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SPEEDCRANE DERRICK HOIST REPLACEMENT ANALYSIS

MARTHA L. BLACK | ICE BREAKER



For



Pêches et Océans
Canada

Fisheries and Oceans
Canada

Garde côtière

Coast Guard

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Document

C20-14-009-01 R1 Speedcrane derrick hoist replacement analysis

Description of revisions

Rev	Date	Description	Done by	Approved by
0	2020-06-18	Original document	H.R.	H. Royer, ing.
1	2020-07-24	Design change for lead block bracket and supporting structure	H.R.	H. Royer, ing.



2020-07-24

Table of contents

1	Introduction.....	1
2	Assumptions	1
3	Analysis results	2
3.1	Compliance of boom structure and block brackets	2
3.2	Pulley blocks, swivels and gear.	2
3.3	Foundation for the winch	2
4	conclusion.....	3

Table of Appendixes

Annexe A	Structural Calculation Details
Annexe B.....	Increase Hoist 5T to 8T Support Drawing

1 Introduction

The Speedcrane derrick actually installed on the Martha L. Black has a global safe working load (SWL) of 28 metric tonnes. It is fitted with 3 hoists;

- A 20t SWL hoist
- A 8t SWL hoist
- A 5t SWL hoist

Concept Naval was mandated to conduct a feasibility study to replace the 5t hoist by a 8t hoist. This implies the validation of;

- The main boom increased load and acceptability of stresses.
- The head block bracket on main boom. (block # 21)
- The heel block attachment structure on main boom. (block # 20)
- The lead block bracket and backup structure on wheelhouse top. (block # 19)
- The supporting structure in way of the winch on lower deck.

2 Assumptions

To determine the loads for this analysis, the design parameters as found in the crane manual, *Job No. 1DG 6030-33*, were assumed;

- The crane can be operated at a maximum sea state of Beaufort 3 corresponding to a maximum wave height of 1.2m
- The global crane SWL remains at 28t.
- Only two(2) of the hoist can be used simultaneously; 20t with the 8t or 20t with the 5t.
- The de-rating according to sea waves height as described on Transport Canada Certificate no. *R34043-7097* still applies.

The structural validation was conducted to be in accordance with the *ABS Guide for Certification of Lifting Appliances*. The crane is treated as a *Shipboard crane* with the relevant amplification factors.

- No accumulated ice load has been considered.

3 Analysis results

3.1 Compliance of boom structure and block brackets

The main boom, including the structural brackets for the auxiliary hoist head block no.21 were found with acceptable induced stresses under the relevant loads.

The heel block no. 20 supporting structure was not analysed but is identical in design and located at the same location along the boom as the heel block no. 7 which is design for a 8t SWL hoist on the port side of the boom. The strength of the bracket structure is then considered acceptable. It is however to be noted that the block no.20 itself was not analysed by Concept Naval. If it cannot be confirmed suitable for the increased load of 8t (axle, sheave, etc.) then the block shall be replaced with a certified one.

The upper bracket supporting the lead pulley block no. 19 just above wheelhouse top is found too weak to support the increased load such as the backup structure inside the top box and these need some replacement and reinforcements. The detail of the modifications can be found on drawing C20-14-160-01 R1 Sheets 4 and 5.

3.2 Pulley blocks, swivels and gear.

Many diameters or material grade of existing equipment could not be verified by a visual inspection. All related pulleys are to be confirmed adequate for the increased safe working load of 8.0 tones or shall be replaced (entirely or individual parts) with certified ones including all connecting gears, swivels, sheaves, axles, pins.

3.3 Foundation for the winch

In terms of strength, the existing seat and the local deck structure already in place for the 5t auxiliary hoist winch is suitable for the increased load of 8t. Supporting calculation are shown in Annexe A

It is also understood that the actual winch housing can be reused as being suitable for the increased load. Replacement of different gears and parts are assumed to be the only structural modification required for the winch part. This is out of Concept Naval scope.



4 conclusion

Our analysis has revealed that the strength of the existing boom and block supporting brackets are adequate for the increased load of 8t on the whip hoist with the exception of the top lead block bracket and support structure that requires reinforcement. This is assuming the assumptions stated in this report are valid.

Concept Naval did not make any selection of replacement equipment neither did validate whether existing gear are adequate for any updated cable diameter. Also, the feasibility of converting the hoist winch from a 5t capacity to an 8t capacity was not validated.

Annexe A

Structural Calculation Details



ABS Guide for Certification of Lifting Appliances

	Sea state 3			
	Significant wave height	Hs	1.2	1.2 m
	Hoist description		Whip	Main
	Position along boom		17.374	21.184 m
	Safe working load	SWL	8	20 t
	Live load	LL	78.48	196.2 kN
	Boom angle		20	20 degrees from horizontal
2-2/5.17	vertical acceleration	a _v	0.070	0.070 g
2-2/5.17	horizontal acceleration	a _h	0.045	0.045 g
				g
2-2/5.17	Dead load vertical factor		1.070	1.070
2-2/5.17	Dead load horizontal factor		0.045	0.045
	Combined dead load factor		1.071	1.071
2-2/7.3	Live load vertical factor	VAF	1.300	1.300 Considering as a shipboard crane
2-2/5.17	Live load horizontal factor		0.045	0.045
	Combined live load factor		1.301	1.301
	Live load considered		10.41	26.02 t
	Cos20° component		0.940	0.940
	Sin20° component		0.342	0.342 t
	Max force along boom		14.0	34.9
	Force component lateral to boom		9.78	24.45
	Moment w/r boom pivot		169.9	517.9 tm
	Total moment			687.8 tm
	Lateral component topping cables			32.5 t
	Angle of topping cables with boom			33 deg
	Component of topping along boom			50.0 t
	Max axial force along boom			98.9 t
Block #20 bracket attach point under boom.				
	Considered length of weld		450	mm
	Weld troath		8.98	mm
	Distance between welds		210	mm
	Weld shear area		8081	mm ²
	Sec. mod. weld connect. to boom		589857	mm ³
	Force along boom		137001	N
	Lever		199	mm
	Bending stress (shear in welds)		46.2	N/mm ²
	Pure shear along boom		17.0	N/mm ²
	Total shear in welds		63.2	N/mm ²
	Allowable shear stress		99.2	N/mm ²



Projet / description : Boom tube stress calculation; Boom Angle from horizontal : 20°

Données

Portée de la poutre : L 21.184 m Type de Poutre :
Support intermédiaire : L' m Supportée - Supportée

Charges et moments ponctuels

a (m)	17.374	21	21.18						
Charge F (t)	9.78								
Moment M (tm)	-6.40	-17.6	13.7						

Charge Distribuée n°1	
Charge totale P (t)	5.82
a (m)	10.592
x1 (m)	0
x2 (m)	21.184
Charge répartie F1 (t/m)	
Charge répartie F2 (t/m)	

Charge Distribuée n°2	
Charge P (t)	0
a (m)	
x1 (m)	
x2 (m)	
F1(t)	
F2(t)	

Type de raidisseur : Round tube OD: 666 ID: 634 Module d'Young du matériel E 200000 N/mm2

Résultats

Aire totale (tôle et raidisseur) : A 32673 mm²

Aire résistant au cisaillement : AC 32673 mm²

Poids linéaire 0.0 kg/m

avec tôle associée 0.0 kg/m

Hauteur de l'axe neutre : NA 0.0 mm

Intertie p/r à l'axe neutre : Ixx 172657 cm⁴

Section module : SM 5184.9 cm³

	Abs(BM)	47.69	tm
Moment de flexion maximum	Abs(V)	11.41	tonnes
Effort tranchant maximum	M1	0.00	tm
Moment à gauche	M2	0.00	tm
Moment à droite	R1	-4.18	tonnes
Réaction à gauche	R2	11.41	tonnes
Réaction à droite	Abs(Y)	56.42	mm
Déformation maximale			

Assumed steel yield resistance σ_y	248 N/mm ²	
Axial load F_{axial}	969950	N
	Actual	Allowable
Axial stress: σ_{axial}	29.7	N/mm ²
Contrainte de flexion $\sigma_{bending}$	90.2	148.8 N/mm ²
Contrainte de cisaillement τ	3.4	99.2 N/mm ²
Total normal stress σ_{total}	119.9	148.8 N/mm ²
Combined stress σ_{comb}	120.1	186 N/mm ²



ABS Guide for Certification of Lifting Appliances

	Sea state 3			
	Significant wave height	Hs	1.2	1.2 m
	Hoist description		Whip	Main
	Position along boom		17.374	21.184 m
	Safe working load	SWL	8	20 t
	Live load	LL	78.48	196.2 kN
	Boom angle		70	70 degrees from horizontal
2-2/5.17	vertical acceleration	a _v	0.070	0.070 g
2-2/5.17	horizontal acceleration	a _h	0.045	0.045 g
				g
2-2/5.17	Dead load vertical factor		1.070	1.070
2-2/5.17	Dead load horizontal factor		0.045	0.045
	Combined dead load factor		1.071	1.071
2-2/7.3	Live load vertical factor	VAF	1.300	1.300 Considering as a shipboard crane
2-2/5.17	Live load horizontal factor		0.045	0.045
	Combined live load factor		1.301	1.301
	Live load considered		10.41	26.02 t
	Cos70° component		0.342	0.342
	Sin70° component		0.940	0.940 t
	Max force along boom		20.2	50.5
	Force component lateral to boom		3.56	8.90
	Moment w/r boom pivot		61.8	188.5 tm
	Total moment			250.3 tm
	Lateral component topping cables			11.8 t
	Angle of topping cables with boom			12.6 deg
	Component of topping along boom			52.9 t
	Max axial force along boom			123.5 t
Block #20 bracket attach point under boom.				
	Considered length of weld		450	mm
	Weld troath		8.98	mm
	Distance between welds		210	mm
	Weld shear area		8081	mm ²
	Sec. mod. weld connect. to boom		589857	mm ³
	Force along boom		198015	N
	Lever		199	mm
	Bending stress (shear in welds)		66.8	N/mm ²
	Pure shear along boom		24.5	N/mm ²
	Total shear in welds		91.3	N/mm ²
	Allowable shear stress		99.2	N/mm ²



Projet / description : Boom tube stress calculation; Boom Angle from horizontal : 70°

Données									
Portée de la poutre : L		21.184		m		Type de Poutre :			
Support intermédiaire : L'				m		Supportée - Supportée			
Charges et moments ponctuels									
a (m)	17.374	21	21.18						
Charge F (t)	3.56								
Moment M (tm)	-9.24	-25.5	14.5						
Charge Distribuée n°1					Charge Distribuée n°2				
Charge totale P (t)		5.82		Charge P (t)		0			
a (m)		10.592		a (m)					
x1 (m)		0		x1 (m)					
x2 (m)		21.184		x2 (m)					
Charge répartie F1 (t/m)				F1(t)					
Charge répartie F2 (t/m)				F2(t)					
Type de raidisseur :		Round tube		Module d'Young du matériel		E		200000 N/mm2	
		OD: 666 ID: 634							
Résultats									
Aire totale (tôle et raidisseur) : A		32673		mm²		Hauteur de l'axe neutre : NA		0.0 mm	
Aire résistant au cisaillement : AC		32673		mm²		Intertie p/r à l'axe neutre : Ixx		172657 cm⁴	
Poids linéaire		0.0		kg/m		Section module : SM		5184.9 cm³	
avec tôle associée		0.0		kg/m					
Moment de flexion maximum		Abs(BM)		36.69		tm			
Effort tranchant maximum		Abs(V)		6.78		tonnes			
Moment à gauche		M1		0.00		tm			
Moment à droite		M2		0.00		tm			
Réaction à gauche		R1		-2.60		tonnes			
Réaction à droite		R2		6.78		tonnes			
Déformation maximale		Abs(Y)		45.76		mm			

Assumed steel yield resistance σ_y	248	N/mm²
Axial load F_{axial}	1211668	N
	Actual	Allowable
Axial stress: σ_{axial}	37.1	N/mm²
Contrainte de flexion $\sigma_{bending}$	69.4	148.8 N/mm²
Contrainte de cisaillement τ	2.0	99.2 N/mm²
Total normal stress σ_{total}	106.5	148.8 N/mm²
Combined stress σ_{comb}	106.6	186 N/mm²

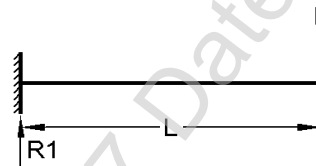


Lead block no.19 bracket connection at top box

Nominal tension	8.0 tonnes
dynamic factor	1.301
loss per pulley	3 %
Tension in hoist side wire	11.0 tonnes
Tension in winch side wire	11.3 tonnes

Données de la poutre

Longueur de la poutre	L	0.7 m
Force totale appliquée	F	22.38 tonnes
Module d'Young du matériel	E	200000 N/mm ²



Encastré-libre force ponctuelle

Moment de flexion maximum	BM	15.7 tm
Effort tranchant maximum	V	22.4 tonnes
Moment à gauche	M1	15.7 tm
Moment à droite	M2	0.0 tm
Réaction à gauche	R1	22.4 tonnes
Réaction à droite	R2	0.0 tonnes

Type de raidisseur

Poutre construite

Dimension de la tôle associée	375 x 10 mm	Assuming weld area only
Dimension de l'âme	500 x 10 mm	See C20-14-601-01 Sheet 4
Dimension du fer plat	375 x 10 mm	

Aire totale (tôle et raidisseur)	A	12500 mm ²	Hauteur de l'axe neutre	NA	250.0 mm
Aire résistant au cisaillement	Ac	5200 mm ²	Intertia p/r à l'axe neutre	Ixx	59192 cm ⁴
Poids linéaire		68.3 kg/m	Section module	SM	2276.6 cm ³
avec tôle associée		97.5 kg/m	Déflexion maximale	D	0.212 mm

Contrainte de flexion	σ	67.5 MPa	Allowed	157.5 N/mm ²
Contrainte de cisaillement	τ	42.2 MPa	Allowed	91.3 N/mm ²
Combined stress	σ	99.5 MPa		

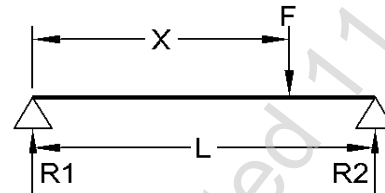
Vertical distance between flange plates:	500 mm
Couple developed horizontal tension/compression at top and bottom flange plates:	31.3 tonnes



Vertical frame I.W.O. lead block no.19 bracket

Données de la poutre

Longueur de la poutre	L	0.975 m
Force totale appliquée	F	31.3 tonnes
Localisation de la force	X	0.515 m
Module d'Young du matériel	E	200000 N/mm ²



Simple-simple force ponctuelle

Moment de flexion maximum	BM	7.6119 tm
Effort tranchant maximum	V	16.548 tonnes
Moment à gauche	M1	0 tm
Moment à droite	M2	0 tm
Réaction à gauche	R1	14.78 tonnes
Réaction à droite	R2	16.548 tonnes

Type de raidisseur Poutre Construite

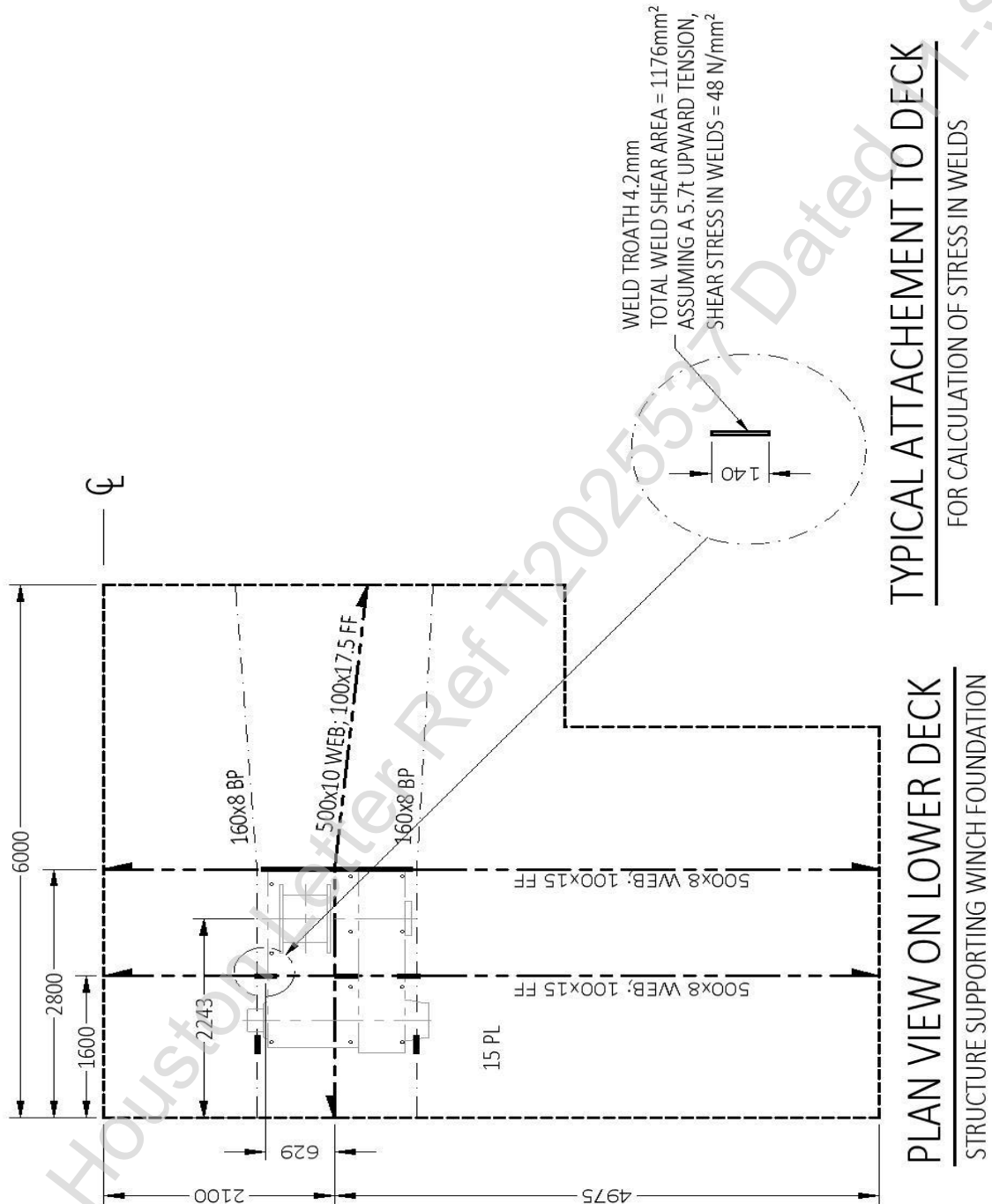
Dimension de la tôle associée	195 x 11 mm
Dimension de l'âme	205 x 20 mm
Dimension du fer plat	70 x 30 mm

Aire totale (tôle et raidisseur)	A	8345 mm ²	Hauteur de l'axe neutre	NA	104.3 mm
Aire résistant au cisaillement	Ac	4920 mm ²	Inertie p/r à l'axe neutre	Ixx	6852 cm ⁴
Poids linéaire		48.4 kg/m	Section module	SM	524.3 cm ³
avec tôle associée		65.1 kg/m	Déflexion maximale	D	0.430 mm

Contrainte de flexion	σ	142.4 MPa
Contrainte de cisaillement	τ	33.0 MPa
Combined stress	σ	153.5 MPa

Allowed 157.5 N/mm²

Lower deck structure in way of winch foundation



Refer to drawing C20-14-601-01 Sheet 7 for details of winch foundation

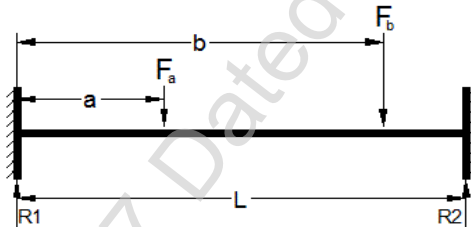
Girder at 2100 stbd of CL

Assuming total load from lead cable is distributed equally on CL girder at both transverse beam location

Total load from lead cable 11.3 tonnes

Données de la poutre

Longueur de la poutre	L	6.0 m
Force appliquée en "a"	F _a	5.7 tonnes
Force appliquée en "b"	F _b	5.7 tonnes
Localisation de la force "F _a "	a	1.6 m
Localisation de la force "F _b "	b	2.8 m
Module d'Young du matériel	E	200000 N/mm ²



Encastré-encastré 2 Forces non-égales

Moment de flexion maximum	BM	9.398 tm
Effort tranchant maximum	V	7.797 tonnes
Moment à gauche	M1	9.398 tm
Moment à droite	M2	-5.728 tm
Réaction à gauche	R1	7.797 tonnes
Réaction à droite	R2	3.548 tonnes

Type de raidisseur

Poutre Construite

Dimension de la tôle associée	1200 x 15 mm
Dimension de l'âme	500 x 10 mm
Dimension du fer plat	100 x 17.5 mm

Aire totale (tôle et raidisseur)	A	24750 mm ²	Hauteur de l'axe neutre	NA	81.0 mm
Aire résistant au cisaillement	Ac	5325 mm ²	Inertie p/r à l'axe neutre	Ixx	70853 cm ⁴
Poids linéaire		52.7 kg/m	Section module	SM	1623.3 cm ³
avec tôle associée		193.1 kg/m	Déflexion maximale	D	-0.689 mm

Contrainte de flexion	σ	56.8 MPa
Contrainte de cisaillement	τ	14.4 MPa



Transverse beam under winch foundation

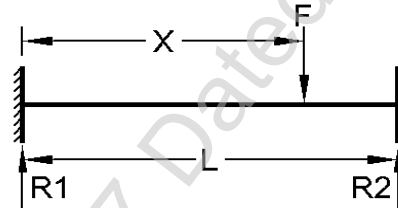
Assuming half the total load from lead cable is concentrated on each transverse beam at 629 from girder connection

Total load from lead cable 11.3 tonnes

Données de la poutre

Longueur de la poutre L 2.1 m
Force totale appliquée F 5.7 tonnes
Localisation de la force X 0.629 m
Module d'Young du matériel E 200000 N/mm²

Moment de flexion maximum BM 1.7507 tm
Effort tranchant maximum V 4.4505 tonnes
Moment à gauche M1 1.7507 tm
Moment à droite M2 0.7486 tm
Réaction à gauche R1 4.4505 tonnes
Réaction à droite R2 1.2218 tonnes



Encastré-encastré force ponctuelle

Type de raidisseur Poutre Construite

Dimension de la tôle associée 420 x 15 mm
Dimension de l'âme 500 x 8 mm
Dimension du fer plat 100 x 15 mm

Aire totale (tôle et raidisseur) A	11800 mm ²	Hauteur de l'axe neutre NA	145.3 mm
Aire résistant au cisaillement Ac	4240 mm ²	Intertia p/r à l'axe neutre Ixx	47120 cm ⁴
Poids linéaire	42.9 kg/m	Section module SM	1274.4 cm ³
avec tôle associée	92.0 kg/m	Déflexion maximale D	0.998 mm

Contrainte de flexion σ	13.5 MPa
Contrainte de cisaillement τ	10.3 MPa



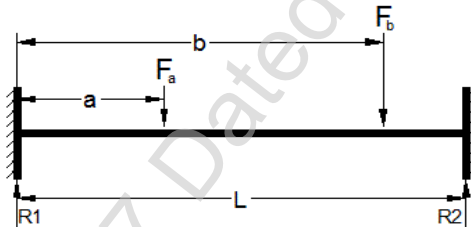
Winch seat girder (span under cable drum)

Assuming total load from lead cable is distributed equally on 2 bolts within this span

Total load from lead cable 11.3 tonnes

Données de la poutre

Longueur de la poutre	L	1.6 m
Force appliquée en "a"	F _a	5.7 tonnes
Force appliquée en "b"	F _b	5.7 tonnes
Localisation de la force "F _a "	a	0.256 m
Localisation de la force "F _b "	b	1.031 m
Module d'Young du matériel	E	200000 N/mm ²



Encastrement-encastrement 2 Forces non-égales

Moment de flexion maximum	BM	1.764 tm
Effort tranchant maximum	V	6.925 tonnes
Moment à gauche	M1	1.764 tm
Moment à droite	M2	-1.535 tm
Réaction à gauche	R1	6.925 tonnes
Réaction à droite	R2	4.420 tonnes

Type de raidisseur

Poutre Construite

Dimension de la tôle associée	320 x 15 mm	For section refer to; C20-14-601-01 C20-14-601-01 Sheet 7
Dimension de l'âme	172 x 10 mm	
Dimension du fer plat	137 # 25 mm	

Aire totale (tôle et raidisseur)	A	9945 mm ²	Hauteur de l'axe neutre	NA	74.8 mm
Aire résistant au cisaillement	Ac	2120 mm ²	Inertie p/r à l'axe neutre	Ixx	7845 cm ⁴
Poids linéaire		40.1 kg/m	Section module	SM	642.0 cm ³
avec tôle associée		77.6 kg/m	Déflexion maximale	D	-0.079 mm

Contrainte de flexion	σ	27.0 MPa
Contrainte de cisaillement	τ	32.0 MPa

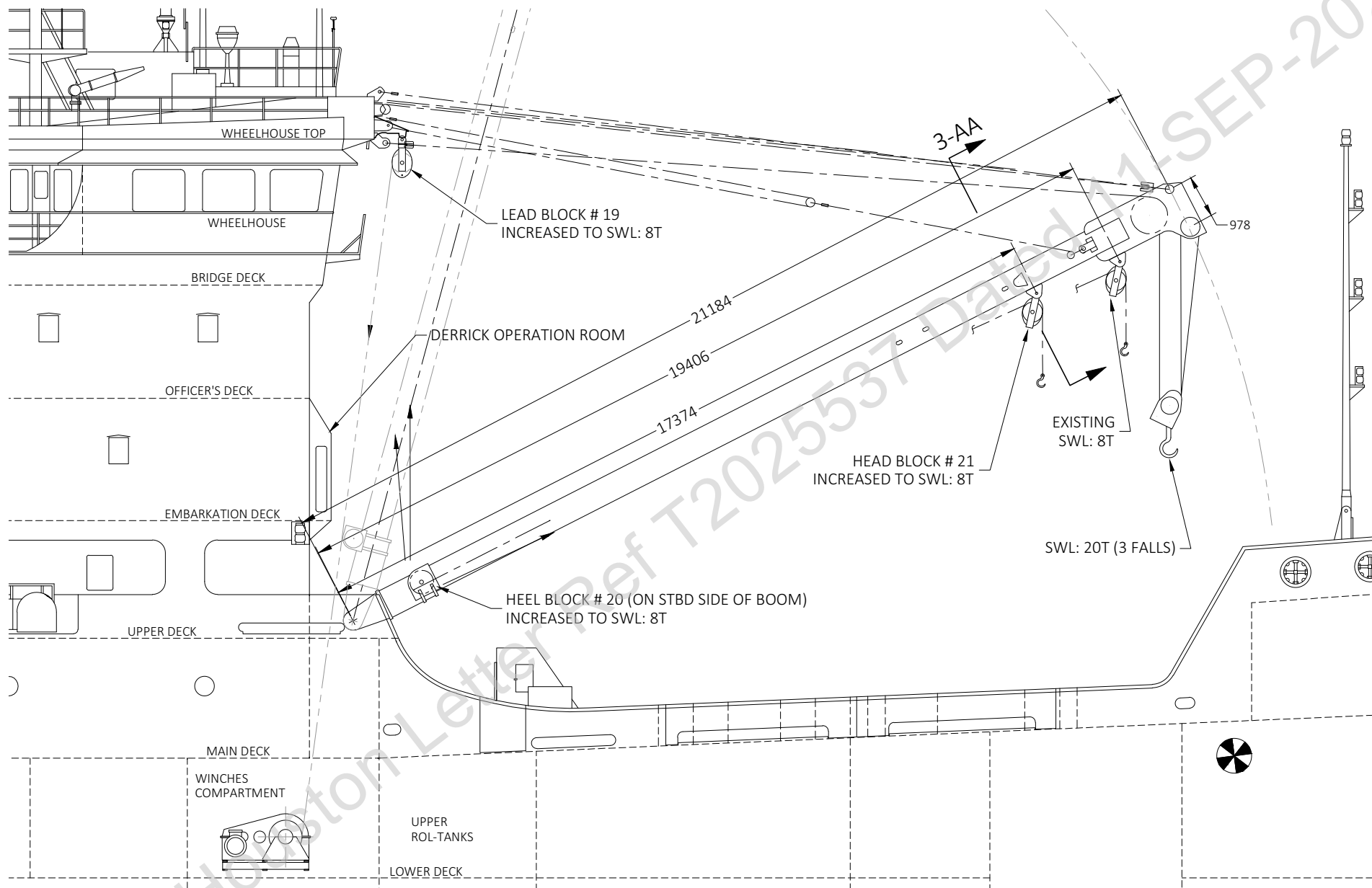


CONCEPT NAVAL
EXPERTS-CONSEILS | GÉNIE MARITIME

Canadian Coast Guard | Martha L. Black

Annexe B

Increase Hoist 5T to 8T Support Drawing



GENERAL PROFILE VIEW

SCALE 1:125

NOTES

1. REFER TO ANALYSIS REPORT C20-14-009-01 FOR MORE DETAILS ON THE CONVERSION FEASIBILITY

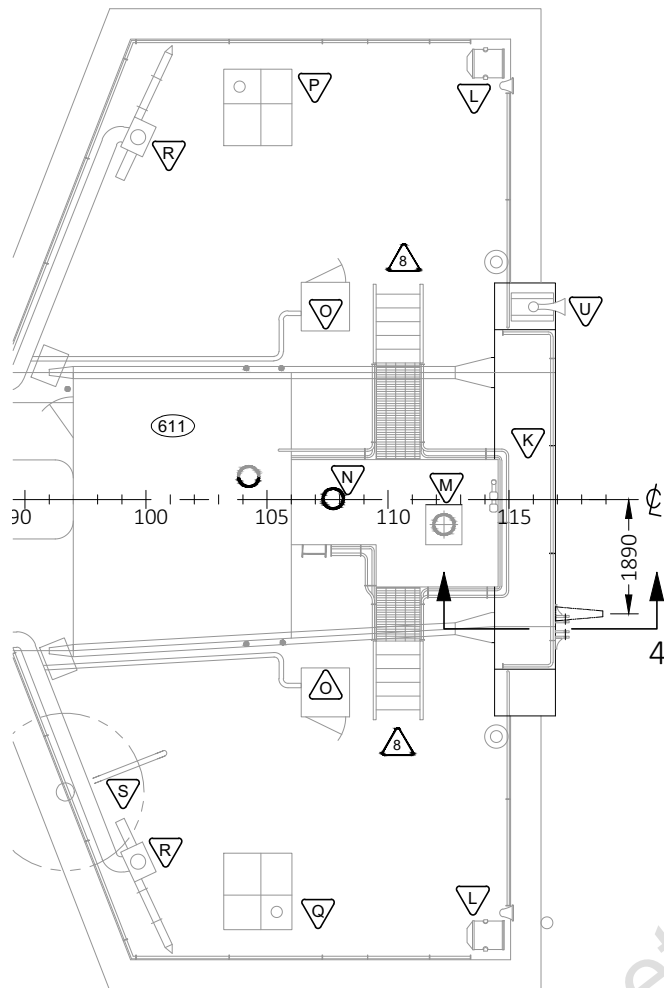
CLIENT/CLIENT:
CANADIAN COAST GUARD
PROJET/PROJECT:
MARTHA L. BLACK DERRICK
TITRE/TITLE:
INCREASE HOIST 5T TO 8 T

NO. DESSIN/DWG. NB: C20-14-601-01
REV. 1
DESSINÉ/DRAWN: T.C. / H.R.
FEUIL/SHIT 1 / 7

PRELIMINARY
PRECISE MESUREMENTS TO BE DONE ONBOARD

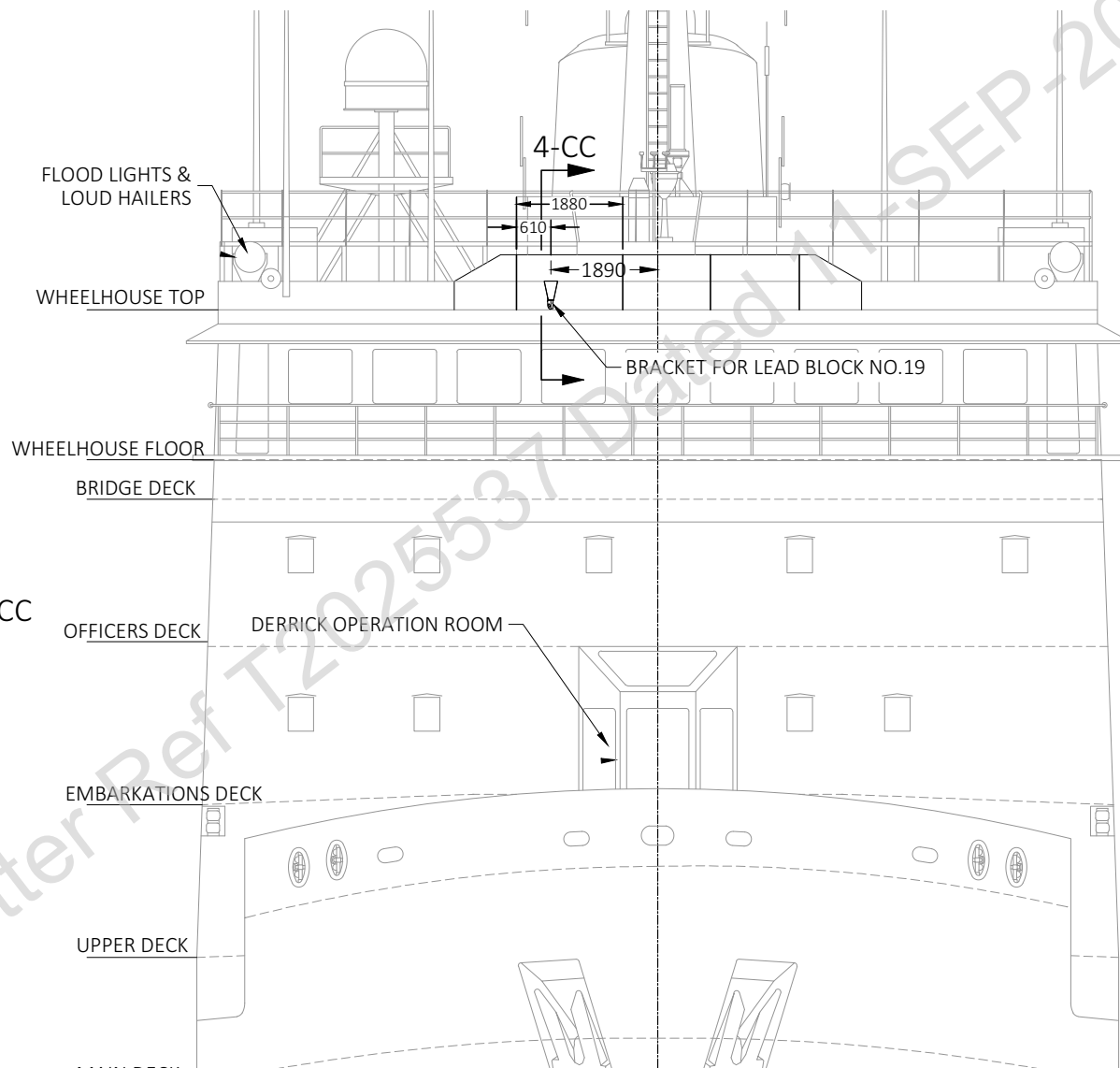


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PLAN VIEW ON WHEELHOUSE TOP

SCALE 1:125



FRONT VIEW OF DECKHOUSE

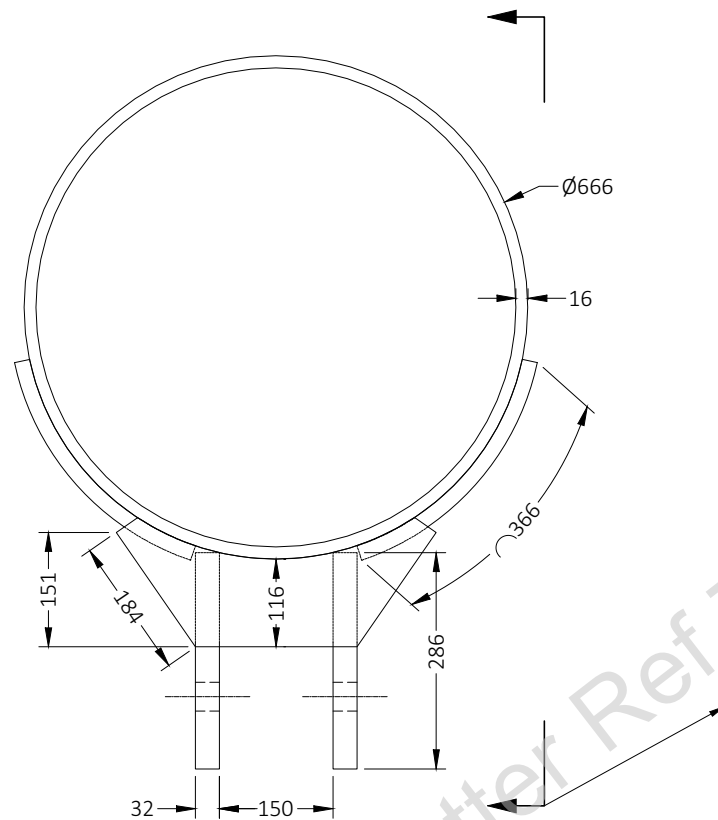
SCALE 1:125

CLIENT/CLIENT:
CANADIAN COAST GUARD
PROJET/PROJECT:
MARTHA L. BLACK DERRICK
TITRE/TITLE:
INCREASE HOIST 5T TO 8 T

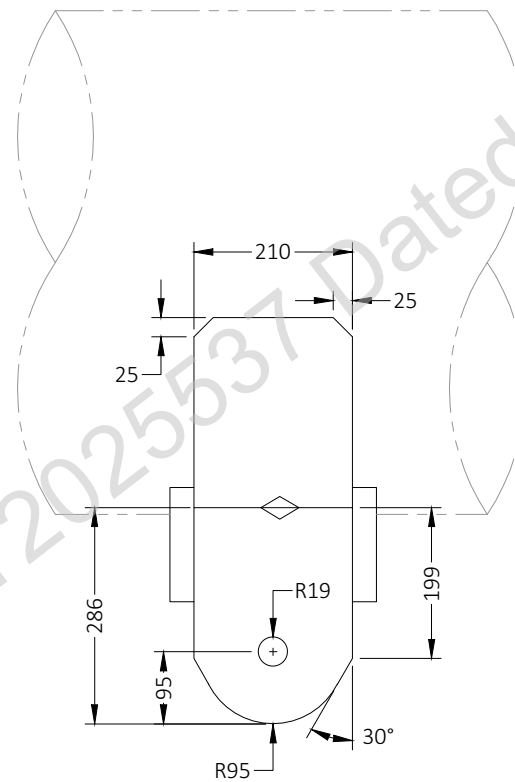
NO. DESSIN/DWG. NB: C20-14-601-01
REV. 1
DESSINÉ/DRAWN: T.C. / H.R.
FEUIL/SHIT 2 / 7
PRELIMINARY
PRECISE MESUREMENTS TO BE DONE ONBOARD



CONCEPT NAVAL
EXPERTS-CONSEILS | GÉNIE MARITIME



SECTION 3-AA
EXISTING DERRICK 5T HEAD BLOCK BRACKET
SCALE 1:10



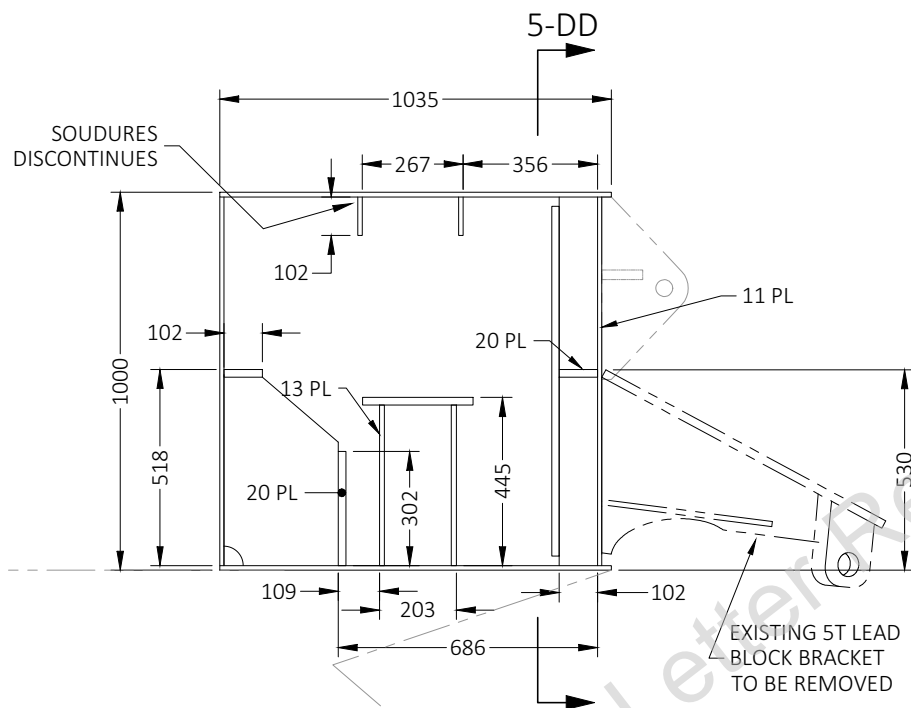
DETAIL 3-BB
HOIST BRACKET
ELEVATION
SCALE 1:10

CLIENT/CLIENT:
CANADIAN COAST GUARD
PROJET/PROJECT:
MARTHA L. BLACK DERRICK
TITRE/TITLE:
INCREASE HOIST 5T TO 8 T

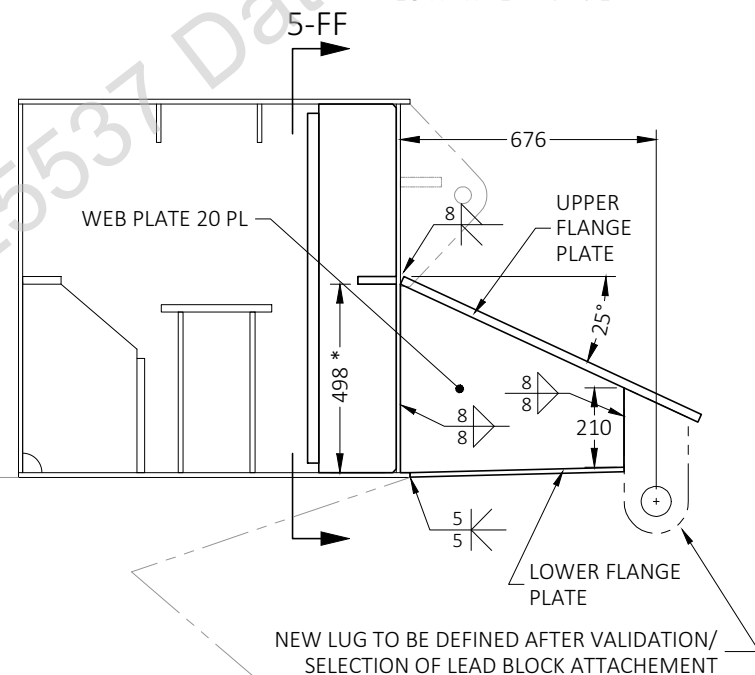
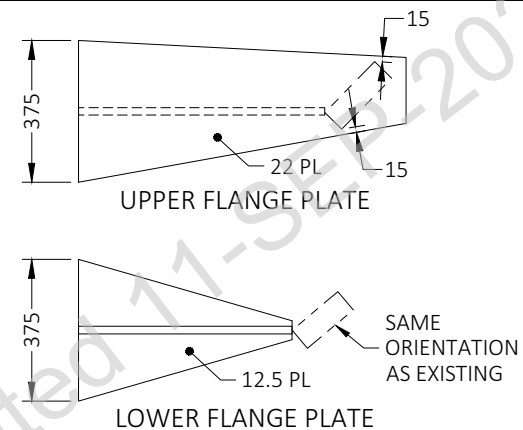
NO. DESSIN/DWG. NB: C20-14-601-01
REV. 1
DESSINÉ/DRAWN: T.C. / H.R.
FEUIL/SHIT 3 / 7
PRELIMINARY
PRECISE MESUREMENTS TO BE DONE ONBOARD



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DETAIL 4-CC
WHEELHOUSE TOP BOX
ELEVATION SECTION, EXISTING
SCALE 1:20



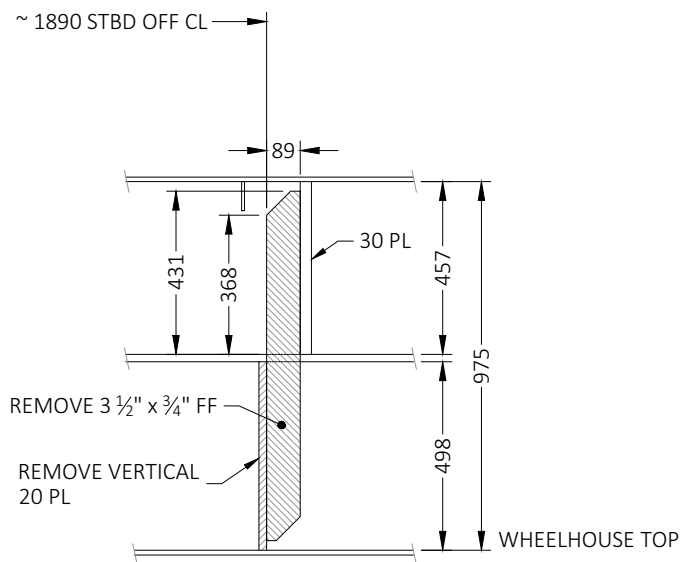
DETAIL 4-GG
WHEELHOUSE TOP BOX
ELEVATION SECTION, MODIFICATIONS
SCALE 1:20

CLIENT/CLIENT:
CANADIAN COAST GUARD
PROJET/PROJECT:
MARTHA L. BLACK DERRICK
TITRE/TITLE:
INCREASE HOIST 5T TO 8 T

NO. DESSIN/DWG. NB: C20-14-601-01
REV. 0
DESSINÉ/DRAWN: T.C. / H.R.
FEUIL/SHIT 4 / 6
PRELIMINARY
PRECISE MESUREMENTS TO BE DONE ONBOARD

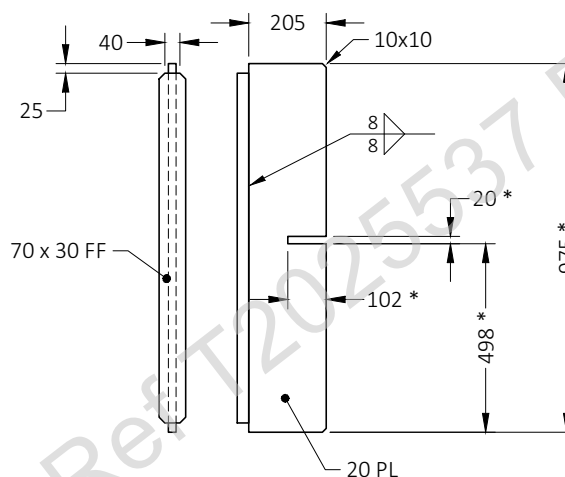


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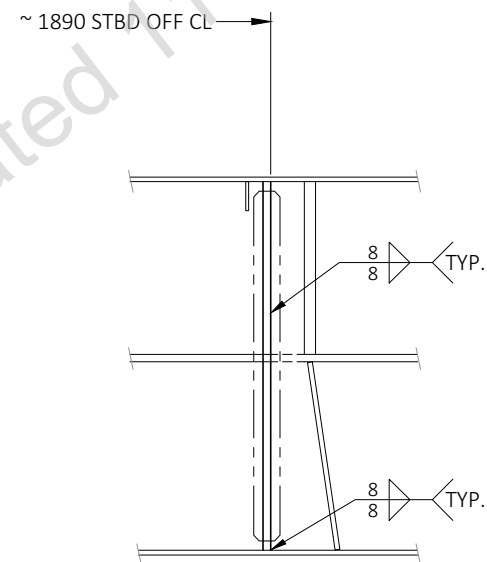
DETAIL 5-DD

INSIDE TOP BOX LOOKING FORWARD
EXISTING STRUCTURE I.W.O 5T LEAD BLOCK BRACKET
STRIP OUT



DETAIL 5-EE

INSIDE TOP BOX LOOKING FORWARD
PRE-FABRICATE NEW STIFFENER
* DIMENSIONS TO BE VALIDATED ON BOARD



DETAIL 5-FF

INSIDE TOP BOX LOOKING FORWARD
INSTALLATION OF NEW STIFFENER

NOTES

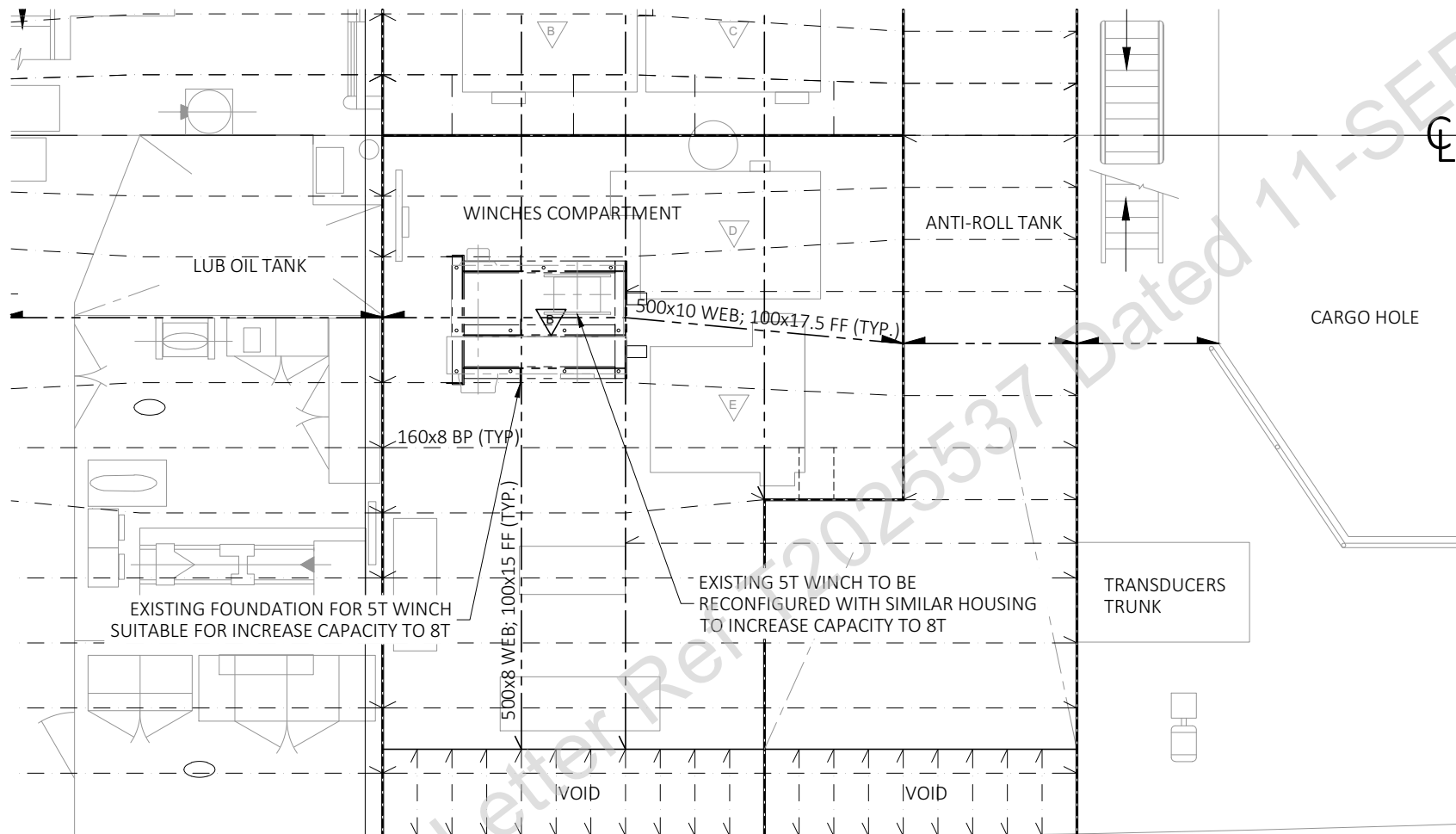
1. STEEL GRADES TO BE GRADE D OR EQUIVALENT FOR LOW TEMPERATURE APPLICATION.
2. WELDINGS AND PROCEDURES TO BE AS PER CLASS REQUIREMENTS.

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NO. DESSIN/DWG. NB: C20-14-601-01
REV. 1
DESSINÉ/DRAWN: T.C. / H.R.
FEUIL/SHIT 5 / 7
PRELIMINARY
PRECISE MESUREMENTS TO BE DONE ONBOARD



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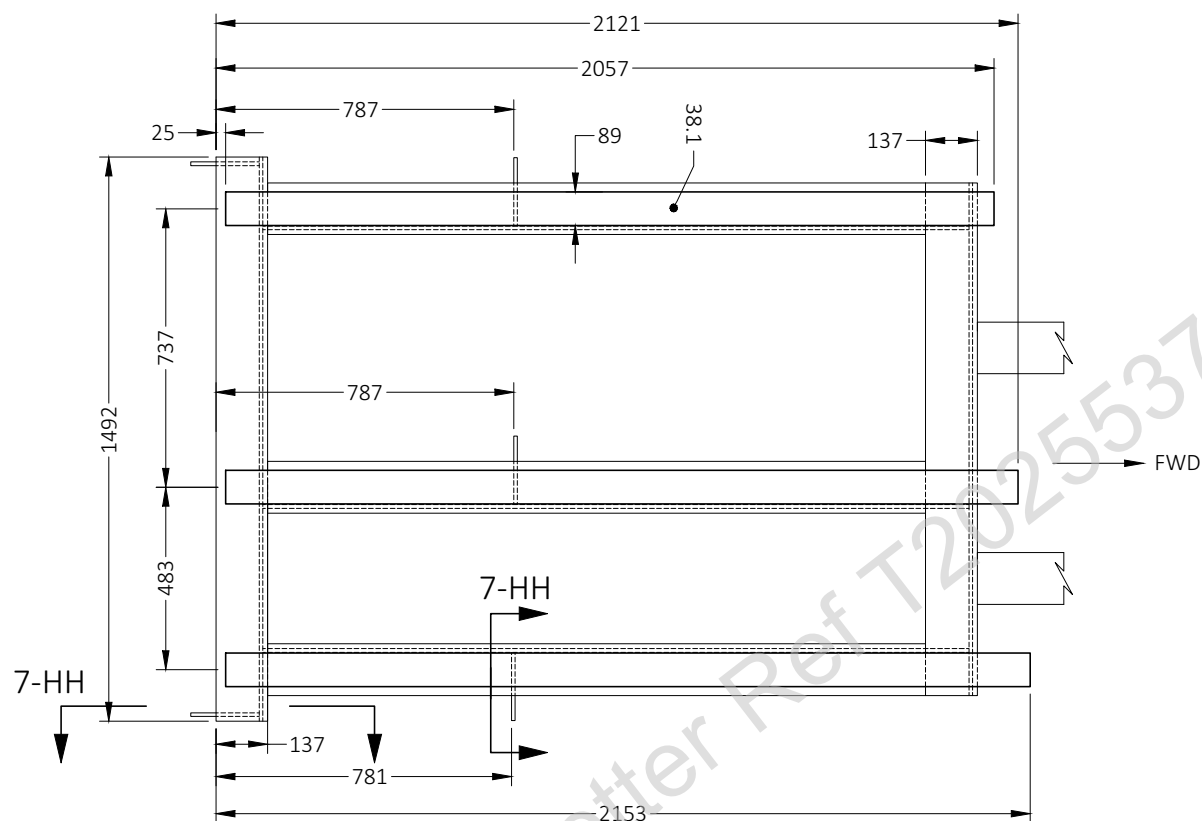
PLAN VIEW ON LOWER DECK
FOUNDATION FOR THE WINCH
SCALE 1:75

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 REV. 1
 DESSINÉ/DRAWN: T.C. / H.R.
 FEUIL/SHIT 6 / 7
 PRELIMINARY
 PRECISE MESUREMENTS TO BE DONE ONBOARD

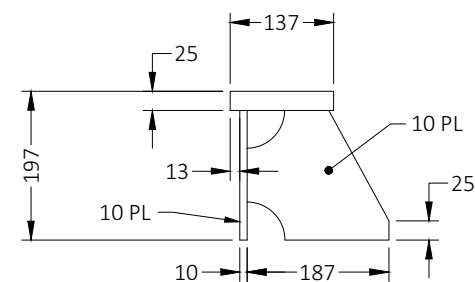


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EXISTING 5T WINCH SEAT (STBD)

PLAN VIEW
SCALE 1:20



DÉTAIL 7-HH

TYPICAL PROFILE SECTION
ÉCHELLE 1:10

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REV. 1
DESSINÉ/DRAWN: T.C. / H.R.
FEUIL/SHIT 7 / 7
PRELIMINARY
PRECISE MESUREMENTS TO BE DONE ONBOARD



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See ABS Houston Letter Ref T2025537 Dated 11-SEP-2020



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