH10-07 also contained a significant amount of woody debris. Levelton recommends that the presence of the midden-like material be reported to the Archaeology Branch of the Ministry of Forests, Lands and Natural Resource Operations.

As described above, the 1.2 m diameter culvert that was located near BH14-02 and BH14-03 has flows entering the inlet but not exiting the pipe. As such, it is likely corroded and is allowing water to enter into the road fill prism and subgrade. This condition could lead to future stability issues if the water scours and removes fill and subgrade material during high flows and washes out parts of the road.

4.2 Potential Mitigation Solutions

From a geotechnical perspective, several options could be considered to help mitigate ongoing settlements in the subject sections. With each option, WSP and the Owner should consider long-term performance expectations. One item that should be considered carefully is the performance of the road structure during strong earthquake ground motions. This is particularly important if the section of road in question is the planned evacuation route from a tsunami. Although not included as part of this geotechnical assessment, the loose and wet nature of the sandy soils and the relatively steep embankment fill slopes would likely not perform well in response to strong earthquake ground motions.

The best solution to mitigate settlement would be to avoid the compressible soils and rebuild the road elsewhere. These soils may have been avoided if the road was originally constructed further north. However, assuming that the road alignment will remain in the same location, the most practical solution would include reconstruction of the poorly performing areas, which would include:

1. Removing existing asphalt, fill, organics and wood debris within the road prism;
2. Removing and replacing corroded culverts;
3. Designing a road prism with stable embankment slopes, with grades typically not steeper than 2H:1V; and
4. Constructing a road embankment using lightweight fill products, such as pumice, or expanded polystyrene.

The intent of the lightweight fill would be to create an unloading effect of the highly compressible soils. As noted above, the organic soils and wood debris should be completely removed as they will settle independently of load due to material decomposition.

The design would have to consider a road prism that is wider than the current prism, or include some form of a retaining wall system to stay within the current footprint. A retaining wall system would have to be light enough so as not to add additional load the compressible soils.

If the road footprint is to be widened, the design should account for encountering potential compressible soils that have not experienced any additional loads. A component of the design would include laboratory consolidation testing of these soils to assess how much additional load could be placed on virgin soils and how much would need to be removed from currently loaded soils. Further, more detailed subsurface work would be required to obtain relatively undisturbed Shelby Tube samples of the compressible soils for laboratory consolidation testing. The more detailed geotechnical assessment would also be used to delineate the extent of the compressible deposits and could also be used to establish parameters for a seismic stability assessment, if this was considered important for emergency road evacuation performance.

If the road cannot be reconstructed at this time, some localized improvements could be carried out. These would include repair of existing culverts along with localized unloading which would involve removing layers of existing asphalt and replacing localized poor soils with lightweight backfill. If this is the only option that is considered at this time, light weight pumice fill soils should be incorporated into a geosynthetically confined soil (GCS) system. GCS is a layered network of closely spaced soil (200 mm thick) confined between layers of geotextile. The GCS would provide increased shear strength to support areas that are locally steep and would buffer settlements across the road. This would be best suited for the high embankment and locally steep embankment areas that were encountered at BH14-01 and BH14-04.

Removing and replacing asphalt in these poorly performing areas will be a short lived improvement. Adding more asphalt will potentially worsen the problem.

5.0 FUTURE GEOTECHNICAL SERVICES

For the proposed road upgrade, Levelton anticipates that the following geotechnical services could be required:

- Meet with WSP and the Owner to discuss mitigation options that are in line with expected performance;
- Propose and implement a detailed geotechnical assessment for consolidation work, seismic design, and delineation of poor areas;
- Prepare a design specification and section for lightweight backfill;
- Prepare a retaining wall design;
- Review geotechnical aspects of tender specifications; and
- Carry out construction reviews and provide geotechnical support.

6.0 CLOSURE

This report has been prepared by Levelton Consultants Ltd. (Levelton) exclusively for WSP Canada Inc. for application to the project described herein. The report has been prepared in accordance with standard soil mechanics practice and the attached Terms of Reference for Geotechnical Reports.

If you have any questions or require further information, please contact the undersigned.

Yours truly,

LEVELTON CONSULTANTS LTD.

Reviewed by:

SIGNATURE ON FILE

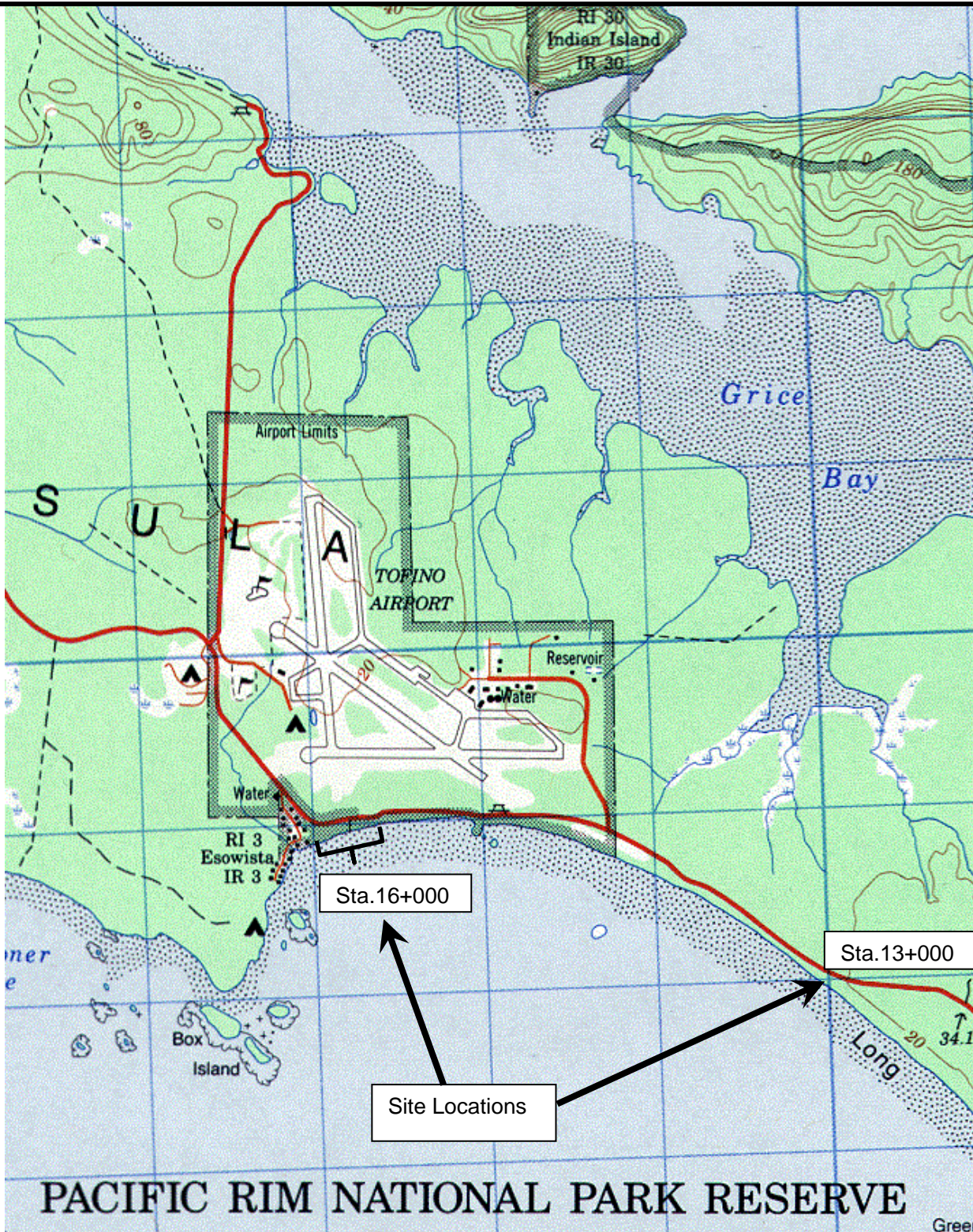
SIGNATURE ON FILE

Per: Don Kaluza, P. Eng.
Senior Geotechnical Engineer

Tom Oxland, P. Eng.
Senior Geotechnical Engineer


Enclosures: Figure 1: Site Location Plan
Figures 2 and 3: Borehole Location Plan
Site Photographs
Borehole Logs
Laboratory Testing
Terms of Reference for Geotechnical Reports





PACIFIC RIM NATIONAL PARK RESERVE

Green

	PROJECT: Geotechnical Assessment Highway No. 4 – Pacific Rim National Park		
	TITLE: Site Location Plan		
	CLIENT: WSP Canada Inc.		
FIGURE NO.: 1	DATE: MARCH 2014	FILE NO.: R714-0308-00	SCALE: NTS




LEGEND:

- APPROXIMATE BOREHOLE LOCATION LEVELTON 2014
- APPROXIMATE BOREHOLE LOCATION LEVELTON 2010

REV. :	DESCRIPTION:	DATE :
		(M/D/YR)

PROJECT:	GEOTECHNICAL ASSESSMENT HIGHWAY NO. 4 - PACIFIC RIM NATIONAL PARK, TOFINO, BC
CLIENT:	WSP CANADA INC.
TITLE:	BOREHOLE LOCATION PLAN - FOR BH14-01, 02, AND 03
THIS DRAWING IS THE SOLE PROPERTY OF LEVELTON CONSULTANTS LTD. AND CANNOT BE USED OR DUPLICATED IN ANY WAY WITHOUT THE EXPRESSED WRITTEN CONSENT OF LEVELTON. THE GENERAL CONTRACTOR SHALL VERIFY ALL DIMENSIONS AND REPORT ANY DISCREPANCIES OR OMISSIONS TO LEVELTON.	

DATE:	MAR 2014
DESIGN BY:	DEK
DRAWN BY:	DEK
CHECKED BY:	TWO
SCALE:	SHOWN
PROJECT No.:	RR14-0308





LEVELTON

FIGURE NO.:
2



LEGEND:

-  APPROXIMATE BOREHOLE LOCATION LEVELTON 2014
-  APPROXIMATE BOREHOLE LOCATION LEVELTON 2010

REV. :	DESCRIPTION:	DATE : (M/D/YR)


PROJECT: GEOTECHNICAL ASSESSMENT HIGHWAY NO 4 - PACIFIC RIM NATIONAL PARK, TOFINO, BC	DATE: MAR 2014	
CLIENT: WSP CANADA INC.	DESIGN BY: DEK	
TITLE: BOREHOLE LOCATION PLAN - BH14-04	DRAWN BY: DEK	
<small>THIS DRAWING IS THE SOLE PROPERTY OF LEVELTON CONSULTANTS LTD. AND CANNOT BE USED OR DUPLICATED IN ANY WAY WITHOUT THE EXPRESSED WRITTEN CONSENT OF LEVELTON. THE GENERAL CONTRACTOR SHALL VERIFY ALL DIMENSIONS AND REPORT ANY DISCREPANCIES OR OMISSIONS TO LEVELTON.</small>	CHECKED BY: TWO	
	SCALE: SHOWN	PROJECT No.: R714-0308
		FIGURE NO.: 3



Photo 1: Condition of road on eastbound lane near Esowista IR #3 (11 February 2014)



Photo 2: Open crack in south shoulder of road near BH14-01 (11 February 2014)


	PROJECT:		Geotechnical Assessment Highway No. 4 – Pacific Rim National Park
	TITLE:		Site Photographs
	CLIENT:		WSP Canada Inc.
PHOTO NOS.: 1 and 2	DATE:	MARCH 2014	FILE NO.: R714-0308-00



Photo 3: Road embankment slope south of BH14-01 (11 February 2014)



Photo 4: View looking east of open crack in road near BH14-02 and BH14-03 (11 February 2014)


	PROJECT:		Geotechnical Assessment Highway No. 4 – Pacific Rim National Park
	TITLE:		Site Photographs
	CLIENT:		WSP Canada Inc.
PHOTO NOS.: 3 and 4	DATE:	MARCH 2014	FILE NO.: R714-0308-00



Photo 5: Road embankment slope south of BH14-01 (11 February 2014)



Photo 6: View looking east of open crack in road near BH14-02 and BH14-03 (11 February 2014)



	PROJECT:		Geotechnical Assessment Highway No. 4 – Pacific Rim National Park
	TITLE:		Site Photographs
	CLIENT:		WSP Canada Inc.
PHOTO NOS.: 5 and 6	DATE:	MARCH 2014	FILE NO.: R714-0308-00



Photo 7: View looking west at road condition near BH14-04 (11 February 2014)



Photo 8: View looking east at road condition near BH14-04 (11 February 2014)

	PROJECT:		Geotechnical Assessment Highway No. 4 – Pacific Rim National Park
	TITLE:		Site Photographs
	CLIENT:		WSP Canada Inc.
PHOTO NOS.: 7 and 8	DATE:	MARCH 2014	FILE NO.: R714-0308-00



Depth (m) (ft)	Description	C	N	Type	Water Level															
						10	20	30	40	50	60	70	80	90						
0	ASPHALT (330mm), ≥ 5 layers.																			
0.5	Compact, dark grey, SAND AND GRAVEL (FILL) , 19mm, crushed, base course.																			
0.5	Loose, black and brown, SAND AND GRAVEL , organic, moist to wet with depth.																			
2	Firm, orange brown, silty, CLAY , trace to some sand lenses.																			
10	- firm, blue grey, wet																			
4	- stiff.																			
15																				
20																				
25																				
30																				
30	Bottom of hole at 9.1 metres																			
10																				
35																				
40																				
45																				

C: Condition of Sample
 Good
 Disturbed
 No Recovery

Type: Type of Sampler
 SPT : 2 in. standard
 S : Shelby
 FP : Fixed Piston
 G : Grab
 CORE

N: Number of Blows
 WH : Weight of Hammer
 WR : Weight of Rod
 Standard Penetration Test : ASTM D1586
 Hammer Type:
 DYNAMIC CONE PENETRATION TEST:

● Moisture Content %
 ▲ Plastic Limit
 ▼ Liquid Limit
 ▽ Ground Water Level
 ⊗ Shear strength in kPa (Torvane or Penetrometer)
 ⊗ Shear strength in kPa (Unconfined)
 ⊗ Shear strength in kPa (field vane)
 ⊗ Remolded strength in kPa
 ■ Percent Passing # 200 sieve

Drill Method:
 Solid Stem Auger / DCPT
 Date Drilled: 23/01/2014
 By: RH

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1 LOG PER PAGE R714-0308-00.GPJ LEVELTON.GDT 12/3/14



Depth (m) (ft)	Description	C	N	Type	Water Level	SPT Blow Count									
						10	20	30	40	50	60	70	80	90	
0.0 - 0.5	ASPHALT (180mm), ≥ 4 layers. Compact, dark grey, SAND AND GRAVEL (FILL), crushed, 19mm.					- Hand excavated									
0.5 - 1.0	Compact, grey, SAND AND GRAVEL (FILL), pit run, moist.														
1.0 - 1.5	Loose, black, SAND AND GRAVEL, organic, wet.			G											
1.5 - 2.0	Loose, black, SAND AND GRAVEL, midden-like, organic, wet.			G											
2.0 - 3.0	Loose, black, SAND, some gravel, wet.			G											
3.0 - 3.7	- layer of gravel/cobble at 3.7 to 4.0m.														
3.7 - 4.0	Firm, grey, silty, CLAY, trace sand and gravel, moist.			G											
4.0 - 6.1	Bottom of hole at 6.1 metres														

C: Condition of Sample Good Disturbed No Recovery	Type: Type of Sampler SPT : 2 in. standard S : Shelby FP : Fixed Piston G : Grab CORE	N: Number of Blows WH : Weight of Hammer WR : Weight of Rod Standard Penetration Test : ASTM D1586 Hammer Type:	● Moisture Content % ▲ Plastic Limit ▼ Liquid Limit ▽ Ground Water Level Shear strength in kPa (Torvane or Penetrometer) Shear strength in kPa (Unconfined) Shear strength in kPa (field vane) Remolded strength in kPa Percent Passing # 200 sieve	DYNAMIC CONE PENETRATION TEST: Blow count no. of blows of a 140 lb (64 kg) hammer dropped 30in. (750mm) to produce 12in (300mm) of a 2in (50mm) diameter cone.	Drill Method: Solid Stem Auger / DCPT Date Drilled: 23/01/2014 By: RH
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1 LOG PER PAGE R714-0308-00.GPJ LEVELTON.GDT 12/3/14



Depth (m) (ft)	Description	C	N	Type	Water Level	Dynamic Cone Penetration Test														
						10	20	30	40	50	60	70	80	90						
0																				
5																				
10																				
4																				
15																				
6																				
20																				
8																				
25																				
10																				
35																				
12																				
40																				
45																				

BH14-03 next to BH14-02
 - likely gravel layering from 3.0 to 4.3m

C: Condition of Sample

- Good
- Disturbed
- No Recovery

Type: Type of Sampler

- SPT : 2 in. standard
- S : Shelby
- FP : Fixed Piston
- G : Grab
- CORE

N: Number of Blows

- WH : Weight of Hammer
- WR : Weight of Rod
- Standard Penetration Test : ASTM D1586
- Hammer Type:

DYNAMIC CONE PENETRATION TEST:
 Blow count no. of blows of a 140 lb (64 kg) hammer dropped 30in. (750mm) to produce 12in (300mm) of a 2in (50mm) diameter cone.

- Moisture Content %
- ▲ Plastic Limit
- ▼ Liquid Limit
- ▽ Ground Water Level
- ⊗ Shear strength in kPa (Torvane or Penetrometer)
- ⊗ Shear strength in kPa (Unconfined)
- ⊗ Shear strength in kPa (field vane)
- ⊗ Remolded strength in kPa
- Percent Passing # 200 sieve

Drill Method: DCPT
 Date Drilled: 23/01/2014
 By: RH

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Depth (m) (ft)	Description	C	N	Type	Water Level	Soil Properties									
						10	20	30	40	50	60	70	80	90	
0.0 - 0.5	ASPHALT (180mm), ≥ 3 layers.			G		Hand excavated									
0.5 - 1.0	Compact, dark grey, SAND AND GRAVEL (FILL), crushed, 19mm.			G											
1.0 - 1.3	Compact, brown, SAND AND GRAVEL (FILL), pit run, moist. - filter cloth (grey and white) observed at 1.3m.			G											
1.3 - 1.6	Firm to stiff, grey, silty, CLAY, some wood debris sizes to 25mm diameter, some organic, moist. - trace shells observed at 1.6m depth			G											
1.6 - 4.0	- blue grey, trace sand and gravel, moist			G											
4.0 - 15.0	- yellow brown, trace gravel, moist			G											
15.0 - 25.0	- blue grey, occasional gravel sizes to 25mm diameter.			G											
25.0 - 7.6	Bottom of hole at 7.6 metres			G											

C: Condition of Sample

- Good
- Disturbed
- No Recovery

Type: Type of Sampler

- SPT : 2 in. standard
- S : Shelby
- FP : Fixed Piston
- G : Grab
- CORE

N: Number of Blows

- WH : Weight of Hammer
- WR : Weight of Rod
- Standard Penetration Test : ASTM D1586
- Hammer Type:

DYNAMIC CONE PENETRATION TEST:

Blow count no. of blows of a 140 lb (64 kg) hammer dropped 30in. (750mm) to produce 12in (300mm) of a 2in (50mm) diameter cone.

- Moisture Content %
- ▲ Plastic Limit
- ▼ Liquid Limit
- ▽ Ground Water Level
- ⊗ Shear strength in kPa (Torvane or Penetrometer)
- ⊗ Shear strength in kPa (Unconfined)
- ⊗ Shear strength in kPa (field vane)
- ⊗ Remolded strength in kPa
- Percent Passing # 200 sieve

Drill Method:

Solid Stem Auger / DCPT

Date Drilled: 23/01/2014

By: RH

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Levelton Consultants Ltd.

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 Canada V9N 7C8
 Tel.: 250-334-9222
 Fax.: 250-334 3955
 E-mail: courtenay@levelton.com

AGGREGATE GRADATION ANALYSIS

IDENTIFICATION:

Client Genivar
 Project Highway 4, Slope Review - Pacific Rim National Park, BC
 Sample Location BH14-01 @ 0.3 to 1.2m depth

File No: R714-0308-00
 Report No.: 1
 Date: 27-Feb-14

SAMPLING INFORMATION:

Material: Organic Sand, fine to medium grained, trace gravel, some silt
Specification: Gradation

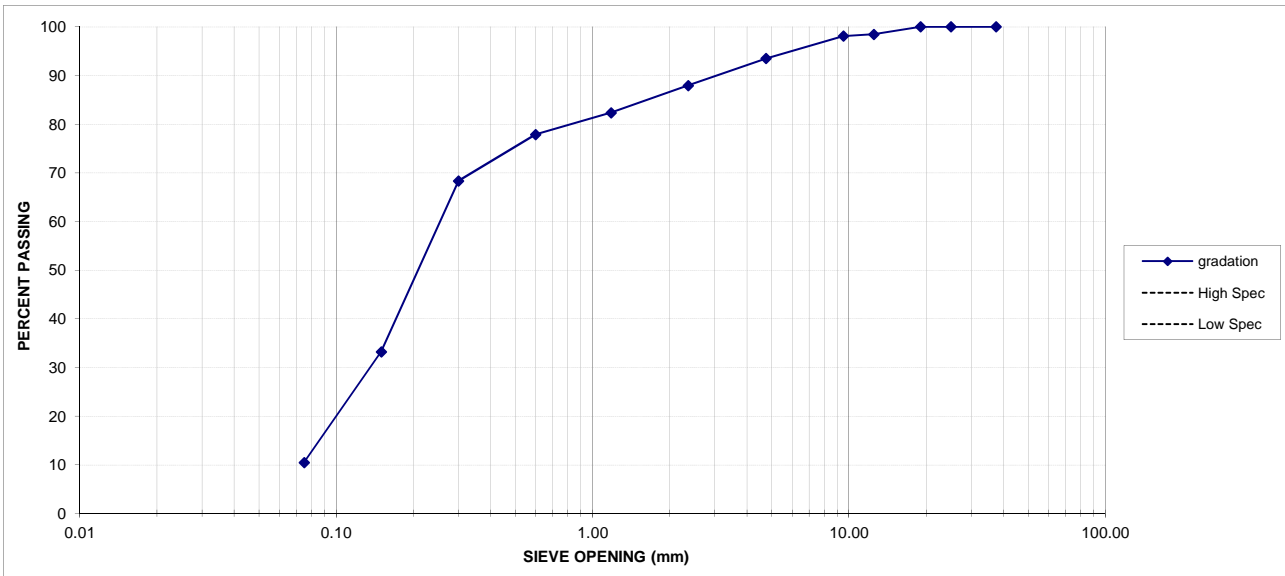
Material Specification
 Sieve High Spec Low Spec

Sieve Analysis
 Sieve % Passing

Date Sampled 21-Feb-14
Date Tested 27-Feb-14
Sample No.: 1
Fracture: na
Supplier: LCL
Sampled by: RH
Tested by: RH

Sieve	% Passing
37.5	100.0
25	100.0
19	100.0
12.5	98.5
9.50	98.1
4.75	93.5
2.36	87.9
1.18	82.4
0.600	77.9
0.300	68.4
0.150	33.3
0.075	10.5

AGGREGATE GRADATION:



REMARKS: Tested in accordance with ASTM C- 136 and C-117
Wood Debris observed to be approximately 50%
by volume retained on the 2.36mm sieve.

REPORTS TO: _____

LEVELTON CONSULTANTS LTD.

per: _____



LEVELTON

Sewer and Lift Stations Tofino, BC Geotechnical Assessment

BH10-07

Pg 1 of 1

Project No: V/10-1223-00

Depth		Description	C	N	Type	Water Level	10 20 30 40 50 60 70 80 90														
(m)	(ft)																				
		ASPHALT																			
		Compact, grey, SAND AND GRAVEL (FILL), occasional cobble.																			
	2	Loose, VARIOUS FILL, some sand and gravel, some silt, moist.																			
	4	ORGANIC SILT , moist. - lots of wood debris observed			G																
	6	- some gravel observed below 1.5m - wet below 1.5m depth.																			
	8				G																
	10	Bottom of hole at 3.1 metres																			
	12																				
	14																				
	16																				
	18																				
	20																				
	22																				
	24																				

1 LOG PER PAGE: V/10-1223-00.GPJ LEVELTON.GDT 8/19/10

C: Condition of Sample Good Disturbed No Recovery	Type: Type of Sampler SPT : 2 in. standard S : Shelby FP : Fixed Piston G : Grab CORE	N: Number of Blows WH : Weight of Hammer WR : Weight of Rod Standard Penetration Test : ASTM D1586 Hammer Type : Trip Hantzner	● Moisture Content % ▽ Plastic Limit ▲ Liquid Limit ▼ Ground Water Level ⊗ Shear strength in kPa (Torsion or Penetrometer) X Shear strength in kPa (Unconfined) ⊙ Shear strength in kPa (field vane) ⊠ Remolded strength in kPa ⊞ Percent Passing # 200 sieve	Drill Method: Solid Stem Auger / DCPT Date Drilled: 7/23/2010 By: RH

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Sewer and Lift Stations
Tofino, BC
Geotechnical Assessment

BH10-17

Pg 1 of 1

Project No: V110-1223-00

Depth		Description	C	N	Type	Water Level																						
(m)	(ft)						10	20	30	40	50	60	70	80	90													
		Compact, SAND AND GRAVEL (FILL) , road base to subbase, moist.																										
2		Dense, grey, SAND , medium to fine grained, trace to some gravel, moist. - wet below 2.0m - gravel content increases with depth.			G																							
4																												
6																												
8																												
10																												
12																												
14																												
16																												
18																												
20																												
22																												
24																												
		Bottom of hole at 3.1 metres																										

1 LOG PER PAGE V110-1223-00.GPJ LEVELTON.GOT 8/19/10

<p>C: Condition of Sample Good Disturbed No Recovery </p>	<p>Type: Type of Sampler SPT : 2 In. standard S : Shelby FP : Fixed Piston G : Grab CORE</p>	<p>N: Number of Blows WH : Weight of Hammer WR : Weight of Rod Standard Penetration Test : ASTM D1586 Hammer Type: Trip Hammer</p>	<p> Moisture Content % Plastic Limit Liquid Limit Ground Water Level Shear strength in kPa (Torvane or Penetrometer) Shear strength in kPa (Unconfined) Shear strength in kPa (field vane) Remolded strength in kPa Percent Passing # 200 sieve </p>	<p>Drill Method: Solid Stem Auger Date Drilled: 7/22/2010 By: RH</p>
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


Sewer and Lift Stations
Tofino, BC
Geotechnical Assessment

BH10-20

Pg 1 of 1

Project No: V110-1223-00

Depth		Description	C	N	Type	Water Level	Soil Properties														
(m)	(ft)						10	20	30	40	50	60	70	80	90						
0	0	Compact, SAND AND GRAVEL (VARIOUS FILL), road base and subbase, trace to some silt, moist.																			
2	2	Soft to firm, mottled orange brown, SILT, trace gravel, moist.																			
4	4	Firm, orange brown, silty, CLAY, trace sand and gravel.																			
6	6																				
8	8	- firm, blue grey, trace to some gravel, moist at 2.5m.																			
10	10	- increased plasticity content below 3.0m - trace to some sand below 3.0m depth.																			
12	12	Bottom of hole at 3.7 metres.																			
14	14																				
16	16																				
18	18																				
20	20																				
22	22																				
24	24																				

<p>C: Condition of Sample Good  Disturbed  No Recovery </p>	<p>Type: Type of Sampler SPT : 2 in. standard S : Shelby FP : Fixed Piston G : Grab CORE</p>	<p>N: Number of Blows WH : Weight of Hammer WR : Weight of Rod Standard Penetration Test : ASTM D1586 Hammer Type : Trip Hammer DYNAMIC CONE PENETRATION TEST: Blow count no. of blows of a 140 lb (64 kg) hammer dropped 30in. (750mm) to produce 12in (300mm) of a 2in (50mm) diameter cone.</p>	<p>Moisture Content % Plastic Limit Liquid Limit Ground Water Level Shear strength in kPa (Torvane or Penetrometer) Shear strength in kPa (Unconfined) Shear strength in kPa (field vane) Remolded strength in kPa Percent Passing # 200 sieve</p>	<p>Drill Method: Solid Stem Auger / DCPT Date Drilled: <u>7/22/2010</u> By: <u>RH</u></p>

1 LOG PER PAGE V110-1223-00.GPJ LEVELTON.GDT 8/19/10



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Sewer and Lift Stations
Tofino, BC
Geotechnical Assessment

BH10-21

Pg 1 of 1

Project No: V110-1223-00

Depth (m) (ft)	Description	C	N	Type	Water Level	SPT														
						10	20	30	40	50	60	70	80	90						
0 - 2	Compact to dense, brown, SAND AND GRAVEL (FILL) , roadbase/subbase, occasional cobble sizes to 100mm diameter.																			
2 - 6	Firm to stiff, mottled orange brown/grey, SILT , trace sand, occasional gravel sizes to 50mm diameter, moist.																			
6 - 10	-stiff, greenish/blue, trace to some sand, moist.																			
10 - 12	Compact to dense, blue grey, silty, SAND AND GRAVEL , numerous gravel sizes to 25mm diameter, wet.																			
12 - 14	Bottom of hole at 4.0 metres																			
14 - 24																				

PP @ 1.2m = 2.0 tsf
 PP @ 1.5m = 2.0 tsf
 PP @ 1.8m = 1.0 tsf
 PP @ 2.1m = 1.5 tsf

1. LOG PER PAGE: V110-1223-00.GPJ LEVELTON.GDT 8/19/10

C: Condition of Sample Good Disturbed No Recovery	Type: Type of Sampler SPT : 2 in. standard S : Shelby FP : Fixed Piston G : Grab CORE	N: Number of Blows WH : Weight of Hammer WR : Weight of Rod Standard Penetration Test : ASTM D1586 Hammer Type: Trip Hammer DYNAMIC CONE PENETRATION TEST: Blow count no. of blows of a 140 lb (64 kg) hammer dropped 30in. (750mm) to produce 12in (300mm) of a 2in (50mm) diameter cone.	Moisture Content % Plastic Limit Liquid Limit Ground Water Level Shear strength in kPa (Torvane or Penetrometer) Shear strength in kPa (Unconfined) Shear strength in kPa (field vane) Remolded strength in kPa Percent Passing # 200 sieve	Drill Method: Solid Stem Auger / DCPT Date Drilled: 7/22/2010 By: RH
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