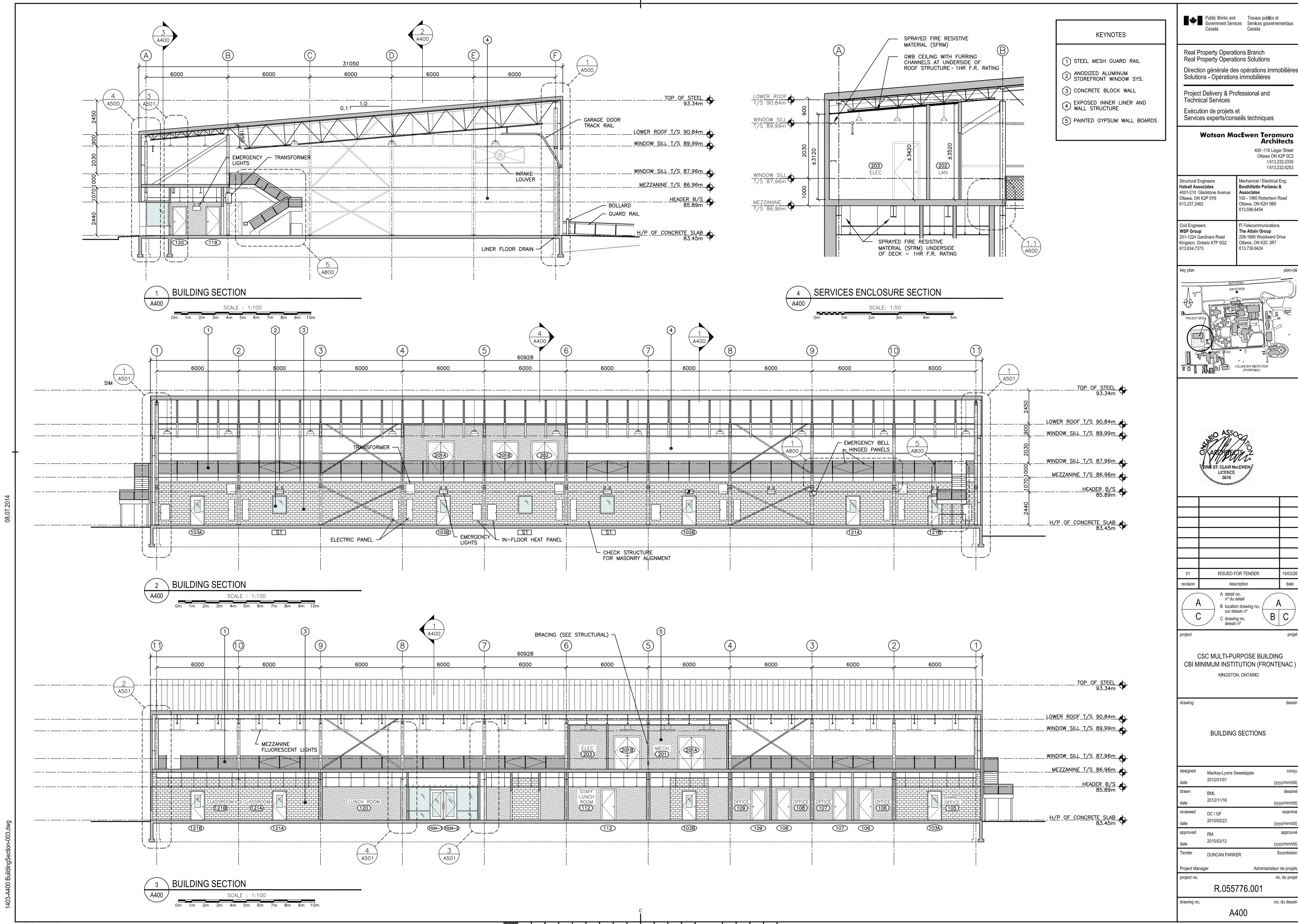


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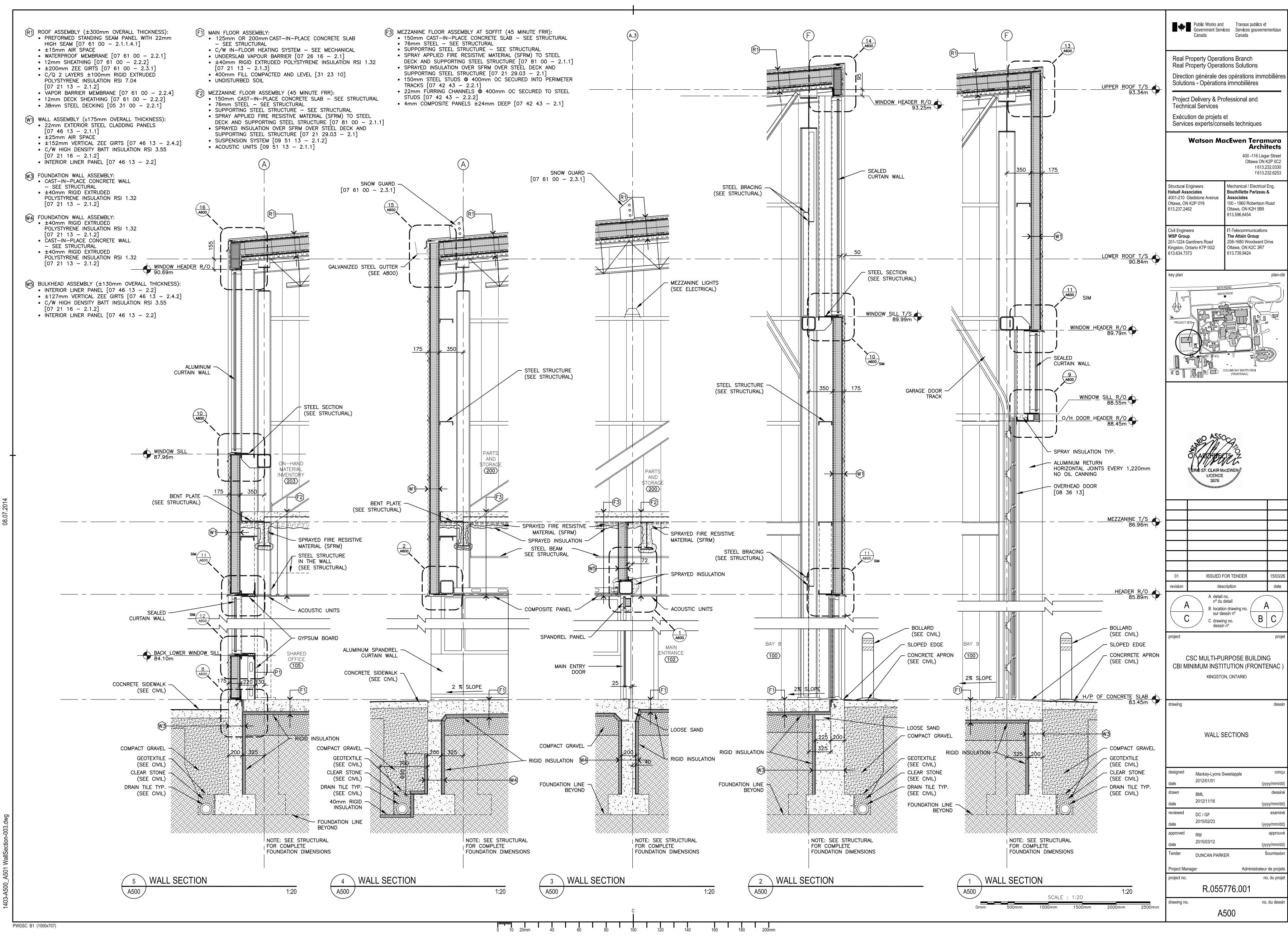


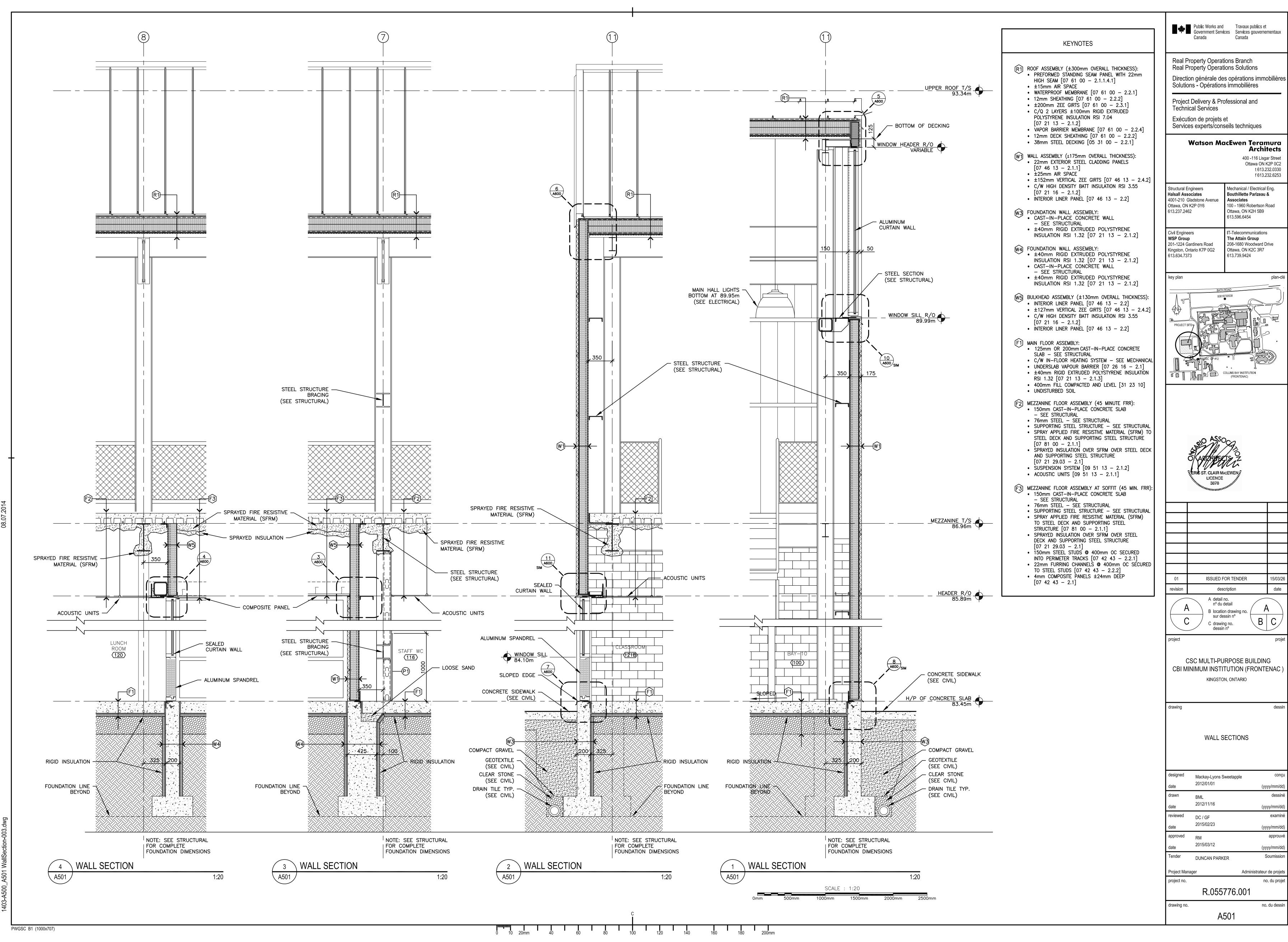


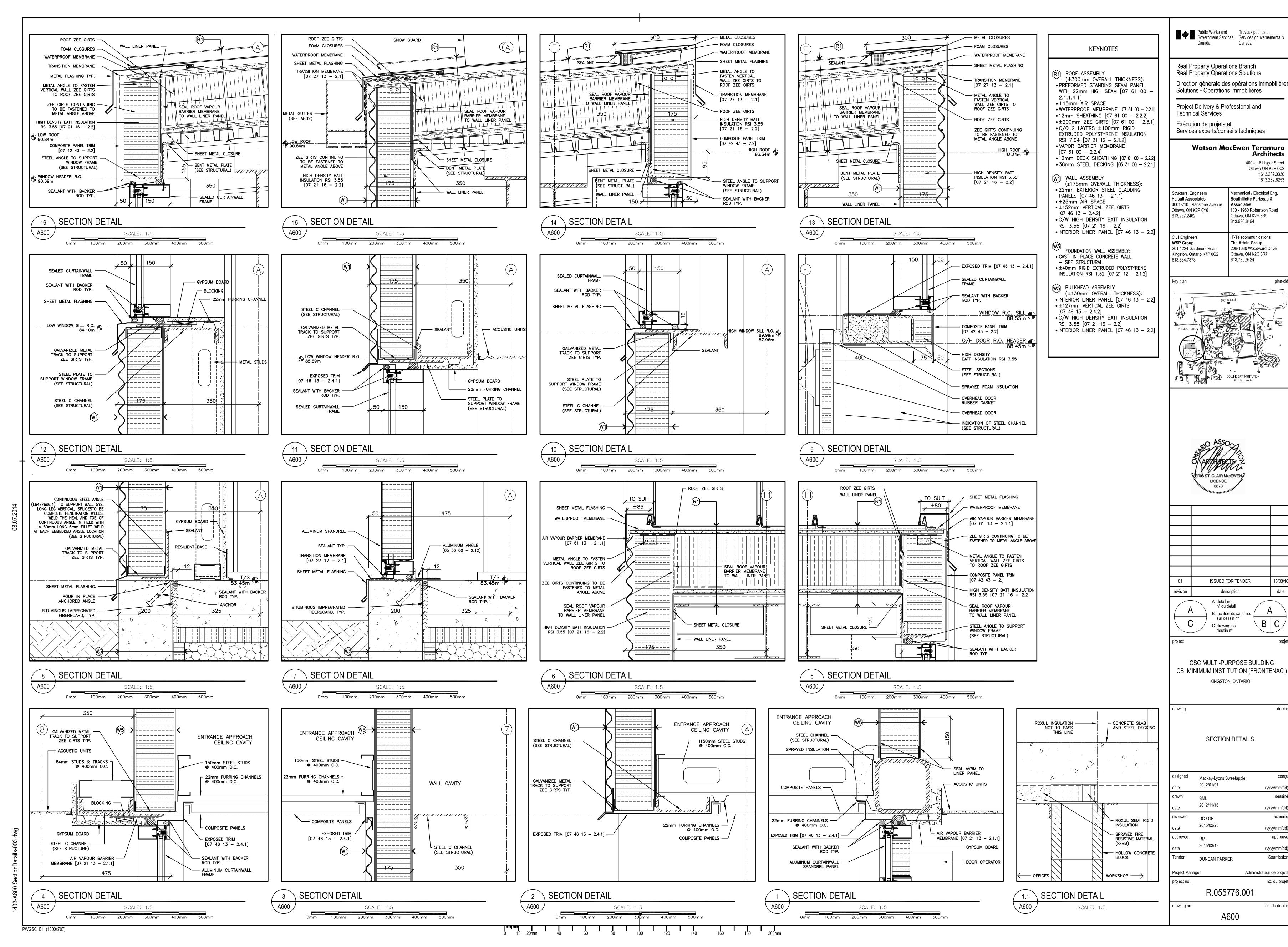
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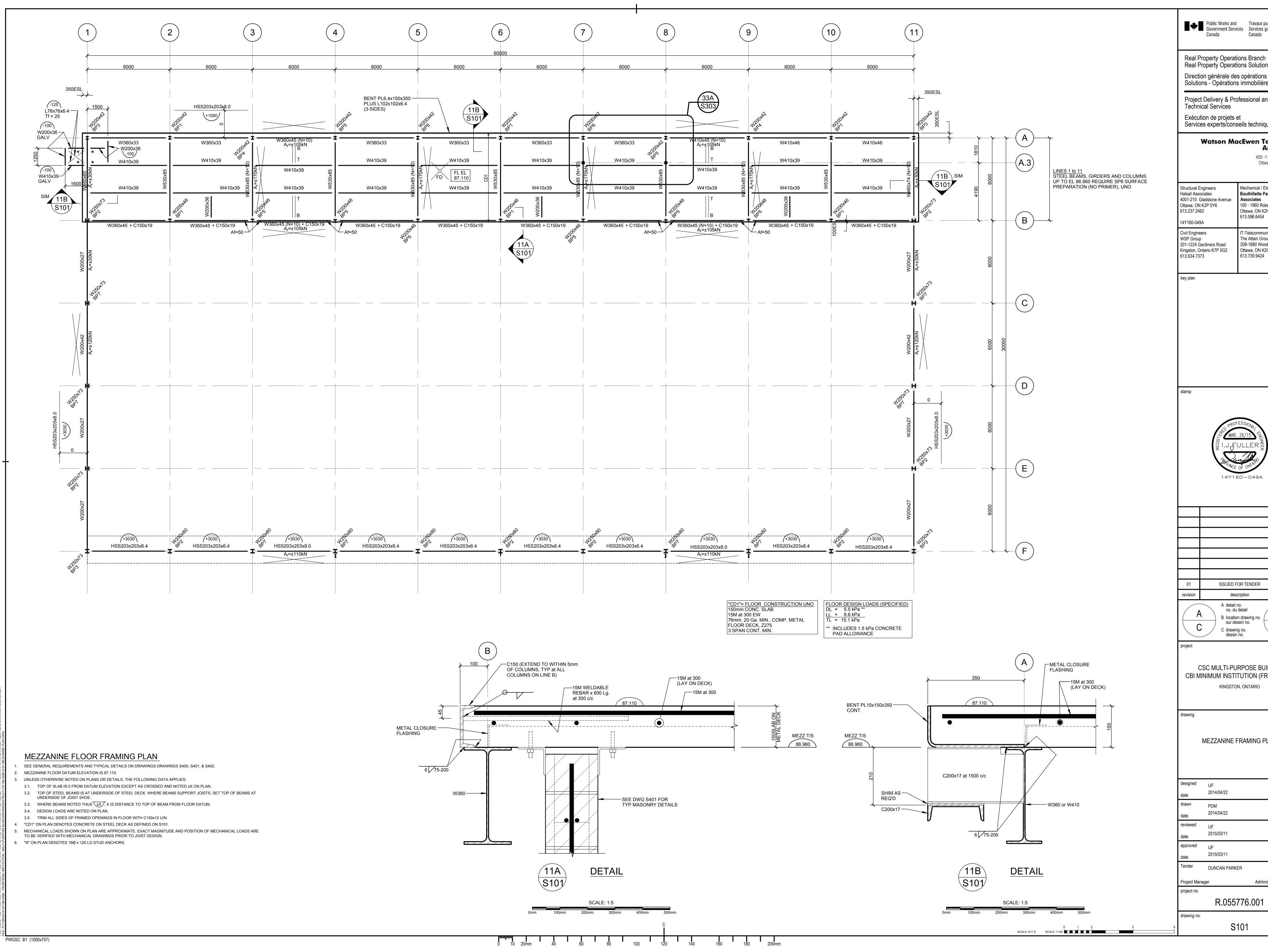




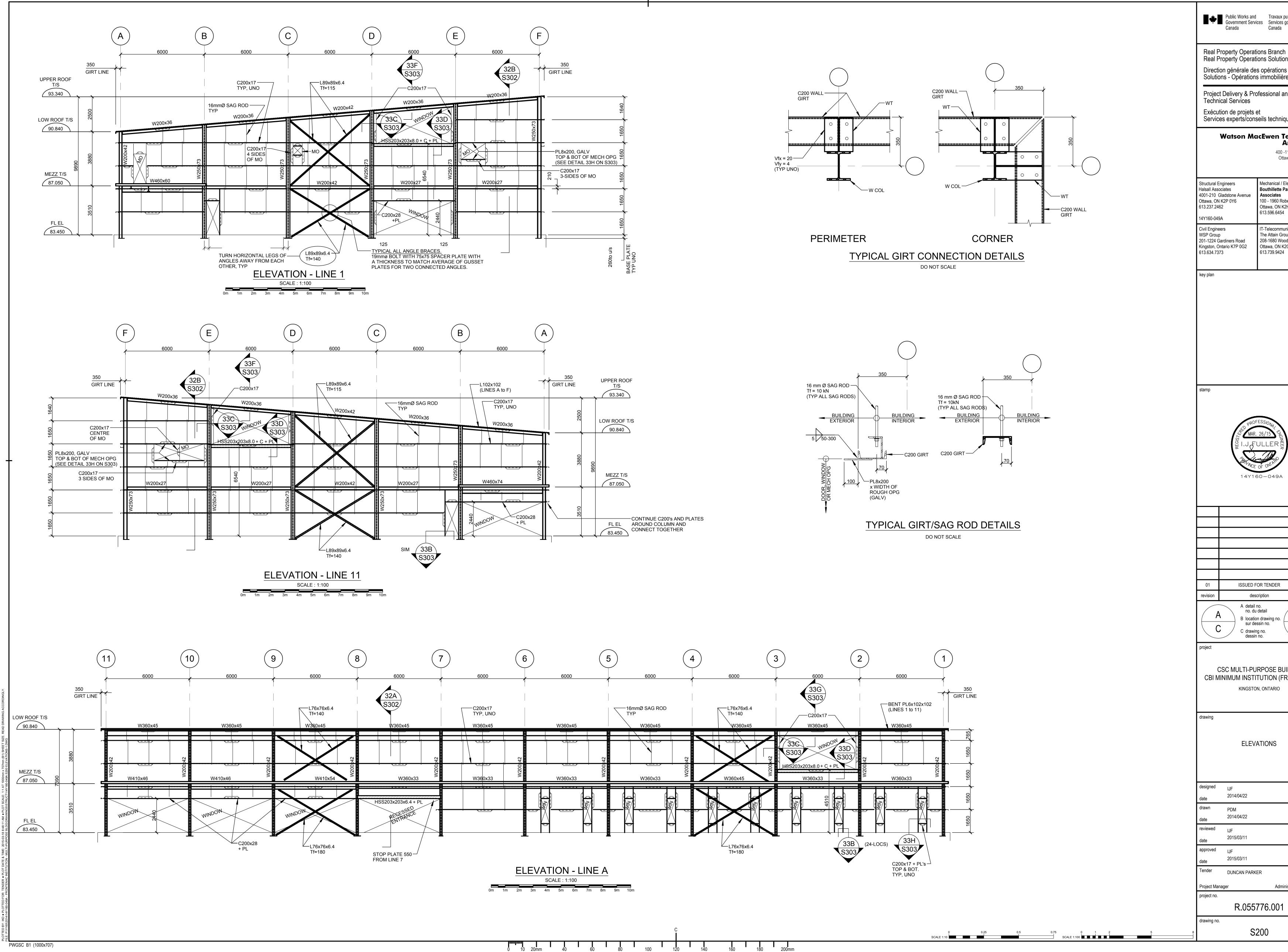




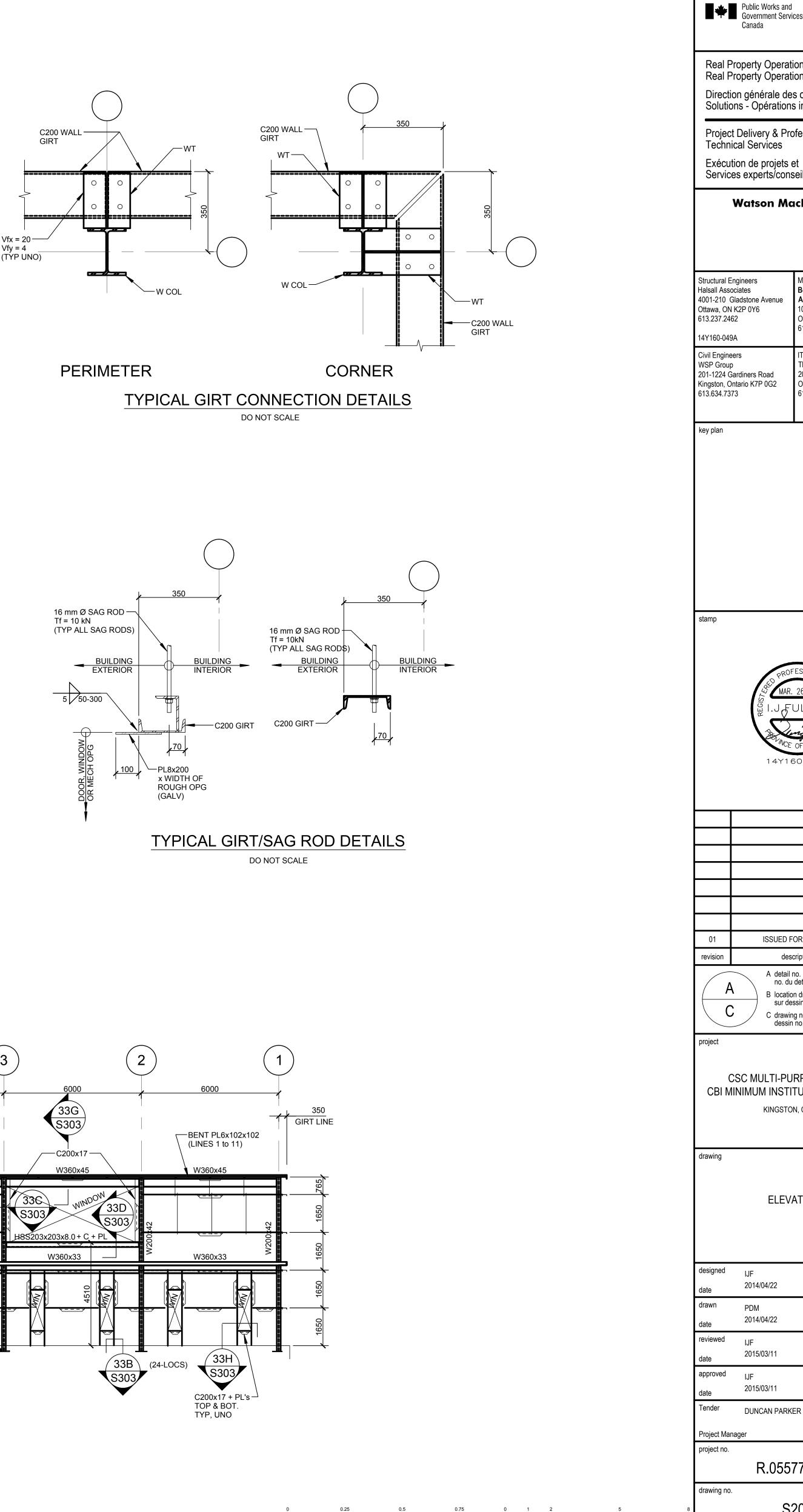


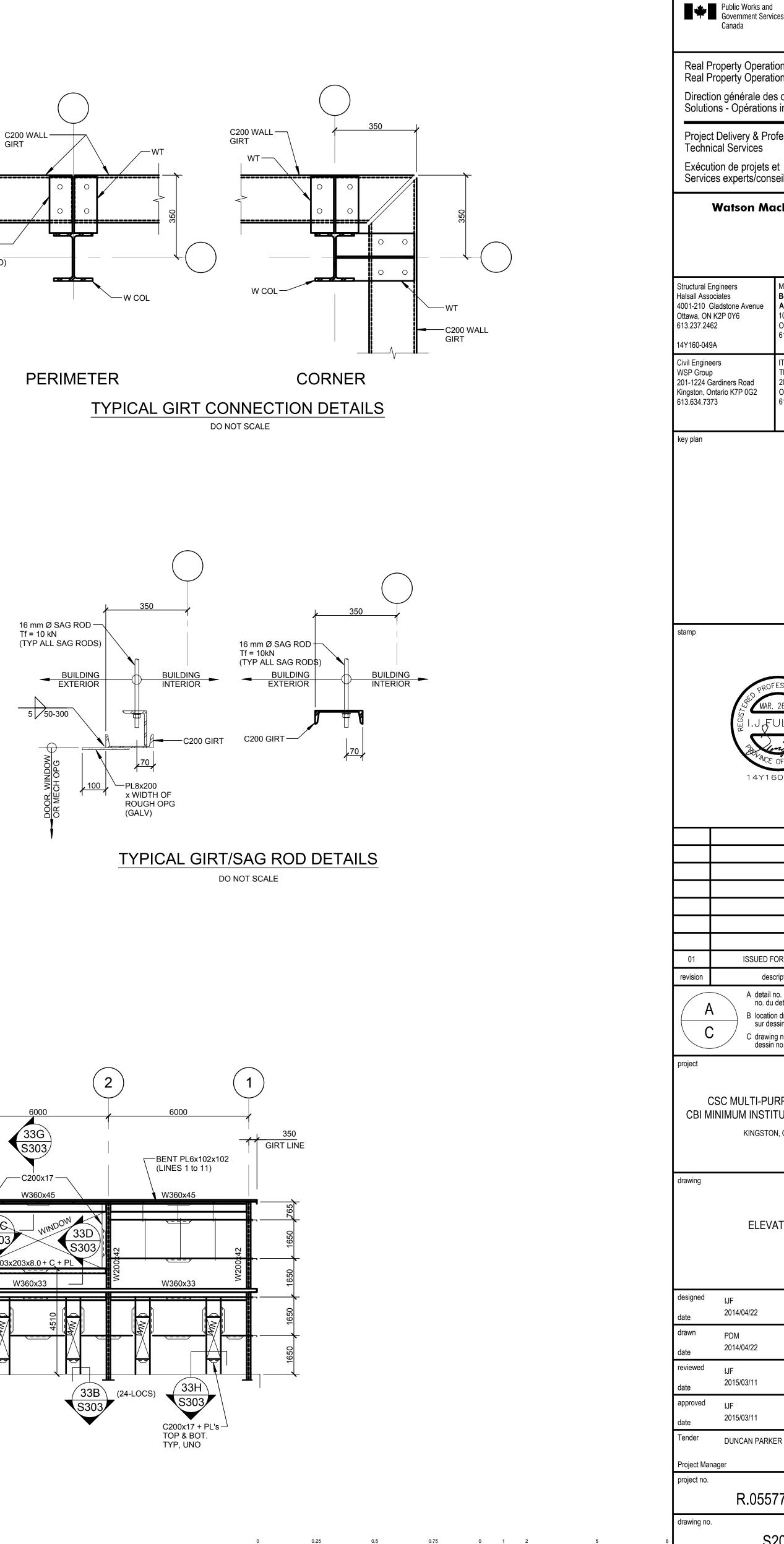


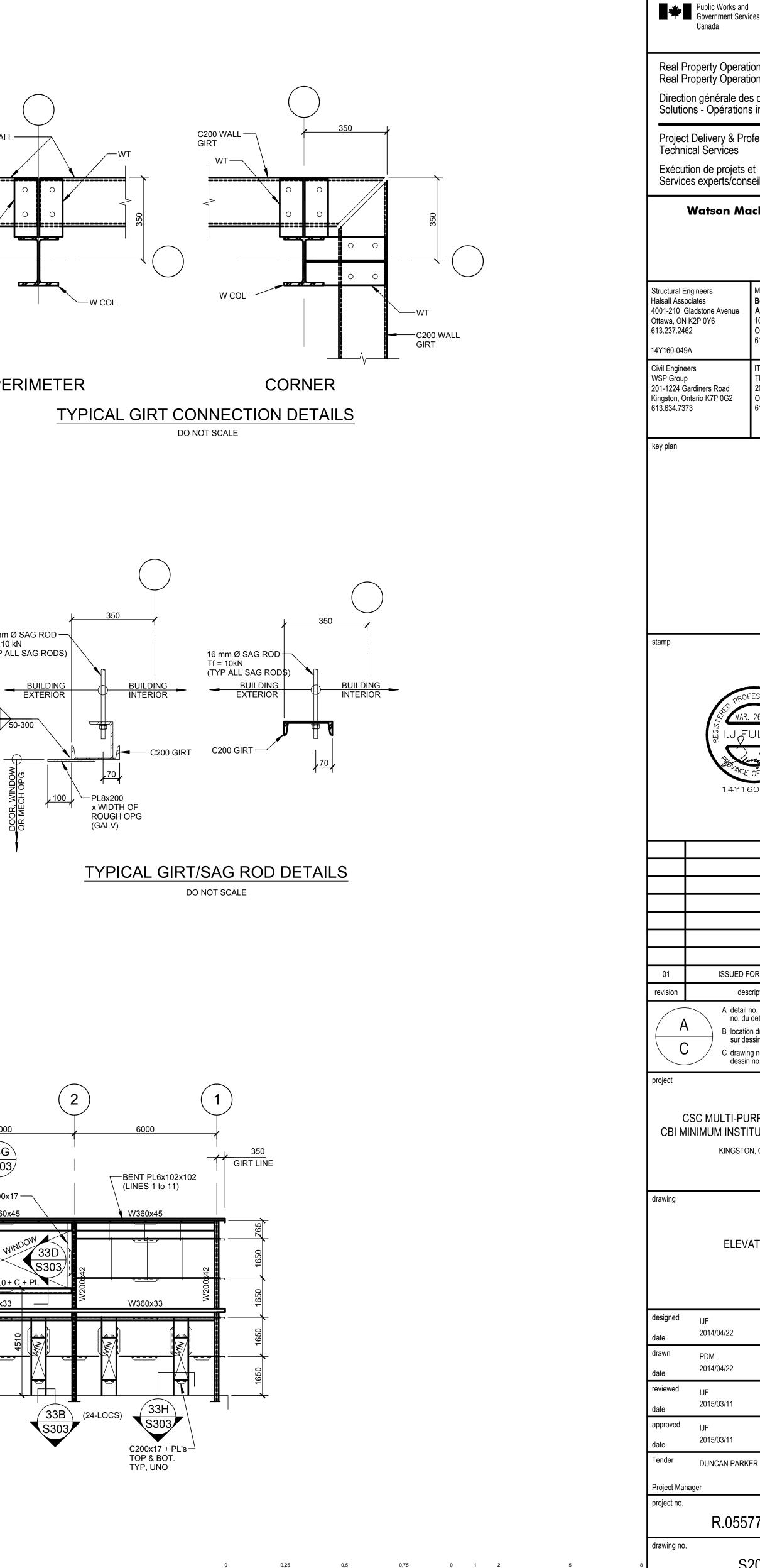
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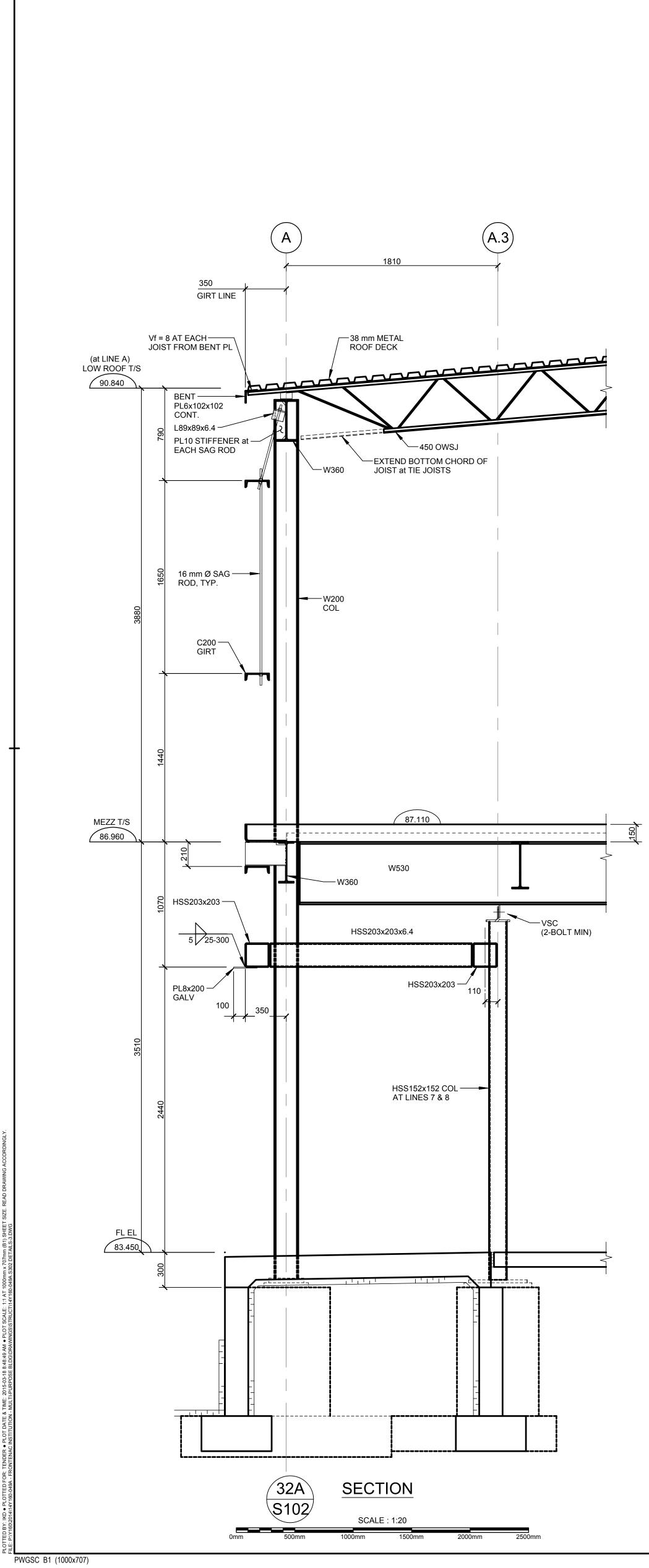
PWGSC B1 (1000x707)

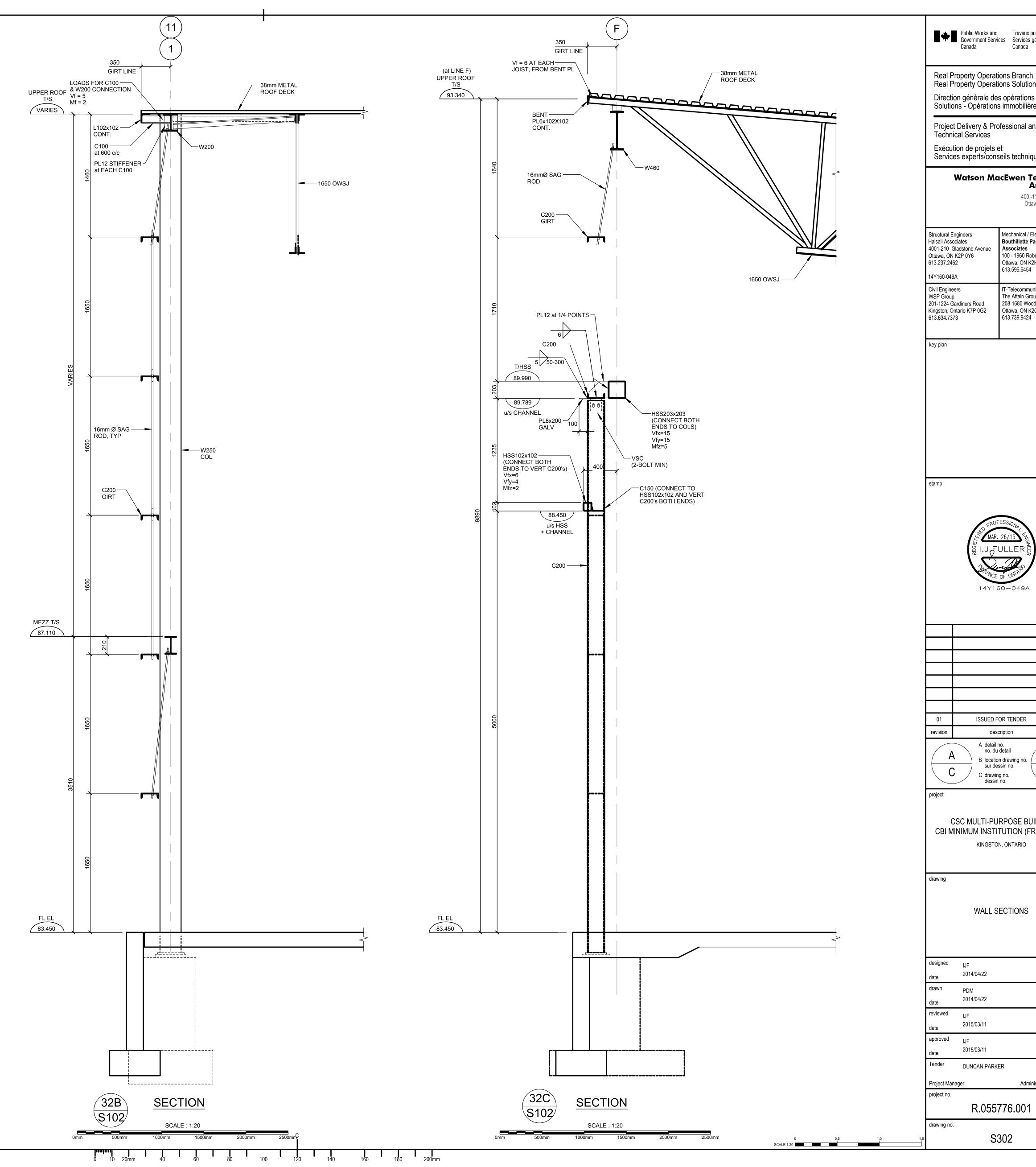






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	GENERAL NOTES		MATERIAL AND DESIGN DATA
-	(NBCC2010) INCLUDING AMENDMENTS.		 FOOTING BEARING RESISTANCE: kPa AT ULS (ULTIMATE LIMIT STATES DESIGN) 150 kPa AT SLS (SERVICEABILITY LIMIT STATES DESIGN)
2		RAL DRAWINGS WITH THE ARCHITECTURAL DRAWINGS. REPORT EEDING WITH THE WORK. DO NOT SCALE THESE DRAWINGS. ALL	MODULUS OF SUBGRADE REACTIONS (ASSUMED FOR DESIGN OF SLABS ON SEE SOILS REPORT PREPARED BY: DBA ENGINEERING LTD.
3		VALLS AND COLUMNS BELOW THE FLOOR OR ROOF STRUCTURE JMNS ABOVE THE FLOOR ARE SHOWN WITH CONTINUOUS LINES.	 CONCRETE SPECIFIED COMPRESSIVE STRENGTH, fc, IS 25 MPa EXCEPT FOR
4	THAN ACTUAL CONDITIONS FOR THIS F		DOCKING AREA - 35 MPa SLAB ON GRADE - 30 MPa AND WHERE SHOWN ON PLANS AND SCHEDULES.
5		TA CAPABLE OF SUPPORTING THE DESIGN BEARING PRESSURES NOT LESS THAN REQUIRED TO PROVIDE A MINIMUM OF 1500	INCREASE STRENGTH AS REQUIRED FOR REQUIRED CLASS OF EXPOSURE, 3. REINFORCING STEEL: CAN/CSA G30.18M - GRADE 400R 400W
6	PROTECT FOOTINGS, WALLS, SLABS-OF ACTION AT ALL TIMES DURING CONSTR	N-GRADE AND ADJACENT SOIL AGAINST FREEZING AND FROST RUCTION.	4. STRUCTURAL STEEL (EXCEPT HSS): CAN/CSA G40.21M - WIDE FLANGES: 350 W
7	EXCEED A RISE OF 7 IN A RUN OF 10.	INT EXCAVATIONS FOR FOOTINGS OR TRENCHES SHALL NOT	- ANCHOR RODS: 300 W - ALL OTHER STEEL: 300 W
8 9		OF 1200 APART. MAXIMUM STEP APPROXIMATELY 600. CENTROID OF COLUMNS, UNLESS OTHERWISE NOTED.	 STRUCTURAL STEEL (HSS ONLY): ASTM A500 GRADE C (345 MPa FOR SQUARE/RECTANGULAR AND 317 MPa G40.21 GRADE 350W CLASS C OR H HSS MEMBERS REQUIRED TO BE GALVANIZED SHALL BE CLASS H, OR ST
1		TAINING EARTH UNTIL ELEMENTS PROVIDING LATERAL SUPPORT, PLETED. PLACE BACKFILL SIMULTANEOUSLY ON BOTH SIDES OF	 ALVANIZING STRUCTURAL MASONRY:
1	SHOWN ON THESE DRAWINGS. LEAVE	N CONCRETE WALLS ARE NOT PERMITTED, EXCEPT WHERE CHASES AND POCKETS IN WALLS FOR SEATING OF SLABS AND	 HOLLOW BLOCK: CSA A165.1 - H/15/A/M SOLID BLOCK: CSA A165.1 - S/15/A/M MORTAR: CSA A179M - TYPE S
1	BEAMS. 2. REINFORCEMENT FOR CONCRETE WAL FOLLOWS:	LS NOT COVERED BY SECTION, PLAN OR SCHEDULE SHALL BE AS	 GROUT FOR BLOCK CORES: CSA A179M - COARSE GROUT 1:3:2 CEMENT:SAND:PEA-STONE BY VOLUME WITH 200 SLUMP SPECIFIED COMPRESSIVE STRENGTH, fm, IS:
	200 MAXIMUM WALL: 10 @ 500 H	H + 10 @ 400 V IN CENTRE HEF + 10 @ 500 VEF	HOLLOW BLOCK - 9.8 MPa SOLID AND GROUTED HOLLOW BLOCK - 7.5 MPa - SPECIFIED FLEXURAL TENSILE STRENGTH ft (NORMAL TO BED JOINTS) IS
	300 MAXIMUM WALL: 10 @ 300 H	HEF + 10 @ 500 VEF HEF + 10 @ 400 VEF HEF + 15 @ 400 VEF	SOLID AND HOLLOW BLOCK - 0.4 MPa GROUTED HOLLOW BLOCK - 0.65 MPa
1	 REINFORCEMENT FOR CONCRETE CUR DOWELS + 2-10H. 	RBS NOT COVERED BY SECTION OR PLAN SHALL BE 10@400	 DESIGN LOADS FOR BUILDING STRUCTURE: DESIGN LOADS PRESENTED BELOW HAVE BEEN DEVELOPED FOR THE REF LOCATED IN THE FOLLOWING MUNICIPALITY: KINGSTON, ON
	SHALL BE 10@300 EA. WAY PLACED 50r		THE VALUES FOR CLIMATIC DATA USED IN THE DETERMINATION OF DESIG OBTAINED FROM: <u>THE SUPPLEMENTARY STANDARD SB-1 TABLE 1.2</u>
	CLASS B LAPS.	E TERMINATED IN STANDARD HOOKS AT ENDS AND SPLICED USING	.1 GRAVITY LOADS AS SHOWN ON PLANS
	 ALL REBAR HOOKS TO BE STANDARD L PROVIDE CONTINUOUS GALVANIZED VI CONCRETE SURFACES WITH MASONRY 	ERTICAL DOVETAIL ANCHOR SLOTS AT 600 CENTRES IN ALL	.2 GROUND SNOW LOAD AND ASSOCIATED RAIN LOAD: Ss = 2.1 kN/m^2 Sr = 0.4 kN/m^2
1	8. STANDARD LINTELS:		SPECIFIED SNOW LOAD S = Is [Ss x Cb x Cw x Cs x Ca + Sr] = Is x [$2.1x0.8x1.0x1.0x1.0+0.4$
	TYPICAL DETAILS. CHECK ARCHITECTL REQUIRING STANDARD LINTELS WHICH	L OPENINGS IN MASONRY WALLS AND PARTITIONS AS SHOWN ON JRAL, MECHANICAL AND ELECTRICAL DRAWINGS FOR OPENINGS I ARE NOT NECESSARILY SHOWN ON THE STRUCTURAL	ULS SLS: Is = 1.0 Is = 0.9 S = 2.08 kN/m ² S = 1.87 kN/m ²
	DRAWINGS. SPECIAL LINTELS:		.3 24 HOUR RAINFALL: 108 mm .4 WIND:
1	9. UNLESS OTHERWISE NOTED, PROVIDE	TEL SCHEDULE AT LOCATIONS GIVEN ON PLAN. A CONTINUOUS BOND BEAM AT TOPS OF ALL WALLS. FILL ALL	IMPORTANCE CATEGORY = NORMAL
-	CONTINUOUS.	0 MPa CONCRETE REINFORCED WITH 1-10 TOP AND BOTTOM	$\frac{\text{IMPORTANCE FACTOR:}}{\text{Iw} = 1.00 \text{ (ULS)}}$ $\text{Iw} = 0.75 \text{ (SLS)}$
2	CONCRETE SLABS SHALL HAVE A MININ AND JOISTS SHALL BE PREFILLED WITH	MUM BEARING OF 100. VOIDS IN MASONRY UNITS UNDER BEAMS I GROUT FOR A MINIMUM VERTICAL DEPTH OF 600 AND A LENGTH ISE 75% SOLID BLOCKS FOR FILLING. DO NOT USE MORTAR TO FILL	$\frac{1/50 \text{ Yr HOURLY WIND PRESSURE:}}{q} = 0.47 \text{ kPa}$
2	MASONRY UNITS.	ORCING BARS, CLOSEST TO THE CONCRETE SURFACE, IN mm,	TERRAIN TYPE: OPEN ROUGH
	UNLESS OTHERWISE NOTED: FOR CONCRETE EXPOSURE CLASSES I FOOTINGS 75 TO BOT	N, F1 AND F2: ITOM BARS, 50 TO TOP BARS	H = MAX HEIGHT ABOVE GRADE = 8.64 m Ds = SMALLER PLAN DIMENSION = 30.0 m
	PIERS 50 COLUMNS 40	RFACES EXPOSED TO GROUND OR OUTSIDE,	^H ∕ _{Ds} = 8.64/30.0 = 0.288 CONCLUSION: BUILDING IS: LOW RISE
	THE BUILD SLABS 25 TO PRO	DTECTED SURFACES (ENTIRELY WITHIN THE VAPOUR BARRIER OF DING ENVELOPE) DTECTED SURFACES (ENTIRELY WITHIN THE VAPOUR BARRIER OF	HIGH RISE EXTERNAL PRESSURE CO-EFFICIENT, GUST EFFECT FACTOR & EXPO
	THE BUILE BEAMS 40 FOR CONCRETE EXPOSURE CLASSES (DING ENVELOPE)	<u>LOW RISE</u> <u>NOT</u>
	ALL STRUCTURAL ELEMENTS (INCLUDI		ROOF SLOPE = 50
	DIAMETER OF 1 FOR CLASS N, 1.5 FOR	CLASSES F1 AND F2 AND 2 FOR CLASSES C1 AND C3.	$\frac{Cp C_{g WINDWARD}}{Cp C_{g LEEWARD}} = 0.75$ $= -0.55$
			$\frac{\text{EW WIND}}{\text{Cp } C_{g \text{ WINDWARD}}} = 0.75$ $\text{Cp } C_{g \text{ LEEWARD}} = -0.55$
	SHOP DRAWING RE	VIEW	$\begin{array}{ccc} \underline{\text{HIGH RISE}} \\ \hline C_{\text{E WINDWARD}} \\ C_{\text{E LEEWARD}} \end{array} = \begin{array}{ccc} (\text{VARIES WITH HEIGHT}) \\ \hline \end{array}$
	DOCUMENTS AND SPECIFICATIONS. CO	Y FOR GENERAL CONFORMITY WITH STRUCTURAL CONTRACT DMMENTS MADE ON THE SHOP DRAWINGS DURING THIS REVIEW DR FROM COMPLIANCE WITH THE REQUIREMENTS OF THE	Cg = 2.0
	TO THE CONTRACT. REVIEW OF A SPI WHICH THE ITEM IS A COMPONENT. TH	AND SPECIFICATIONS, NOR DO THEY AUTHORIZE ANY CHANGES ECIFIC ITEM SHALL NOT INCLUDE REVIEW OF AN ASSEMBLY OF HE CONTRACTOR'S RESPONSIBILITIES INCLUDE ALL QUANTITIES,	<u>NS WIND</u> D = m H/D =
	AND PROCEDURES OF CONSTRUCTION ALL WORK IN A SAFE AND SATISFACTO	MENTS, FABRICATION PROCESS, MEANS, METHODS, SEQUENCES I, COORDINATION OF WORK WITH ALL TRADES AND PERFORMING INTY MANNER. THE REVIEW OF SHOP DRAWINGS DOES NOT IMPLY ILTANTS' OR PROFESSIONALS' RESPONSIBILITIES RELATED TO	$ \begin{array}{ccc} C_{p & WINDWARD} & = \\ C_{p & LEEWARD} & = \\ \underline{EW & WIND} \end{array} $
		INED BY THE SPECIFICATIONS (SUCH AS STRUCTURAL STEEL	$ \begin{array}{ccc} D & = & m \\ H/D & = & \\ C_{p WINDWARD} & = & \\ \end{array} $
	NOT REVIEWED - SHOWS WORK CONSULTING S		C _{p LEEWARD} = FACTORED DESIGN LOADS (1.4W)
	NOTED - RELEASED FO FINAL RECORE	R FABRICATION. PR FABRICATION AFTER REVISIONS NOTED ARE MADE. SUBMIT O PRINT. D RESUBMIT FOR REVIEW PRIOR TO FABRICATION.	NS WIND BASE SHEAR (ULS) = 280 kN BASE OVERTURNING MOMENT (ULS) = 2520 kN.n
			EW WIND BASE SHEAR (ULS) = 140 kN BASE OVERTURNING MOMENT (ULS) = 1185 kN.n
			.5 <u>SEISMIC:</u>
			SEISMIC FORCE RESISTING SYSTEM (SFRS) SFRS: SYSTEM & CONNECTIONS: (CLAUSE 4.1.8.9/4.1.8.10) LATERAL LOAD RESISTING SYSTEM: CONVENTIONAL CONS Rd = 1.5
			Ro = 1.3 CSA STANDARD: CAN CSA-S16-09 APPLICABLE CLAUSE(S): 27.10
			SFRS: DIAPHRAGMS & CONNECTIONS: (CLAUSE 4.1.8.15) CSA STANDARD: CAN CSA-S16-09 APPLICABLE CLAUSE(S): 27.10 SFRS: SYSTEM FOUNDATIONS: (CLAUSE 4.1.8.16)
			SFRS: SYSTEM FOUNDATIONS: (CLAUSE 4.1.8.16) CSA STANDARD: CSA A23.3-04 APPLICABLE CLAUSE(S): 21.11
			IMPORTANCE FACTOR: [CLAUSE 4.1.8.5] IE = 1.0
			PROJECT LOCATION: KINGSTON,ON 5% DAMPED SPECTRAL RESPONSE ACCELERATION VALUES
			PGA = 0.12 Sa(0.2) = 0.29
			Sa(0.5) = 0.18 Sa(1.0) = 0.099 Sa(2.0) = 0.031
			SITE CLASS: THE NOTED SITE CLASSIFICATION FOR SEISMIC SITE RE AND SHEAR WAVE VELOCITY PARAMETERS INDICATED ARE AS REPORTED IN THE GEOTECHNICAL REPORT DBA ENGINEERING LTD.
			□A □B ■C □D □E □F (SITE SPECIFIC SPECT HORIZONTAL SHEAR WAVE VELOCITY: □ m/s ■ NOT PER
			Fa = 1.0 Fv = 1.0 DESIGN SPECTRAL RESPONSE ACCELERATION VALUES
			S(0.2) = 0.29 S(0.5) = 0.18
			S(1.0) = 0.099 S(2.0) = 0.031 S(4.0) = 0.0155
			leFaSa (0.2) = 0.29 <u>FUNDAMENTAL PERIOD DATA</u>
			EMPIRICAL FORMULA [CLAUSE 4.1.8.11(3)] Ta = 0.185 sec
000	R1 (1000-707)		
აას	B1 (1000x707)		

					400W				
- WIE - ANG	CTURAL ST DE FLANGE CHOR ROD OTHER S	DS:): CAN/0 350 W 300 W 300 W	SA G4	0.21M				
- AS - G40 - HS	⁻ M A500 GF 0.21 GRADE	EEL (HSS ONLY): RADE C (345 MPa F 350W CLASS C O S REQUIRED TO BI G	RH						
STRUC - HOI - SOI - MO - GRO	CTURAL MA LOW BLOC LID BLOCK RTAR: DUT FOR E	ASONRY: CK: : BLOCK CORES: DMPRESSIVE STRE	CSA A CSA A CSA A 1:3:2 C BY VO	165.1 - 179M - 179M - EMENT LUME V 'm, IS:	VITH 200 \$	A-STONE			
SOI - SPI SOI	ECIFIED FL	ck - Routed Hollow I .exural tensile : Dllow Block - Dllow Block -	STRENG 0.4 MP	7. 5TH ft (N a	8 MPa 5 MPa JORMAL T	O BED JOIN	NTS) IS	::	
		FOR BUILDING STR			DEVELO	PED FOR TH	HE REF	ERENCED BU	UILDING T
		IE FOLLOWING MU OR CLIMATIC DATA					DESIG	N LOADS HAV	/E BEEN
OBTA		DM: <u>THE SUPPLEME</u>			ARD SB-1	<u>TABLE 1.2</u>			
.2	Ss = 2.	SNOW LOAD AND 1 kN/m² 4 kN/m²	ASSOCI	ATED R	ain load	Ľ			
		D SNOW LOAD [Ss x Cb x Cw x Cs	x Ca + S	r] =	ls x [2.1x0	.8x1.0x1.0x1	1.0+0.4] = ls x 2.08 kN	√/m²
	$\frac{\text{ULS}}{\text{Is} = 1.0}$		Ī	<u>SLS:</u> s = 0.9					
.3	S = 2.08 24 HOUR	3 kN/m² RAINFALL: 108 mm		5 = 1.87	′ kN/m²				
.4	WIND:								
		NCE CATEGORY =	NORMA	Ĺ					
	IMPORTA Iw = Iw =	<u>NCE FACTOR:</u> 1.00 (ULS) 0.75 (SLS)							
	<u>1/50 Yr HC</u> q =	OURLY WIND PRES	SURE:						
	y – TERRAIN					OPE			
		HEIGHT ABOVE GR				ROU	GΠ		
	₩s = 8.64 CONCLUS	/30.0 = 0.288 SION: BUILDING	IS:				RISE		
	<u>EXTERNA</u>	L PRESSURE CO-E	FFICIEN	IT, GUS	T EFFEC				<u>DR</u>
	LOV	<u>W RISE</u>					NOT /	APPLICABLE	
		C _E ROOF SLOPE		= 0.97 = 50	(AT H)			
		<u>NS WIND</u> Cp C _{g WINDWARD} Cp C _{g LEEWARD}		= 0.75 = -0.55					
		EW WIND Cp C _{g WINDWARD} Cp C _{g LEEWARD}		= 0.75 = -0.55					
	<u>HIG</u>	H RISE C _{E WINDWARD} C _{E LEEWARD}	:	= <u></u> →_ :	(VARI (AT H	ES WITH HI /2)	EIGHT)) =	
		Cg = 2.0 NS WIND						•	
		D H/D C	=	= m = =				:	
				=				•	
		EW WIND D H/D	=	= m =				:	
	FACTORE	C _{p WINDWARD} C _{p LEEWARD}	:	=				:	
	<u>NS '</u>	<u>WIND</u> BASE SHEAR BASE OVERTUR	NING MO	OMENT	(ULS) (ULS)	= 280 = 252) kN 20 kN.n	n	
	EW	WIND BASE SHEAR BASE OVERTUR	NING MO	OMENT	(ULS) (ULS)	= 140 = 118) kN 35 kN.n	n	
		<u>SMIC:</u>	QVOT-		2)				
	SFRS:	FORCE RESISTING SYSTEM & CONNE LATERAL LOAD R Rd = 1.5 Ro = 1.3	ECTIONS	S: (CLAI	JSE 4.1.8.	9/4.1.8.10) /ENTIONAL	CONS	TRUCTION O	F BRACEI
	SFRS:	CSA STANDARD: (APPLICABLE CLAI DIAPHRAGMS & C CSA STANDARD: (APPLICABLE CLAI	JSE(S): ONNEC CAN CSA	27.10 TIONS: A-S16-0	(CLAUSE	4.1.8.15)			
	SFRS:	SYSTEM FOUNDA CSA STANDARD: (APPLICABLE CLA)	CSA A23	.3-04	E 4.1.8.16	□ FO		HORED FOOT	
	IMPORTA	NCE FACTOR: [CLA 1.0	USE 4.1	.8.5]					
		LOCATION: KINGS			_				
	<u>5% DAMP</u> PGA	ED SPECTRAL RES	PONSE	ACCEL	ERATION	VALUES			
	Sa(0.2) Sa(0.5) Sa(1.0) Sa(2.0)	= 0.12 = 0.29 = 0.18 = 0.099 = 0.031							
	AND SHE	SS: THE NOTED SI AR WAVE VELOCIT ED IN THE GEOTEC □A □B ■ HORIZONTAL	Y PARA HNICAL C □D	METER REPOF	S INDICAT RT DBA EN DF (SITE	TED ARE AS IGINEERING SPECIFIC S	S G LTD. SPECT m/s	BY 12-2334-0	1
	Fa = 1.0 Fv = 1.0						⊂CK		
	DESIGN S	PECTRAL RESPON	ISE ACC	ELERA	TION VAL	<u>UES</u>			
	a : :								
	S(0.2) S(0.5) S(1.0)	= 0.29 = 0.18 = 0.099							
	S(0.5)	= 0.18							
	S(0.5) S(1.0) S(2.0) S(4.0) IeFaSa (0.	= 0.18 = 0.099 = 0.031 = 0.0155	- •						

	MATERIAL AND DESIGN DATA	MATERIAL AND DESIGN DATA (CONT'D)
1.	FOOTING BEARING RESISTANCE: kPa AT ULS (ULTIMATE LIMIT STATES DESIGN) 150 kPa AT SLS (SERVICEABILITY LIMIT STATES DESIGN)	ALTERNATE METHOD OF MECHANICS [CLAUSE 4.1.8.11(3)(d)]
	MODULUS OF SUBGRADE REACTIONS (ASSUMED FOR DESIGN OF SLABS ON GRADE) 24,000 kN/m ³	NOT USED Ta(NS) =sec ■ Ta(EW) =sec ■
	SEE SOILS REPORT PREPARED BY: DBA ENGINEERING LTD. REPORT NUMBER: 12-2334-01 DATED: NOVEMBER 8, 2012	DESIGN PERIOD
2.	CONCRETE SPECIFIED COMPRESSIVE STRENGTH, fc, IS 25 MPa EXCEPT FOR: DOCKING AREA - 35 MPa	Ta(NS) = 0.185 sec Ta(EW) = 0.185 sec
	SLAB ON GRADE - 30 MPa AND WHERE SHOWN ON PLANS AND SCHEDULES. INCREASE STRENGTH AS REQUIRED FOR REQUIRED CLASS OF EXPOSURE, REFER TO SPECIFICATIONS.	DESIGN SPECTRAL RESPONSE ACCELERATION AT FUNDAMENTAL PERIOD S(Ta)NS = 0.29 Mv(NS) = 1.0 J(NS) = 1.0
3.	REINFORCING STEEL: CAN/CSA G30.18M - GRADE 400R 400W	S(Ta)EW = 0.29 $M_{V}(EW) = 1.0$
4.	STRUCTURAL STEEL (EXCEPT HSS): CAN/CSA G40.21M - WIDE FLANGES: 350 W - ANCHOR RODS: 300 W	J(EW) = 1.0 IRREGULARITY REVIEW: [CLAUSE 4.1.8.6]
	- ALL OTHER STEEL: 300 W	1. VERTICAL STIFFNESS: PYES NO 2. WEIGHT: PYES NO
6.	STRUCTURAL STEEL (HSS ONLY): - ASTM A500 GRADE C (345 MPa FOR SQUARE/RECTANGULAR AND 317 MPa FOR ROUND) OR - G40.21 GRADE 350W CLASS C OR H	3. VERTICAL GEOMETRIC: PYES NO 4. IN-PLANE DISCONTINUITY: PYES NO 5. OUT-OF-PLANE: PYES NO
	 HSS MEMBERS REQUIRED TO BE GALVANIZED SHALL BE CLASS H, OR STRESS RELIEVED PRIOR TO GALVANIZING 	6. WEAK STOREY: □ YES ■ NO 7. TORSIONAL: □ YES ■ NO B(NS) = 1.306
7.	STRUCTURAL MASONRY: - HOLLOW BLOCK: CSA A165.1 - H/15/A/M - SOLID BLOCK: CSA A165.1 - S/15/A/M - MORTAR: CSA A179M - TYPE S - GROUT FOR BLOCK CORES: CSA A179M - COARSE GROUT 1:3:2 CEMENT:SAND:PEA-STONE BY VOLUME WITH 200 SLUMP	B(EW) = 1.149 8. NON-ORTHOGONAL: • YES • NO CONCLUSION: BUILDING IS: • REGULAR • IRREGULAR DYNAMIC ANALYSIS: • REQUIRED DYNAMIC PROCEDURE METHOD: • MODAL RESPONSE SPECTRUM • NUMERICAL INTEGRATION TIME HISTORY • N/A
	- SPECIFIED COMPRESSIVE STRENGTH, fm, IS: HOLLOW BLOCK - 9.8 MPa SOLID AND GROUTED HOLLOW BLOCK - 7.5 MPa	TORSIONAL ECCENTRICITY: PROCEDURE)
	SPECIFIED FLEXURAL TENSILE STRENGTH ft (NORMAL TO BED JOINTS) IS: SOLID AND HOLLOW BLOCK - 0.4 MPa GROUTED HOLLOW BLOCK - 0.65 MPa	□ ± 0.10 Dnx (CLAUSE 4.1.8.12 (4)(a)), B > 1.7 (3-D DYNAMIC ANALYSIS) □ ± 0.05 Dnx (CLAUSE 4.1.8.12 (4)(b)), B < 1.7, (3-D DYNAMIC
8.	DESIGN LOADS FOR BUILDING STRUCTURE:	ANALYSIS) BASE SHEARS / OVERTURNING MOMENTS
	DESIGN LOADS PRESENTED BELOW HAVE BEEN DEVELOPED FOR THE REFERENCED BUILDING TO BE LOCATED IN THE FOLLOWING MUNICIPALITY: KINGSTON, ON	EQUIVALENT STATIC FORCE PROCEDURE:

BASE SH	EARS		
NS DIRE	CTIONS		
VMIN	= S(2.0) Mv le \	N/(Rd Ro)	= 0.0238 W
VMAX	= (2/3) S(0.2) le	e W/(Rd Ro)	= 0.0991 W
EW DIRE	CTIONS		
VMIN	= S(2.0) Mv le \	N/(Rd Ro)	= 0.0238 W
VMAX	= (2/3) S(0.2) le	e W/(Rd Ro)	= 0.0991 W
DESIGN E	BASE SHEARS & (OVERTURNING MOMENTS	
V(NS)	= 0.0991 W	= 0.0991 x 5275	= 523 kN
M(NS)	= M x J	= 3690x 1.0	= 3690 kN.m
V(EW)	= 0.0991 W	= 0.0991 x 5275	= 523 kN
M(EW)	= M x J	= 3690 x 1.0	= 3690 kN.m

OPEN

	-
ROUGH	

LOW RISE ■ HIGH RISE □

TOR & EXPOSURE FACTOR

NOT APPLICABLE	

TH HEIGHT) ∎

. .

= 280 kN = 2520 kN.m

= 140 kN = 1185 kN.m

8.10) IONAL CONSTRUCTION OF BRACED FRAME

15)

FOR ANCHORED FOOTINGS FOR UNANCHORED FOOTINGS

SMIC SITE RESPONSE ARE AS EERING LTD. BY 12-2334-01 CIFIC SPECTRUM:)

□ ____ m/s ■ NOT PERFORMED

DRAWING LEGEND AND ABBREVIATION

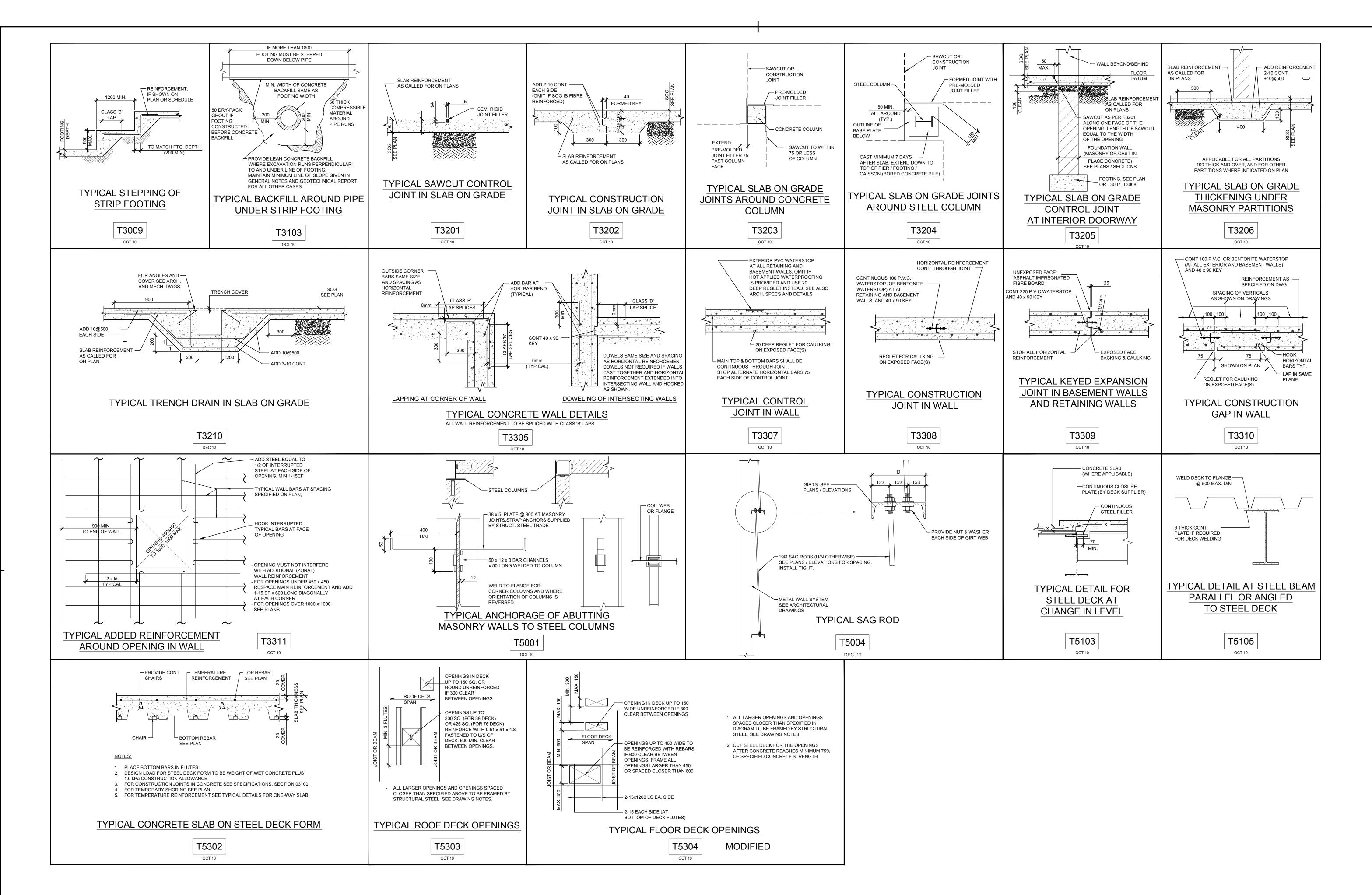
UNLESS OTHERWISE NOTED, DESIGN LOADS SHOWN ARE SPECIFIED (UNFACTORED) USED FOR ULS DESIGN. FOR POINT LOADS, IF ONLY ONE LOAD IS GIVEN, CONSIDER IT WIND AND SNOW LOADS TO BE USED FOR SLS DESIGN, REFER TO MATERIAL AND DESIG

A.ROD	ANCHOR ROD	LE
AEC	ARCHITECTURALLY EXPOSED CONCRETE	LG.
AESS	ARCHITECTURALLY EXPOSED STRUCTURAL STEEL	UL
Af		LL
	(+ INDICATES TENSION, - INDICATES COMPRESSION)	LL LLH
ALT.	ALTERNATE	LLV
ARCH.	ARCHITECTURAL	LSV
		LSH
B, BOT. BCP	BOTTOM BORED CONCRETE PILE	LP
BEW	BORED CONCRETE FILE BOTTOM EACH WAY	MAX.
BLL	BOTTOM LOWER LAYER	MAA. Mf
BM.	BEAM	MJ
BOF	ELEV BOTTOM OF FOOTING	MIN.
BOP BP	ELEV BOTTOM OF PILE BEARING/BASE PLATE	MTf
BSMT.	BASEMENT	
BUL	BOTTOM UPPER LAYER	NF
BUP	BOTTOM OF UNDERPINNING	NTS
CA	COLUMN ABOVE ONLY (NO COLUMN BELOW)	O/C
CAM.	CAMBER	0/0
CANT.	CANTILEVER	OPEN, OPG.
CB	COLUMN BELOW	
C/C		P
CEL CF	CUT OFF ELEVATION FOR PILES CONCRETE FIREPROOFED	Pf PL
CJ	CONTROL JOINT	FL
CL	CLEAR	RA
¢		RD
CNT COMP.	STEEL DECK CORE NOMINAL THICKNESS COMPOSITE	REINF. RE
CONSTR. JT.		RE
COL.	COLUMN	Rf
CONC.	CONCRETE	RHf
CONT.		
CP CWS	CONNECTION PLATE	SCA
CLS	SEE GENERAL NOTES	
css J		SDL
DCA DET.	DRILLED CONCRETE ANCHOR DETAIL	SECT.
D.F-L	DOUGLAS FIR-LARCH	SIM. SJ
DIA.	DIAMETER	SLS
DIM.	DIMENSION 2	SL.
DL DMA	DEAD LOAD IN KN/m ² DRILLED MASONRY ANCHOR	SL1, SL2
DNA DN.	DOWN	SOG
DO.	DITTO	SPF STIR.
DP.	DEEP	STIFF.
DWG. DWL.	DRAWING DOWEL	
DVVL.	DOWEL	t T
EA.	EACH	T TEW
ECR	EPOXY COATED REINFORCEMENT	THK.
EE	EACH END	TJ
EF EJ, EXP.JT.	EACH FACE EXPANSION JOINT	TLE
EL., ELEV.		TLL TOF
EMBED.	EMBEDMENT	TOP
EQ.	EQUAL	TPC
EX., EXIST.	EXISTING	TRE
FD	FLOOR DRAIN	TUL TYP.
FF	FAR FACE	IIF.
FIN.	FINISHED	ULS
FL. FMC	FLOOR FULL MOMENT CONNECTION	U/S
FTG.	FOOTING	U/N
fc	COMPRESSIVE STRENGTH OF CONC IN MPa	UPT.
fy	YIELD STRENGTH IN MPa	VB
		V, VEF
GALV.	GALVANIZED STEEL	Vf VIC
GB	GRADE BEAM	V, VERT., VERTS.
GL	GRIDLINE	VSC
h	TOTAL THICKNESS	
H, HOR. HDG	HORIZONTAL HOT DIPPED GALVANIZED	VXB
HEF	HORIZONTAL EACH FACE	WC
НН	HOOK-HOOK (HOOK EACH END)	WWA
	HOLE THROUGH CONCRETE BEAM	WWF
→ →	HOLE THROUGH STEEL BEAM	700
HIC	HORIZONTAL IN CENTRE	ZRP
HK. HP	HOOK HIGH POINT	
		00
IBA	INTEGRITY BARS ADDED	SXXX SIM.
IBE	INTEGRITY BARS EXTERIOR	\smile
IBI	INTEGRITY BARS INTERIOR	· / / / / / / /
JG	JOIST GIRDER	
ld	TENSION DEVELOPMENT LENGTH OF REBAR	
ldc	COMPRESSION DEVELOPMENT LENGTH OF REBAR	
L	SINGLE ANGLE	
٦L	DOUBLE ANGLES	

TIONS	Public Works and Government Serv Canada	
ACTORED) LOADS, TO BE ISIDER IT LIVE LOAD. FOR ND DESIGN DATA NOTES.		
LEFT END LONG/LENGTH UPPER LEVEL BM/JOIST LOWER LEVEL BM/JOIST LIVE LOAD IN kN/m ² LONG LEG HORIZONTAL LONG LEG VERTICAL	Real Property Operat Real Property Operat Direction générale de Solutions - Opération	tions Solu es opérations
LONG ELG VERTICAL LONG SIDE HORIZONTAL LOW POINT MAXIMUM	Project Delivery & Pro Technical Services Exécution de projets	
FACTORED MOMENT IN kN.m MOVEMENT JOINT MINIMUM MOMENT CONNECTION FACTORED TORSION IN kN.m	Services experts/con Watson Ma	seils tech
NEAR FACE		4
NOT TO SCALE ON CENTRE OUT TO OUT OPENING		т.
POINT LOAD IN KN FACTORED POINT LOAD IN KN PLATE ROCK ANCHOR ROOF DRAIN REINFORCEMENT	Structural Engineers Halsall Associates 4001-210 Gladstone Avenue Ottawa, ON K2P 0Y6 613.237.2462	Mechanica Bouthillett Associate 100 - 1960 Ottawa, Ol 613.596.64
RIGHT END RIGID FRAME EACTORED VERTICAL REACTION IN KN	14Y160-049A	
FACTORED VERTICAL REACTION IN KN FACTORED HORIZONTAL REACTION IN KN STEEL COLUMN ABOVE (NO STEEL COLUMN BELOW) STEP DOWN FOOTING IN DIRECTION OF ARROW SUPERIMPOSED DL	Civil Engineers WSP Group 201-1224 Gardiners Road Kingston, Ontario K7P 0G2 613.634.7373	IT-Telecom The Attain 208-1680 V Ottawa, Ol 613.739.94
(EXCLUDING SELF-WEIGHT) IN KN/m ² SECTION SIMILAR STEEL JOIST SERVICEABILITY LIMIT STATE SLAB SHELF ANGLE 1, ETC SLAB ON GRADE SPRUCE PINE FIR STIRRUP STIFFENER THICKNESS TOP TOP EACH WAY THICK TIE JOIST TOP LACH WAY THICK TIE JOIST TOP LEFT END TOP OF PILE CAP TOP UPPER LAYER TYPICAL ULTIMATE LIMIT STATE UNDERSIDE UNLESS NOTED UPTURNED VERTICAL BRACING VERTICAL BRACING VERTICAL, VERTICAL EACH FACE FACTORED SHEAR IN KN VERTICALLY SLOTTED CONNECTION TO ALLOW FOR DEFLECTION VERTICAL 'X' BRACING WIND COLUMN WINDOW WASHING ANCHORS WELDED WIRE FABRIC	LSION I.J.F	
ZINC RICH PAINT SECTION NUMBER SECTION DRAWING		
REFERENCE MASONRY WALL FULLY GROUTED MASONRY WALL		
STRUCTURAL PRECAST CONCRETE		
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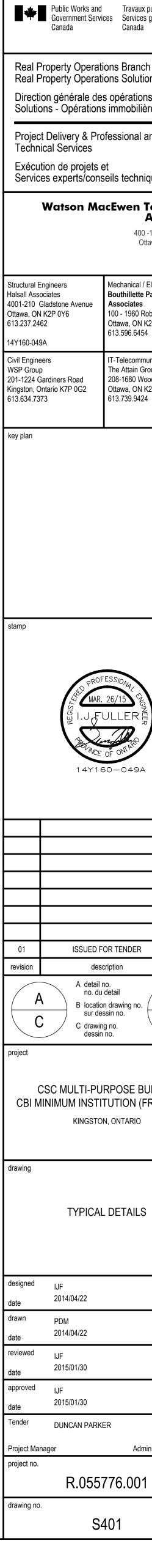
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Public Works and Government Servi Canada		mentaux		
Real Property Operations Branch Real Property Operations Solutions Direction générale des opérations immobilières Solutions - Opérations immobilières				
Project Delivery & Professional and Technical Services Exécution de projets et				
Services experts/cons				
Watson MacEwen Teramura Architects 400 -116 Lisgar Street Ottawa ON K2P 0C2 t 613.232.0330 f 613.232.6253				
ructural Engineers Isall Associates 01-210 Gladstone Avenue tawa, ON K2P 0Y6 3.237.2462	Mechanical / Electrical Eng. Bouthillette Parizeau & Associates 100 - 1960 Robertson Road Ottawa, ON K2H 5B9 613.596.6454			
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oject Manager Administrateur de projets oject no. no. du projet				
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PWGSC B1 (1000x707)



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